Draft Final

INITIAL SCREENING OF ALTERNATIVES

Group I - Sites 05, 06 and 13

Group II - Site 08

Group III - Sites 12 and 14

Group VI - Site 10

NAVAL CONSTRUCTION BATTALION CENTER DAVISVILLE, RHODE ISLAND

Contract No. N62472-85-C-1026 April 1993

Prepared by:
TRC Environmental Corporation
TRC Project No. 13249-N41-10



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EXECUTIVE SUMMARY

Under the Navy's Installation Restoration Program and in accordance with the requirements of the Comprehensive Environmental Response, Compensation and Liability Act (CERCLA) as amended by the Superfund Amendments and Reauthorization Act (SARA), a Remedial Investigation/Feasibility Study is being conducted for the Naval Construction Battalion Center located in North Kingstown, Rhode Island (referred to as NCBC-Davisville). Included herein is the first step of the Feasibility Study, referred to as the Initial Screening of Alternatives, for the following groups of sites at the NCBC-Davisville facility:

- Group I Sites
 - Site 05 Transformer Oil Disposal Area
 - Site 06 Solvent Disposal Area
 - Site 13 Disposal Area Northwest of Buildings W-3, W-4, and T-1
- Group II Sites
 - Site 08 DPDO Film Processing Disposal Area
- Group III Sites
 - Site 12 Building 316, DPDO Transformer Oil Spill Area
 - Site 14 Building 38, Transformer Oil Leak Area
- Group VI Sites
 - Site 10 Camp Fogarty Disposal Area

The remaining sites at the NCBC-Davisville facility are being addressed within a separate report (TRC, .1993). All site locations are indicated in Figure ES-1.

The Feasibility Studies for the NCBC-Davisville sites are being performed in a phased manner. The Inital Screening of Alternatives Report is organized as follows:

 Information gained through previous investigations, including the Phase I Remedial Investigation, is summarized;

- Existing site contamination information is compared to Applicable or Relevant and Appropriate Requirements (ARARS), To-Be-Considered criteria (TBCs), and calculated risk-based cleanup levels based on future residential use and a 1 x 10⁻⁶ risk level;
- Remedial response objectives are developed;
- General response actions are identified;
- Remedial technologies and process options are screened;
- Remedial alternatives are developed;
- Remedial alternatives are evaluated individually and comparatively on the basis of effectiveness, implementability, and cost; and
- Remedial alternatives which do not offer significant advantages over comparable alternatives are screened from further analysis.

A Detailed Analysis of Alternatives Report (DAA) will be conducted at a later date incorporating Phase II Remedial Investigation (RI) results, as available. If necessary, additional remedial alternatives will be considered at that time based on the added site characterization data.

The Initial Screening of Alternatives (ISA) efforts are summarized on the following pages individually for each group of sites.

GROUP I SITES

SITE 05 - TRANSFORMER OIL DISPOSAL AREA, SITE 06 - SOLVENT DISPOSAL AREA, AND SITE 13 - DISPOSAL AREA NORTHWEST

<u>Site 05 - Transformer Oil Disposal Area</u>

Site 05 consists of an approximately 1,500 square foot area located east of Building 37, adjacent to Camp Avenue and just outside of the NCBC fence In 1968 or 1969, approximately 30 gallons of oil containing polychlorinated biphenyls (PCBs) were reportedly drained from a transformer and poured onto the ground at this site. While a soil sample collected in 1984 by the Navy contained 6 parts per million (ppm) of PCBs, subsequent surface and near surface soil sampling has not detected significant levels of Polynuclear aromatic hydrocarbons (PAHs), pesticides and inorganics have been identified in the site soils. Current and future carcinogenic risks due to exposures to site soils are estimated to range from 2.28×10^{-7} to 7.5 \times 10^{-5} based on worst case and most probable case exposure scenarios. These risk values are driven by arsenic, beryllium and PAHs. Non-cancer risk estimates for soil exposures were within the acceptable limit. No ground water investigation has been conducted at this site. The presence of inorganics in site soils presents a potential ecological risk under a theoretical worst-case scenario. Ecological risks will be further evaluated as part of the Phase II RI.

Site 06 - Solvent Disposal Area

Site 06 is a flat grassy area located between Buildings 67 and 38 and covering roughly a quarter of an acre in area. From 1970 to 1972, waste chlorinated hydrocarbon solvents were reportedly drained in this area, with an estimated total disposal volume of 1,750 gallons. Studies conducted at the site have included the sampling of surface and subsurface soils as well as ground water sampling from three monitoring wells located at the site. Contaminants detected in site soils include volatile organic compounds (VOCs), semi-volatile organic compounds (SVOCs) and inorganics. Inorganics were the only contaminants detected in ground water samples. Current and future carcinogenic risks due to exposures to site soils are estimated to range from 3.93×10^{-8} to 7.99×10^{-7} based on worst case and most probable case exposure scenarios, with PAHs driving the risk values. Worst-case ground water ingestion cancer risks were on the order of 1.10×10^{-3} , with arsenic and beryllium driving the risk estimate. Non-cancer risk estimates were less than the acceptable limit except for the worst-case childhood ingestion of ground water scenario, where manganese drives the calculated hazard index ratio. Ecological risks associated with the site appear to be minimal but will be further investigated within the Phase II RI.

Site 13 - Disposal Area Northwest

Site 13 is approximately 6 acres in size, bounded on three sides by roads. Three catch basins are located within the site area. From 1945 to 1955, this area was reportedly used for vehicle storage and the disposal of approximately 300 gallons of waste oils per month. Studies conducted at the

site have included the sampling of surface and subsurface soils, sediments from on-site catch basins, and ground water from the four on-site monitoring wells. Contaminants detected in site soils include VOCs, SVOCs, PCBs, pesticides and inorganics. The contaminants detected in site soils and catch basin sediment samples at the highest levels were PCBs. SVOCs and inorganics were detected in ground water samples. Current carcinogenic risks due to exposures to site soils are estimated at 2.53 x 10^{-3} for the worst case exposure scenario, with PCBs driving the risk value. Worst-case ground water ingestion cancer risks were on the order of 3.93 x 10^{-3} , with arsenic and beryllium driving the risk estimate. Non-cancer risk estimates exceeded the acceptable limit under both current use and future use scenarios based on PCB levels in site soils and ingestion of inorganics in ground water. Ecological risks associated with the site appear to be minimal but will be further investigated within the Phase II RI.

Comparison of Contaminant Levels to ARARs/TBCs and Risk-Based Cleanup Levels

Soil

PCBs were detected at Sites 05 and 13 in surface soils at levels exceeding the historic RIDEM cleanup standard of 1 ppm. When compared to the proposed RIDEM solid waste definition and TSCA cleanup standard for unrestricted areas of 10 ppm for PCBs, only Site 13 exhibits surface soil concentrations which exceed the 10 ppm value. Soil cleanup levels based on a 1 x 10^{-6} risk were calculated. At Site 05, risk-based cleanup levels for PAHs, arsenic and beryllium were exceeded and at Site 13, the risk-based cleanup level for arsenic was exceeded. However, reasonable maximum risks for future soil exposures at both Sites 05 and 13 fall within the acceptable carcinogenic risk range of 10^{-4} to 10^{-6} for remedial actions at Superfund sites. No risk-based soil cleanup levels were exceeded at Site 06.

Ground Water

Inorganics were detected at Sites 06 and 13 in ground water samples at levels exceeding MCLs, federal action levels or secondary MCLs. At Site 13, bis(2-ethylhexyl)phthalate was also detected at a level exceeding the MCL. At Sites 06 and 13, manganese was detected at levels exceeding the risk-based cleanup level.

Remedial Response Objectives

The following remedial response objectives were developed for soil and ground water at the Group I sites:

Soil

- Minimize current and future exposures to surficial soil contaminants at levels which exceed ARARs/TBCs or which pose unacceptable risks to human health and the environment; and
- Minimize off-site migration of surface soil contaminants.

Ground Water

Prevent exposure, due to ground water ingestion, to contaminants at levels exceeding acceptable ARARs/TBCs or which pose unacceptable risks to human health and the environment; and

 Minimize migration of ground water contaminants and any associated environmental impacts.

Development of Remedial Alternatives

With the remedial response objectives in mind, preliminary areas requiring remediation were estimated, remedial technologies identified, and technologies and associated process options were screened. Based on the lack of soil contaminants at Site 06 at levels exceeding ARARs/TBCs or risk-based cleanup levels, remediation of soils at Site 06 was not evaluated. Two soil remedial scenarios were evaluated for Sites 05 and 13, one in which the sites would be remediated to meet ARARs/TBCs and risk-based cleanup levels, and the other in which the sites would be remediated to meet only ARARs/TBCs (remaining risk levels would fall within the acceptable range of 10^{-4} to 10^{-6} for remedial actions).

With respect to ground water contamination, in evaluating the extent of ground water contamination at Sites 06 and 13, it was determined that sufficient information does not exist to allow for an analysis of appropriate ground water extraction, treatment or discharge alternatives at this time. Therefore, ground water at Sites 06 and 13 will be addressed as a separate operable unit upon completion of Phase II remedial investigations at these sites.

Based on the technology and process option screening, the remedial alternatives identified in Table ES-1 were developed. The alternatives include a no action alternative (I-1), a limited action alternative (I-2) consisting of site fencing and deed restrictions, a containment alternative (I-3) consisting of a RCRA Subtitle D soil cap and deed restrictions, and a disposal/treatment alternative (I-4) under which four soil disposal/treatment options were considered. They include off-site landfilling/incineration (Option A), on-site incineration (Option B), stabilization/solidification (Option C), and acid extraction and solvent extraction (Option D).

After conducting an initial evaluation of these alternatives on the basis of effectiveness, implementability and cost, all of the alternatives and options were retained evaluation in the Detailed for Analysis However, the remedial scenario under which soils would be remediated to meet both ARARs/TBCs and risk-based cleanup levels will be screened from further evaluation. Uncertainties associated with calculation of the risk-based cleanup levels as well as with the applicability of the risk-based cleanup levels to site-specific conditions are the basis of this screening. The significant additional cost of remediating to risk-based cleanup levels further supports this screening. The scenario in which the sites are remediated to meet ARARs/TBCs will be retained. If additional information gathered during the Phase II RI supports further consideration of remediation to meet risk-cased cleanup levels, the screened scenario will be re-evaluated within the Detailed Analysis of Alternatives:

GROUP II SITES

SITE 08 - DPDO FILM PROCESSING AREA

Site 08 - DPDO Film Processing Area

Site 08 consists of an approximately 1,600 square foot flat, grassy area located east of Building 314 at West Davisville. The area is reported to have received runoff from an adjacent paved area where waste liquids from a silver recovery process were reported discharged over a six-month period during 1973. A soil sample collected in 1985 contained 0.15 ppm of silver. Subsequent surface and near surface soil sampling and analysis has identified the presence of VOCs, PAHs, PCBs, and inorganics in surface or near surface soils. Future carcinogenic risks due to exposures to site soils are estimated at 3.14 x 10^{-5} based on the worst case exposure scenario. This risk value is driven by arsenic, beryllium, PAHs, PCBs and bis(2-ethylhexyl)phthalate. Non-cancer risk estimates for soil exposures were within the acceptable limit. No ground water investigation has been conducted at this site. Ecological risks associated with the site appear to be minimal but will be further investigated within the Phase II RI.

Comparison of Soil Contaminant Levels to ARARs/TBCs and Risk-Based Cleanup Levels

PCBs were detected in one Site 08 surface soil sample at a level exceeding the historic RIDEM cleanup standard of 1 ppm. When compared to the proposed RIDEM solid waste definition and TSCA cleanup standard for unrestricted areas of 10 ppm for PCBs, however, no exceedances are observed. Soil cleanup levels based on a 1 x 10^{-6} risk were calculated. Risk-based cleanup levels for PAHs, arsenic and beryllium were also exceeded at Site 08. However, it should be noted that existing reasonable maximum risks at Site 08 fall within the acceptable carcinogenic risk range of 10^{-4} to 10^{-6} for remedial actions at Superfund sites.

Remedial Response Objectives

The following remedial response objectives were developed for soil at the Group II site:

- Minimize current and future exposures to surficial soil contaminants at levels which exceed ARARs/TBCs or which pose unacceptable risks to human health and the environment; and
- Minimize off-site migration of surface soil contaminants.

Development of Remedial Alternatives

With the remedial response objectives in mind, preliminary areas requiring remediation were estimated, remedial technologies identified, and technologies and associated process options were screened. Two soil remedial scenarios were evaluated for Site 08: one in which the site would be remediated to meet ARARs/TBCs and risk-based cleanup levels, and one in which the site would be remediated to meet only ARARs/TBCs (remaining risk levels would fall within the acceptable range for remedial actions).

Based on the technology and process option screening, the remedial alternatives identified in Table ES-2 were developed. The alternatives include a no action alternative (II-1), a limited action alternative (II-2) consisting of site fencing and deed restrictions, a containment alternative (II-3) consisting of a RCRA Subtitle D soil cap and deed restrictions, and a disposal/treatment alternative (II-4) under which three soil disposal/treatment options were considered. They include off-site landfilling (Option A), off-site incineration (Option B) and fungal degradation (Option C).

After conducting an initial evaluation of these alternatives on the basis of effectiveness, implementability and cost, all of the alternatives and options were retained for evaluation in the Detailed Analysis of Alternatives.

GROUP III SITES

SITE 12 - BUILDING 316, DPDO TRANSFORMER SPILL AREA SITE 14 - BUILDING 38, TRANSFORMER OIL LEAK AREA

Site 12 - Building 316, DPDO Transformer Spill Area

Site 12 is located within Building 316 at West Davisville. In 1977, a transformer containing PCB oil was accidentally punctured with a forklift and the resultant spill area was cleaned up by NCBC-Davisville personnel. Subsequent sampling indicated the concrete was contaminated with PCBs and a removal action was implemented in 1991. Confirmation sampling conducted after the removal was completed indicated that the horizontal extent of PCB contamination is more extensive than originally believed.

Site 14 - Building 38, Transformer Oil Leak Area

Site 14 is located within Building 38, adjacent to Site 06. In 1981, oil spillage was noted in a transformer storage area within Building 38. The resultant spill area is believed to have been cleaned up by NCBC-Davisville personnel. Subsequent sampling indicated the asphalt surface was contaminated with PCBs and a removal action was implemented in 1991. Confirmation sampling conducted after the removal was completed indicated that, as with Building 316, the horizontal extent of PCB contamination is more extensive than originally believed.

Comparison of PCB Contaminant Levels to ARARs/TBCs

PCBs were detected in chip samples at Site 12 at concentrations as great as 1,200 ppm. At Site 14, chip sample concentrations as great as 150 ppm have been detected. Therefore, both sites exhibit PCB contamination at levels exceeding the historic RIDEM cleanup standard of 1 ppm and the proposed RIDEM solid waste definition and TSCA cleanup standard for unrestricted areas of 10 ppm for PCBs. One soil sample collected from the previous removal area at Site 14 contained PCBs at 1.6 ppm, which also exceeds the historic RIDEM cleanup standard.

Remedial Response Objectives

The following remedial response objectives were developed for floor surface materials at the Group III sites:

 Prevent exposures to PCB-contaminated surfaces and soil at levels which exceed ARARs/TBCs.

Development of Remedial Alternatives

With the remedial response objectives in mind, preliminary areas requiring remediation were estimated, remedial technologies identified, and technologies and associated process options were screened. Two remedial scenarios were evaluated for Sites 12 and 14: one in which the sites would be remediated to meet the historic RIDEM cleanup standard of 1 ppm PCBs, and one in which the sites would be remediated to meet the 10 ppm proposed RIDEM solid waste definition level and TSCA cleanup level.

Based on the technology and process option screening, the remedial alternatives identified in Table ES-3 were developed. The alternatives include a no action alternative (III-1), a limited action alternative (III-2) consisting of site access and deed restrictions, a containment alternative (III-3) consisting of sealing of PCB-contaminated surfaces, a disposal alternative (III-4) consisting of removal of contaminated floor surfaces and soil for disposal off-site at a TSCA-permitted landfill, and a treatment alternative (III-5) consisting of solvent washing of PCB-contaminated surfaces.

After conducting an initial evaluation of these alternatives on the basis of effectiveness, implementability and cost, all of the alternatives and options were retained for evaluation in the Detailed Analysis of Alternatives.

GROUP VI SITES

SITE 10 - CAMP FOGARTY DISPOSAL AREA

Site 10 - Camp Fogarty Disposal Area

Site 10 consists of an area within Camp Fogarty, a 347-acre parcel of land located in East Greenwich, Rhode Island. The study area is located in a depression west of an active firing range, between the firing range berms and a steeply rising hill to the west. The area is heavily wooded and interspersed with meadow areas. Ground water in the area is classified as GAA-NA. Cans of rifle- and weapon-cleaning oils and preservatives, as well as miscellaneous municipal-type garbage were reportedly occasionally disposed of in a shallow, sandy excavation in this area. The rifle bore oils were reportedly subsequently removed from the site and relocated at NCBC-Davisville. Rusted empty paint cans, 55-gallon drums and miscellaneous metal parts are visible on the site's surface. Surface and near-surface soil sampling as well as ground water sampling have been conducted at the site. PAHs and inorganics have been identified in the site soils. Inorganics have been detected in ground water samples. Current and future carcinogenic risks due to exposures to site soils are estimated to range from 3.33 x 10^{-7} to 2.63 $imes 10^{-6}$ based on worst case and most probable case exposure scenarios. These risk values are driven by arsenic, beryllium and PAHs. Worst-case ground water ingestion cancer risks were on the order of 7.17×10^{-4} , with arsenic driving the risk estimate. Non-cancer risk estimates were within the acceptable limit for both soil and ground water exposures. With respect to potential ecological risks, current access restrictions would tend to reduce exposures to most ecological receptors. However, the known breeding of two State Species of Concern, the marbled and four-toed salamanders, in the vicinity of the site justifies further analysis of risks, as will be conducted during the Phase II RI.

Comparison of Contaminant Levels to ARARs/TBCs and Risk-Based Cleanup Levels

Soil

No soil contaminants were detected at levels exceeding available ARARs/TBCs. Soil cleanup levels based on a 1 x 10^{-6} risk were calculated. PAHs and beryllium were detected at levels exceeding calculated risk-based cleanup levels. Arsenic was detected in a soil sample collected as a background sample at a level exceeding calculated risk-based cleanup levels. However, reasonable maximum risks for future soil exposure fall within the acceptable carcinogenic risk range of 10^{-4} to 10^{-6} for remedial actions at Superfund sites.

Ground Water

Inorganics were detected at Site 10 in ground water samples at levels exceeding MCLs, federal action levels or secondary MCLs. No risk-based cleanup levels were calculated for Site 10 ground water contaminants.

Remedial Response Objectives

The following remedial response objectives were developed for soil and ground water at the Group VI site:

Soil

 Minimize current and future exposures to surficial soil contaminants at levels which pose unacceptable risks to human health and the environment; and

Minimize off-site migration of surface soil contaminants.

Ground Water

Prevent exposure, due to ground water ingestion, to contaminants at levels exceeding acceptable ARARs/TBCs;

Minimize migration of ground water contaminants and any associated environmental impacts; and

Restore contaminated ground water for future designated use (GAA).

Development of Remedial Alternatives

With the remedial response objectives in mind, preliminary areas requiring remediation were estimated, remedial technologies identified, and technologies and associated process options were screened. Because no soil contaminants were identified at levels exceeding ARARs/TBCs, a single soil remedial scenario was evaluated for Site 10, one in which the site is remediated to meet risk-based cleanup levels.

In evaluating the extent of ground water contamination at Site 10, it was determined that, while sufficient information does not exist to allow for a detailed analysis of ground water extraction, treatment or discharge alternatives, because the site is in a class GAA area a preliminary evaluation of ground water remediation is appropriate at this time. Ground water remediation will be addressed in more detail upon completion of Phase II remedial investigations at this site.

Based on the technology and process option screening, the remedial alternatives identified in Table ES-4 were developed. The alternatives include a no action alternative (VI-1), a limited action alternative (VI-2) consisting of continued ground water monitoring, site fencing and deed restrictions, a containment alternative (VI-3) consisting of a RCRA Subtitle D soil cap and deed restrictions with an option for construction of a slurry wall, and an active restoration alternative (VI-4) under which various soil and ground water treatment options were considered. They include off-site landfilling (Option A), soil washing (Option B), stabilization/solidification (Option C), ground water extraction (Option D), ground water treatment using membrane microfiltration (Option E), ground water treatment using ion exchange (Option F) and discharge of treated ground water to ground water (Option G) or to surface water (Option H).

After conducting an initial evaluation of these alternatives on the basis of effectiveness, implementability and cost, it was determined that the reduction in risk offered by the soil treatment options, Options A, B and C under Alternative VI-4, is not well-defined. Uncertainties are associated with the calculation of the risk-based cleanup levels as well as with the applicability of the risk-based cleanup levels to site-specific conditions. Implementation of the soil treatment alternatives could only be accomplished at a very high cost. Therefore, the soil treatment options are screened from further evaluation. If significantly increased soil exposure risks or contaminant levels exceeding ARARS/TBCs are identified as a result of Phase II remedial investigations, soil treatment options will be reconsidered. All of the remaining alternatives and options were retained for evaluation in the Detailed Analysis of Alternatives.

TABLE ES-1 ALTERNATIVES UNDERGOING PRELIMINARY SCREENING SURFACE SOIL/SEDIMENT GROUP I SITES - SITE 05, 06, 13

Alternative I-1

No Action

Alternative I-2

Limited Action

- Fencing/Deed Restrictions

Alternative I-3

Containment

- RCRA Subtitle D Soil Cap/Deed Restrictions

Alternative I-4

Active Restoration

- Off-Site Landfill/Off-Site Incineration or
- On-Site Incineration or
- Stabilization/Solidification or
- Acid Extraction and Solvent Extraction

TABLE ES-2 ALTERNATIVES UNDERGOING PRELIMINARY SCREENING SURFACE SOIL GROUP II SITE - SITE 08 (DPDO FILM PROCESSING AREA)

Alternative II-1

No Action

Alternative II-2

Limited Action

- Fencing/Deed Restrictions

Alternative II-3

Containment

- RCRA Subtitle D Soil Cap/Deed Restrictions

Alternative II-4

Active Restoration

- Off-Site Landfill or
- Off-Site Incineration or
- Fungal Degradation

TABLE ES-3 ALTERNATIVES UNDERGOING PRELIMINARY SCREENING BUILDING SURFACES AND SURFACE SOILS GROUP III SITES - SITE 12 (BUILDING 316) AND SITE 14 (BUILDING 38)

Alternative III-1

No Action

Alternative III-2

Limited Action

- Site Access/Deed Restrictions

Alternative III-3

Containment

- Surface Sealing

Alternative III-4

Excavation/Treatment/Disposal

- Removal with Off-Site Disposal/Incineration

Alternative III-5

Treatment

- Solvent Washing

TABLE ES-4 ALTERNATIVES UNDERGOING PRELIMINARY SCREENING SURFACE SOIL/GROUND WATER GROUP VI SITE - SITE 10 (CAMP FOGARTY DISPOSAL AREA)

Alternative VI-1

No Action

Alternative VI-2

Limited Action

- Fencing/Deed Restrictions/Continued Ground Water Monitoring

Alternative VI-3

Containment

- RCRA Subtitle D Soil Cap and/or Slurry Wall

Alternative VI-4

Active Restoration

Soil Remediation:

- Off-Site Landfill or
- Soil Washing or
- Stabilization/Solidification

and Ground Water Restoration:

- Extraction Wells or
- Interceptor Trench

and

- Membrane Microfiltration or
- Ion Exchange

and

- Discharge to Ground Water or
- Discharge to Surface Water

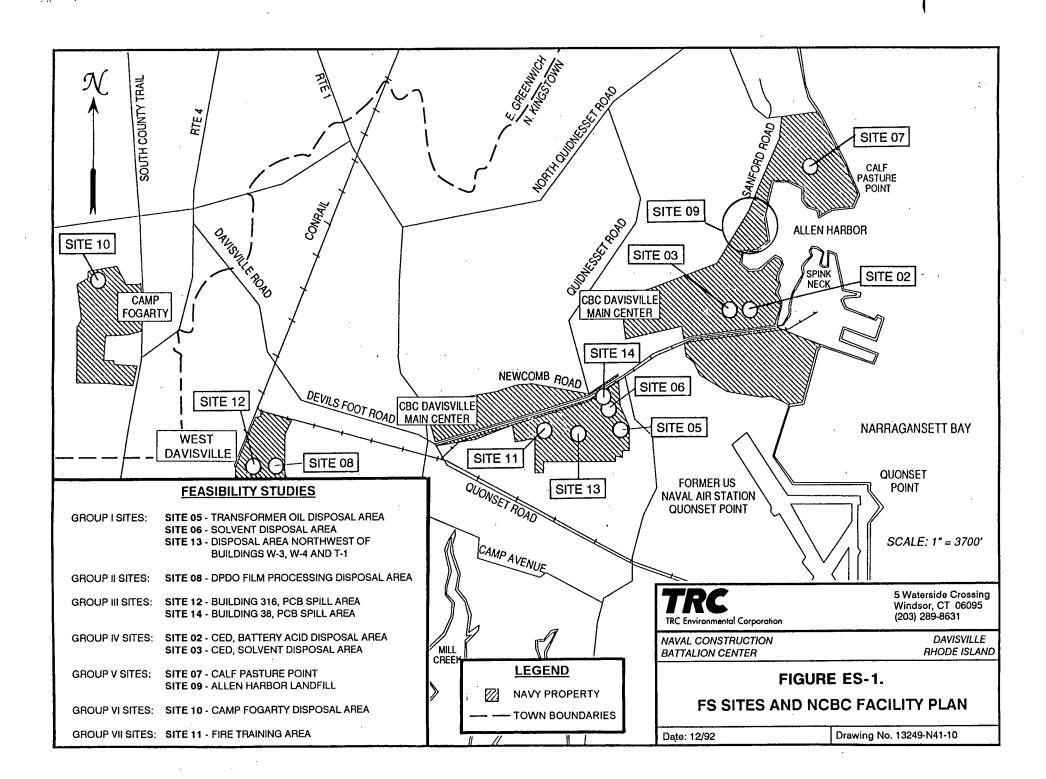


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1.0 INTRODUCTION

TRC Environmental Corporation (TRC) is conducting a Remedial Investigation/Feasibility Study (RI/FS) at the Naval Construction Battalion Center, located in the northeast section of the town of North Kingstown, Rhode Island (NCBC-Davisville). The RI/FS is being conducted under the Navy's Installation Restoration Program and in accordance with the requirements of the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA), as amended by the Superfund Amendments and Reauthorization Act (SARA). The study is being performed by TRC under Contract N62472-85-C-1026 for NORTHNAVFACENGCOM.

This Feasibility Study will assess potential remedial technologies applicable to environmental conditions at NCBC-Davisville, as defined by existing site information. Previous investigations under which environmental data have been developed include the following:

- Initial Assessment Study (IAS) (Hart, 1984a);
- Verification Step Report (part of a Confirmation Study) (TRC, 1987); and
- Phase I RI Draft Final Report (TRC, 1991).

Based on these studies, twelve sites have been identified for which Feasibility Study efforts are being initiated. The site numbers were assigned during the IAS and have been retained under this investigation for consistency. These twelve sites have been grouped for the purposes of preparing Feasibility Studies as follows:

• Group I Sites*

- Site 05 Transformer Oil Disposal Area
- Site 06 Solvent Disposal Area
- Site 13 Disposal Area Northwest of Buildings W-3, W-4 and T-1

• Group II Sites*

- Site 08 - DPDO Film Processing Disposal Area

• Group III Sites*

- Site 12 Building 316, DPDO Transformer Oil Spill Area
- Site 14 Building 38, Transformer Oil Leak Area

• Group IV Sites

- Site 02 CED, Battery Acid Disposal Area
- Site 03 CED, Solvent Disposal Area

Group V Sites

- Site 07 Calf Pasture Point
- Site 09 Allen Harbor Landfill

Group VI Sites*

- Site 10 Camp Fogarty Disposal Area
- Group VII Sites
 - Site 11 Fire Fighting Training Area

The first step of the Feasibility Study, the Initial Screening of Alternatives (ISA) presented herein, addresses the Group I, Group II, Group III and Group VI sites, noted above with an asterisk (*). The remaining groups of sites will be addressed within a separate report (TRC, 1993).

The purpose of the ISA presented herein is to identify and evaluate alternatives for mitigating site-related contamination at the seven Group I, II, III and VI NCBC-Davisville sites and for controlling the effects of contamination on public health and the environment. By evaluating remedial solutions selected from the range of technologies available for site cleanup, a response can be formulated which is technically feasible, protects public health and the environment, is cost-effective, and is consistent with applicable or relevant environmental standards. The Feasibility Study process was formulated by the U.S. EPA to properly implement CERCLA. The National Oil and Hazardous Substances Pollution Contingency Plan (NCP, 40 CFR Part 300) establishes the framework for performing Feasibility Studies. Further

definition of the FS process is provided in the <u>Guidance for Conducting</u>

Remedial Investigations and Feasibility Studies under CERCLA (U.S. EPA,

Interim Final, October 1988).

Figure 1-1 provides a summary of the approach being used in this investigation to formulate appropriate remedial responses for the seven Group I, II, III and VI NCBC-Davisville sites. The FS is being conducted in phases. This ISA report uses the following general report format:

Introduction/Background Information
Assessment of Applicable or Relevant and Appropriate Requirements
(ARARs)

For each group of sites:

- Site-Specific Information
- General Response Actions
- Identification and Screening of Technologies
- Development and Initial Screening of Alternatives References

The second step of the FS, a Detailed Analysis of Alternatives report, will be prepared subsequent to this document and will include the detailed analysis of remedial alternatives.

Because a second phase of remedial investigations (Phase II RI) will be conducted at most of the sites, the information gained from these investigations will be considered when preparing the Detailed Analysis of Alternatives Report. If warranted by the presence of additional contaminants or increased potential risks to human health or the environment, remedial technologies or process options will be re-evaluated at that time.

1.1 Site Location and Description

NCBC-Davisville is located in the northeast section of the town of North Kingstown, Rhode Island, approximately 18 miles south of Providence. A site location map is provided in Figure 1-2. A significant portion of

NCBC-Davisville is contiguous with Narragansett Bay. NCBC-Davisville is composed of three areas including the Main Center, the West Davisville storage area, and Camp Fogarty, a training facility located approximately 4 miles west of NCBC-Davisville. These areas as well as the locations of the individual FS sites, are noted in Figure 1-3.

Adjoining NCBC-Davisville's boundary on the south is the decommissioned Naval Air Station (NAS) Quonset Point that was declared excess to the Navy in April, 1973. The Quonset Point area is currently owned by the Rhode Island Port Authority (RIPA) and the Rhode Island Department of Transportation (RIDOT), along with some private companies. Hereafter, this area will be referred to as NAS Quonset Point, to distinguish it from NCBC-Davisville.

1.2 NCBC-Davisville History

Quonset Point was the location of the first annual encampment of the Brigade Rhode Island Militia in 1893. During World War I, it was designated for the mobilization and training of troops and later was the home of the Rhode Island National Guard. In the 1920s and 1930s, Quonset Point functioned as a summer resort.

In 1939, Quonset Point was acquired by the Navy to establish a Naval Air Station (NAS), and construction began in 1940. During construction, millions of cubic yards of sediment were dredged to create a ship basin and channel.

By 1942, the operations at NAS Quonset Point had expanded into what is now called NCBC-Davisville. Land at Davisville adjacent to NAS Quonset Point was designated the Advanced Base Depot, and the first of two piers was constructed. Later that year the Naval Construction Training Center (NCTC), known as Camp Endicott, was established to train the newly established construction battalions.

After World War II, activities at NAS Quonset Point remained the same, providing an operating base for aircraft and ships. After 1947, NAS Quonset Point was a site of carrier-based jet aviation. The Antarctic Development Squadron Six was moved to NAS Quonset Point in 1956. A Naval Air Rework Facility (NARF) was created there in 1967. The Naval Hospital was established in 1968.

The NCBC-Davisville area was inactive between World War II and the Korean Conflict. In 1951 it became the Headquarters Construction Battalion Center (CBC). In 1974, the NAS and NARF at Quonset Point were decommissioned, and operations at Davisville were greatly reduced. In 1980, RIPA purchased NAS Quonset Point and the two Davisville piers from the Navy. Current boundaries of the NCBC facility are indicated in Figure 1-3. In 1989, the closure of Davisville was announced, and all operations at Davisville were phased down to the present staffing levels for Public Works, Maintenance, Security and Navy Personnel. Because the future use of most of the facility is unknown, future residential use will be assumed for evaluating preliminary site remediation levels. Site 10, Camp Fogarty, is proposed to be excessed to the U.S. Army. Therefore, continuation of the current use scenario will also be evaluated for Site 10.

1.3 History of Facility Response Actions at NCBC-Davisville

1.3.1 Previous Investigations - U.S. Navy

The Navy Assessment and Control of Installation Pollutants (NACIP) Office awarded Navy Contract No. N62474-83-C-6974 to Fred C. Hart Associates, Inc. (Hart) to conduct an Initial Assessment Study (IAS) of potentially contaminated sites at both NCBC-Davisville and NAS Quonset Point. The IAS identified a total of 14 potentially contaminated sites at NCBC-Davisville

(Hart, 1984a). The IAS concluded that 3 of the 14 sites identified at NCBC-Davisville posed a sufficient threat to human health or to the environment to warrant additional investigation. The IAS report recommended that the Navy conduct a Confirmation Study (CS) as described in the NACIP program on the following three sites: Site 05 - Transformer Oil Disposal Area, Site 07 - Calf Pasture Point, and Site 09 - Allen Harbor Landfill.

A copy of the IAS was submitted by the Navy to the Rhode Island Department of Environmental Management (RIDEM) for review and comment. In a letter dated October 19, 1984, RIDEM presented its review findings and requested that the Navy add 7 of the 14 sites originally identified in the IAS to the list of sites to be examined in the upcoming Confirmation Study. The Navy agreed to the RIDEM request.

The Navy awarded a Confirmation Study (Contract No. N62472-85-C-1026) to TRC Environmental Consultants, Inc. (TRC) in March 1985. Thirteen sites were investigated as part of the Verification Step of the Confirmation Study. The scope of work for the Verification Step included the three sites identified in the IAS as needing additional study, the seven sites requested by RIDEM, and three sites added by the Navy. The sites investigated during the Verification Step program are:

- Site 02 CED Battery Acid Disposal Area;
- Site 03 CED Solvent Disposal Area;
- Site 04 CED Asphalt Disposal Area;
- Site 05 Transformer Oil Disposal Area;
- Site 06 Solvent Disposal Area;
- Site 07 Calf Pasture Point;
- Site 08 DPDO Film Processing Disposal Area;
- Site 09 Allen Harbor Landfill;
- Site 10 Camp Fogarty Disposal Area;
- Site 11 Fire Fighting Training Area;
- Site 12 DPDO Transformer Oil Spill Area;
- Site 13 Disposal Area Northwest of Buildings W-3, W-4 and T-1;
- Site 14 Building 38, Transformer Oil Leaks.

A draft report of the Verification Step of the NCBC-Davisville Confirmation Study was submitted to RIDEM for review and comment. The RIDEM comments suggested additional sampling be conducted, which TRC subsequently performed. The final report of the Verification Step was completed by TRC on February 27, 1987. The Navy received a letter from RIDEM listing their review comments on the final report on September 30, 1987.

1.3.2 Previous Investigations - U.S. EPA

NCBC-Davisville was proposed by the U.S. Environmental Protection Agency (EPA) for inclusion on the National Priority List (NPL) in July 1989.

NCBC-Davisville was added to the NPL on November 21, 1989. EPA developed a Hazard Ranking System (HRS) scoring package to support the proposed and final listings (U.S. EPA, 1989a). The HRS package was based on existing information; a Preliminary Assessment/Site Investigation was not performed.

The HRS package noted that of the 24 potential sites which were identified in a combined study of NCBC-Davisville, West Davisville, Camp Fogarty, and the decommissioned Quonset Point, the most serious sites of concern, and the sites which were aggregated to form the basis of the ranking package, are Site 09 - Allen Harbor Landfill and Site 07 - Calf Pasture Point.

Of the 24 potential sites listed in the HRS package, the areas designated 1 through 14 coincide with the 14 areas identified in the Navy's IAS. The remaining potential areas, 15 through 24, were identified by the EPA from an "Off-Site Activity Investigation" report (Hart, 1984b). The HRS package notes that areas 15 through 24 are on property not currently owned or operated by the U.S. Navy and are not included as part of the NPL site. Several of these areas are being investigated by the Army Corps of Engineers' program aimed at former defense facilities.

1.3.3 Current Remedial Investigation

In 1988, the Navy's three-phase NACIP Program was restructured to conform with EPA's four-phase program. This change was predicated by the Superfund Amendments and Reauthorization Act (SARA) of 1986. The U.S. Navy changed its NACIP Program to closely parallel the EPA requirements for remedial actions at Superfund sites. The Navy's program is now called the Installation Restoration (IR) Program. Under the IR Program, current investigations at NCBC-Davisville are in the Remedial Investigation/Feasibility Study (RI/FS) phase.

In March 1988, TRC was tasked by the Navy to implement recommendations of the Confirmation Study - Verification Step by developing a Plan of Action as a NACIP Confirmation Study - Characterization Step to conduct more extensive sampling. Shortly after initiating this task, the Navy requested TRC to develop a Remedial Investigation (RI) Work Plan conforming to the newly-established Navy IR Program, and to the extent possible, conforming to current EPA requirements under the NCP and the EPA draft RI guidance (U.S. EPA, 1988a). The resulting Phase I RI/FS Work Plan included a Field Sampling Plan, a Health and Safety Plan, a Quality Assurance Project Plan and a Data Management Plan (TRC, 1988). The Phase I RI field investigations were conducted from September 1989 to March 1990 and the Phase I RI Draft Final Report was submitted to the Navy in May 1991. Additional field investigations have been proposed under a Phase II RI/FS Work Plan (TRC, 1992).

1.4 Regional Geology, Hydrogeology and Hydrology

The regional and site-specific geology, hydrogeology and hydrology are briefly discussed in the following sections. More comprehensive descriptions are provided in the Phase I RI Draft Final Report (TRC, 1991) and the Phase II RI/FS Work Plan (TRC, 1992).

1.4.1 Regional Geology

The area of Narragansett Bay, including the surrounding lowlands and islands in the Bay, overlies the Narragansett Basin. This geologic structure is a complex syncline of Pennsylvanian Age metasedimentary rocks about 12 miles wide and up to 12,000 feet deep. The Narragansett Basin's western limit is about 3 miles west of NCBC-Davisville, and its eastern edge is close to Fall River, Massachusetts. All of the NCBC-Davisville sites except Site 10, Camp Fogarty, overlie the Narragansett Basin. The bedrock is overlain by various glacial deposits up to 200 feet thick that have left the basin area relatively flat compared to the surrounding areas (Schafer, 1961).

The bedrock forming the basin is comprised of five formations which consist chiefly of non-marine conglomerates, sandstones, and shales. The principal unit is the Rhode Island Formation, which consists of a gray-greenish fine to coarse conglomerate, sandstone, lithic graywacke, graywacke, arkose, shale, and a minor amount of meta-anthracite and anthracite.

According to Johnson and Marks (1959), in the vicinity of NCBC-Davisville, the bedrock is more than 90 feet below sea level in the West Passage of Narragansett Bay, greater than 70 feet below sea level just west of Frys Pond, nearly 50 feet below sea level near the West Davisville facility, and nearly 100 feet above sea level near Camp Fogarty. The Geologic Map and Sections of the Wickford Quadrangle, Rhode Island (Williams, Bulletin 1158-C, 1964) and visual observations identify a major bedrock outcrop just west of Frys Pond (approximately 300 yards east of Site 05).

The unconsolidated soils overlying the bedrock consist of three general types of glacial deposits: till, water-laid deposits, and wind-deposited material. In the Davisville area, till is exposed along highlands such as Lippitt Hill, the hillside due west of the rifle and pistol range at Camp

Fogarty, and along the hillside of the ridge between West Davisville and NCBC-Davisville. Just northeast of Site 02, there is an end moraine deposit which controlled the pro-glacial melt water drainage system.

Most of the surficial geologic soils in the Davisville area are water-laid deposits. Melt water streams flowing along the west side of the end moraine near Site 02 deposited a sequence of sands and silts over most of NCBC-Davisville, including Sites 02, 03, 05, 06, 11, 13, and 14. Melt water streams also deposited layers of sand and silt near West Davisville and the Allen Harbor Landfill. Fine-grained glaciolacustrine soils underlie Calf Pasture Point. At Camp Fogarty, the rifle and pistol range overlies a kame terrace consisting of sand and gravel deposited by melt water streams which flowed alongside the glacier which moved through the Hunt River valley.

Wind deposited materials in the Davisville area are loose, heterogeneous, and relatively thin in comparison to the other glacial deposits in the area [10 feet at the higher elevations, and over 150 feet thick in some portions of the bedrock valleys (Schafer, 1961)].

1.4.2 Regional Hydrogeology

Ground water hydrogeology in the Davisville area is controlled by the geographic and geologic setting. The underlying bedrock units have primary porosites (pore openings between the grains of mineral crystals forming the rock) of less than 1% and very low secondary porosites (joints, fractures and openings along bedding planes), with only the secondary openings capable of yielding significant amounts of water. In general, well yields from the bedrock formations are low (22 gallons per minute or gpm from an average depth of approximately 225 feet). Flow from the secondary openings is greatest in the top 250 to 300 feet of bedrock (Rhode Island Development Council, 1952).

In the Davisville area, the bedrock is not the principal aquifer and, therefore, is penetrated by only a small portion of wells.

The glacial soils in the Davisville area generally consist of stratified sand/gravel interbedded with very fine sand and silt; glacial till (a heterogeneous mixture of silt, sand, clay, and gravel), and stratified sand or gravel interbedded with varying amounts of glacial till. All of these materials will yield ground water, but only the stratified sands or gravels are permeable enough to yield large quantities of water for development. These very permeable materials form the Hunt Ground Water Reservoir, which is the principal source of potable water in the area. The extent of the Hunt Ground Water Reservoir in the vicinity of NCBC-Davisville is indicated in Figure 1-4. The specific yield capacities can range between 5 and 300 gallons per minute per foot drawdown (gpm/ft). Some wells yield as much as 2,700 gpm. A hydrologic review of the aquifer recharge and discharge shows the long-term sustained yield of the entire Hunt Ground Water Reservoir is about 13 million gallons per day (mgd) (Rosenshein, Gonthiel and Allen, 1968).

Ground water in the Davisville area is unconfined; therefore, movement of the ground water is in direct response to gravity. The direction of regional ground water flow in the Davisville area is west to east, from the highlands towards Narragansett Bay. For small localized areas, the direction of ground water flow will be to the nearest downhill discharge area.

Ground water quality beneath the Davisville area is classified by the RIDEM as GAA-NA (Sites 08, 10, and 12) and GB (Sites 02, 03, 05, 06, 07, 09, 11, 13 and 14). GAA ground water is considered to be suitable for public drinking water use without treatment. Non-attainment areas (NA) are those areas that have pollutant concentrations greater than ground water quality standards for the applicable classification; a goal of restoration to ground

water quality consistent with the standards is applicable to such areas. GB ground water is not suitable for public or private drinking water use. Areas were classified as GB because of known or presumed ground water degradation due to urbanization and/or identified waste disposal sites. Rhode Island regulations do not require cleanup to drinking water standards, but if RIDEM determines resultant impacts need to be addressed or if contaminant levels pose a risk or contaminants migrate off-site, the Department can require remediation. The need for cleanups are determined on a site-by-site basis.

The ground water quality of the Hunt Ground Water Reservoir is suitable for most purposes. It generally contains less than 70 ppm of dissolved solids and the pH is slightly acidic, with a range of 5.5 to 7.0. The principal anions in the ground water are bicarbonate, sulfate, chloride and nitrate, all usually less than 25 ppm. In the vicinity of Narragansett Bay, the chloride value may exceed 250 ppm, due to salt water intrusion. The principal cations are calcium, sodium, magnesium and potassium, each generally less than 10 ppm, resulting in soft water. Iron and manganese usually do not exceed drinking water standards (Rosenshein, Gonthiel and Allen, 1968).

1.4.3 Area Water Use

Available information (Personal Communication, Cohen, Smith, 1992) indicates that potable water in the Davisville area is supplied by either the North Kingstown Water Department or the Rhode Island Port Authority. No information was available on the number, type, or location of private water supply wells, although private wells have been identified in a residential area north of the base. A well survey is currently being conducted.

The North Kingstown Water Department supplies the non-military portion of Davisville and North Kingstown with water. This water is produced by a series

of ten ground water supply wells located in North Kingstown. The Kingstown Water Department (Personal Communication, Smith, 1992) indicated that all ten wells are actively used for water supply purposes. No plans presently exist to develop ground water supply wells or extend existing water mains in the vicinity of NCBC-Davisville.

The Rhode Island Port Authority (RIPA) supplies water on a wholesale basis to the Navy and some private users on Quonset Point (Personal Communication, Cohen, 1992). RIPA obtains its water from a series of three ground water supply wells located in the Hunt Ground Water Reservoir. No active ground water supply wells exist at NCBC-Davisville on Navy property (Personal Communication, Cohen, 1992).

The Kent County Water Authority, which supplies water to towns north of North Kingstown, also maintains a ground water production well in the Hunt Ground Water Reservoir.

The locations of the North Kingstown Water Department, RIPA, and Kent County Water Authority wells are shown in Figure 1-5.

1.4.4 Regional Hydrology

All of the investigated sites lie within the Potowomut-Wickford drainage basin. The basin is about 60 square miles in area and is divided into four smaller sub-basins (Figure 1-6). Camp Fogarty and West Davisville lie within the Potowomut River basin, and NCBC-Davisville lies within the Coastal River basin. All stream flow and river flow eventually discharges into Narragansett Bay (Figure 1-6). Surface water features in the immediate vicinity of NCBC-Davisville are indicated in Figure 1-7. During most of the year, a part of the stream flow consists of water discharged from detention storage in natural, as well as man-made impoundments. The remaining flow is from direct

runoff of precipitation and from base runoff consisting largely of ground water discharge. The ground water contributes close to 50 percent of the average annual stream flow.

Annual precipitation in the area has ranged from 24.8 to 66.2 inches with an average of 42.3 inches. The frequency of measurable precipitation events (0.01 inch or greater) averages once every 3 days and is evenly distributed throughout the year. The average snowfall is almost 40 inches and has varied from 11.3 to 75.6 inches. Roughly 30 percent of the precipitation actually recharges the ground water system; the other 70 percent runs off into streams or is lost through evapotranspiration (Hart, 1984a).

The surface water and ground water quality are similar since ground water contributes a major portion to stream flow. The principal anions are bicarbonate, sulfate, chloride, and nitrate. The principal cations are calcium, sodium, magnesium, and potassium. The pH ranges between 5.5 and 7.0. The iron concentrations in stream water vary from 0.03 to 3.7 ppm with the higher concentrations detected in Sandhill Brook, the lower reach of Hunt River, and the Potowomut River. Manganese concentrations range between less than 0.01 and 0.54 ppm (Rosenshein, Gonthiel, and Allen, 1968).

2.0 IDENTIFICATION OF POTENTIAL APPLICABLE OR RELEVANT AND APPROPRIATE REQUIREMENTS

The Comprehensive Environmental Response, Compensation, and Liability Act of 1980 (CERCLA), as amended by the Superfund Amendments and Reauthorization Act (SARA, 1986), and the NCP (1990) require that all remedial response actions attain or exceed applicable or relevant and appropriate requirements of Federal and more stringent promulgated requirements of State environmental statute(s). The NCP defines applicable requirements as "those cleanup standards, standards of control, other substantive environmental protection requirements or criteria, or limitations promulgated under environmental or state environmental facility siting law that specifically address a hazardous substance, pollutant, contaminant, remedial action, location, or other circumstances found at a CERCLA site." Relevant and appropriate requirements are defined in the NCP as "those cleanup standards, standards of control, and other substantive environmental protection requirements, criteria, or limitations promulgated under Federal or State law that, while not "applicable" to a hazardous substance, pollutant, contaminant, remedial action, location, or other circumstance at the CERCLA site, address problems or situations sufficiently similar to those encountered at the CERCLA site that their use is well suited to the particular site."

To-Be-Considered materials (TBCs) are non-promulgated advisories or guidance issued by federal or state government that are not legally binding and do not have the status of potential ARARs. However, in many circumstances TBCs may be considered along with ARARs in determining the necessary level of cleanup for protection of health or the environment.

Current EPA CERCLA guidance calls for a preliminary identification of potential ARARs during the RI scoping phase to assist in initial identification of remedial alternatives. Early identification also

facilitates communications with support agencies to evaluate ARARs, and may help planning of field activities. Because of the iterative nature of the RI/FS process, ARAR identification continues throughout the RI/FS as better understanding is gained of the site conditions, site contaminants, and remedial action alternatives. Findings of the Phase I RI aided in the selection of ARARs as presented in Volume II of the Phase II RI/FS Work Plan (TRC, 1992). This section revisits the information provided in that report, updating it on the basis of the specific sites addressed herein as well as on the basis of evolving regulatory requirements.

ARARs may be categorized as: 1) chemical-specific requirements, which may define acceptable exposure levels and, therefore, be used in establishing preliminary cleanup goals; 2) location-specific requirements, which may set restrictions on activities within specific locations such as floodplains or wetlands; and 3) performance, design or other action-specific requirements, which may set controls or restrictions for particular treatment and disposal activities related to the management of hazardous wastes. The documents "CERCLA Compliance With Other Laws Manual" (U.S. EPA, 1988b), and "CERCLA Compliance with Other Laws Manual: Part II. Clean Air Act and Other Environmental Statutes and State Requirements" (U.S. EPA, 1989b), contain detailed information on identifying and complying with ARARs.

Preliminary lists of Federal and State of Rhode Island ARARs have been compiled for NCBC-Davisville, as presented in Tables 2-1 through 2-6. Refinement of ARARs will continue throughout the RI/FS process. In the Detailed Analysis of Alternatives, individual remedial alternatives associated with each group of sites will be evaluated in detail to determine their compliance with ARARs/TBCs and the potential impacts of ARARs/TBCs on their implementation. Upon definition of the specific remedial components included

in each alternative, applicable action-specific ARARs/TBCs will be further identified.

2.1 Potential Chemical-Specific ARARs/TBCs

2.1.1 Potential Federal Chemical-Specific ARARs/TBCs

Potential federal chemical-specific ARARS and TBC criteria are presented in Table 2-1. Ground water at NCBC-Davisville is not a current source of drinking water, but is classified as GB at Sites 05, 06, 13 and 14, and as GAA Non-attainment at Sites 08, 10 and 12. Therefore, Maximum Contaminant Levels (MCLs) and Maximum Contaminant Level Goals (MCLGs), published under the Safe Drinking Water Act (40 CFR 141.11-.16, 141.50-.52 and 141.60-.63), as well as the Ground Water Protection Standards Alternate Concentration Limits promulgated under the Resource Conservation and Recovery Act (RCRA) are either applicable or may be relevant and appropriate in assessing potential risks associated with ground water ingestion. The U.S. EPA Risk Reference Doses (RfDs), Lifetime Health Advisories, and the U.S. EPA Human Health Assessment Group Cancer Slope Factors (CSFs) will represent TBC criteria.

Ambient Water Quality Criteria (AWQC) and Effluent Discharge Limitations, both promulgated under the Clean Water Act, represent potential chemical-specific ARARs for alternatives which involve discharges to surface waters.

The Toxic Substances Control Act provides PCB cleanup levels for solid surfaces and soils where spills occurred after May 4, 1987. These levels may be relevant and appropriate for NCBC-Davisville sites. In addition, the Interim Guidance on Establishing Soil Lead Cleanup Levels at Superfund Sites (OSWER Directive 9355.4-02) will represent TBC criteria for lead in soils.

Sections of the Clean Air Act which establish maximum concentrations for particulates and fugitive dust emissions, emissions limitations for new

sources, and emissions limitations for hazardous air pollutants, are considered potential chemical-specific ARARs for remedial alternatives which impact ambient air.

2.1.2 Potential Rhode Island Chemical-Specific ARARs/TBCs

Potential Rhode Island chemical-specific ARARs and TBC criteria are presented in Table 2-2. Potential chemical-specific ARARs for ground water remediation include the Rhode Island Public Drinking Water Regulations (RI Ground Water Protection Act, RIGL, Title 46, Chapter 13). The Rhode Island Water Quality Standards, under the RI Water Pollution Control Law (RIGL, Title 46, Chapter 12), will apply to remedial alternatives which involve discharges to surface waters. The Rhode Island Department of Environmental Management (RIDEM) has historically applied a non-promulgated cleanup standard for PCB contamination of 1 part per million (ppm). In September 1992, proposed Rules and Regulations for the Investigation and Remediation of Hazardous Materials Releases (Site Remediation Regulations) were issued for public comment. proposed regulations require the investigation and/or remediation of PCBs detected at concentrations greater than 10 ppm in any environmental media and/or greater than 2 micrograms/100 cm² on any surface and will be considered TBCs until promulgated. RIDEM and the Rhode Island Department of Health-Risk Assessment consider a safe lead level in soil (total) as under 300 ppm (per RIDEM comments on the draft ISA).

The RI Clean Air Act (RI Title 23, Chapter 23) establishes maximum ambient levels for criteria pollutants under the Air Pollution Control Regulation Standards. These levels constitute potential chemical-specific ARARs for remedial alternatives which emit pollutants into the air.

2.2 Potential Location-Specific ARARs/TBCs

A site's location is a fundamental determinant of its impact on human health and the environment. Location-specific ARARs are restrictions placed on the concentrations of hazardous substances or the conduct of activities solely because they are in a specific location (U.S. EPA, 1988b).

The various NCBC-Davisville sites are situated in a areas with a diversity of land uses. The following sections indicate the various potential federal and state location-specific ARARs or TBCs applicable to these sites. Since none of the four groups of sites addressed herein are coastal sites, coastal zone and harbor protection regulations are not discussed.

2.2.1 Potential Federal Location-Specific ARARs/TBCs

Federal location-specific ARARs and TBCs potentially applicable to the NCBC-Davisville sites are presented in Table 2-3. Wetland regulations, including Executive Order 11990, Wetlands Construction and Management Procedures, and the Clean Water Act: Prohibition of Wetland Filling will apply to any remedial action which impacts on- or off-site wetlands.

Floodplain regulations, including Executive Order 11988 and the Flood Disaster Protection Act of 1973, both of which regulate activities conducted within floodplains, and the National Flood Insurance Act of 1968, which provides insurance for disaster relief and establishes flood control methods, are potential ARARs for remedial activities conducted at those Davisville sites which may be located within the 100-year floodplain zone.

Potential ARARs associated with the presence of rivers consist of the Wild and Scenic Rivers Act, which regulates activities in the vicinity of so designated rivers, and the Fish and Wildlife Coordination Act, which prevents the modification of a stream or river that affects fish or wildlife. These regulations are potential ARARs for sites located near streams and rivers.

The Endangered Species Act of 1973, which restricts activities in areas inhabited by registered endangered species, is a potential ARAR, especially for sites surrounded by wetlands which may sustain endangered or threatened wildlife species.

The National Historic Preservation Act of 1966 and the Archeological and Historic Preservation Act of 1974 are potential ARARs for remedial actions which may impact historic properties or sites of archeological significance.

To determine the potential applicability of the Farmland Protection Policy Act, the U.S. Department of Agriculture Important Farmlands Map for Kent County was reviewed. This map, developed on the basis of soil survey information, indicates that limited areas designated as Prime Farmland and Additional Farmland of Statewide Importance are located in the general vicinity of the NCBC-Davisville facility. Therefore, farmland protection regulations are potential ARARs for remedial actions which impact off-site farmland areas.

2.2.2 Potential State Location-Specific ARARs/TBCs

State location-specific ARARs/TBCs potentially applicable to the NCBC-Davisville sites are presented in Table 2-4. Rhode Island defines and establishes provisions for the protection of swamps, marshes and other freshwater wetlands in the state under the Rhode Island Wetlands Laws, which are potential ARARs if remedial actions impact a wetland area.

Ground water regulations under the Rhode Island Ground Water Protection Act may be potential ARARs for certain Davisville sites (particularly Sites 08, 10 and 12) which are located over ground water which is classified by the State as GAA Non-attainment. For other the Davisville sites, which are located in areas of existing degradation where the ground water is classified as GB, further degradation of ground water quality is not allowed.

The Rhode Island Water Pollution Control Law provides for the protection of state surface waters and will be a potential ARAR for any site where surface water quality may be impacted.

2.3 Potential Action-Specific ARARs/TBCs

Based on the identification of contaminants in various on-site media at the Davisville sites, remediation activities may be required and numerous state and federal requirements could apply to the implementation of these activities. Potential action-specific ARARs/TBCs cannot be well-defined until remedial alternatives are developed and response actions defined. A discussion of potential action-specific ARARs/TBCs pertaining to such general response actions as no action, institutional controls, diversion, containment, material removal, ground water collection, treatment, decontamination and disposal is provided in the following sections.

2.3.1 Potential Federal Action-Specific ARARs/TBCs

Numerous federally promulgated action-specific ARARs and TBC criteria could potentially affect the implementation of remedial measures. The primary federal regulatory requirements potentially applicable to remediation of the Davisville sites appear in Table 2-5.

The primary federal administrative requirements which will guide remediation are those established under the following:

- Resource Conservation and Recovery Act (applicable to hazardous waste treatment, storage and disposal);
- Toxic Substances Control Act (applicable to handling of PCB-contaminated materials);
- Safe Drinking Water Act (applicable to discharges to ground water);
- Clean Water Act (applicable to discharges to surface water and publicly owned treatment works);

- Fish and Wildlife Coordination Act (applicable to modifications of water bodies);
- Clean Air Act (applicable to discharges to the atmosphere);
- Hazardous Materials Transportation Act (applicable to off-site shipment of hazardous wastes);
- Federal Water Pollution Control Act (applicable to discharges to Narragansett Bay); and
- Occupational Safety and Health Act (applicable to personnel involved in hazardous activities).

2.3.2 Potential State Action-Specific ARARs/TBCs

The State of Rhode Island has promulgated regulations similar to those of the federal government. The potential state action-specific ARARs which may be applicable to the remediation of the various NCBC-Davisville sites are presented in Table 2-6.

The RI Water Pollution Control Act is a potential ARAR which establishes general requirements and effluent limits for discharge of treated waters to surface waters, ground waters (including discharge to a sources of public drinking water supplies), or a POTW. This act also establishes ground water classifications and maximum contaminant levels for each classification as well as establishing cleanup levels. Any activities which may impact coastal areas undergo review by the RI Coastal Resource Management Council (CRMC).

The RI Hazardous Waste Management Act of 1978 is a potential ARAR for alternatives which involve the on- or off-site management of hazardous wastes. Proposed Rules and Regulations for the Investigation and Remediation of Hazardous Material Releases present requirements for the design and operation of remedial systems. The RI Hazardous Substance Community Right to Know Act establishes rules for the public's right-to-know concerning hazardous waste storage and transportation. The RI Refuse Disposal Law is the basis for rules and regulations governing solid waste management.

Alternatives involving closure of on-site underground storage tanks are regulated under the RI Underground Storage Tanks Act.

The RI Clean Air Act sets emissions limitations for particulates and visible air contaminants. The Clean Air Act is a potential ARAR for alternatives involving remedial actions which impact ambient air.

3.0 GROUP I SITES - SITE 05 - TRANSFORMER OIL DISPOSAL AREA, SITE 06 - SOLVENT DISPOSAL AREA, AND SITE 13 - DISPOSAL AREA NORTHWEST

3.1 Introduction

Group I sites consist of Site 05 - Transformer Oil Disposal Area, Site 06 - Solvent Disposal Area, and Site 13 - Disposal Area Northwest. These sites are physically situated in close proximity to each other. The relative locations of Sites 05 and 06 are presented in Figure 3-1, while the relative locations of Sites 06 and 13 are provided in Figure 3-2. The relative locations of all three sites were previously presented in Figure 1-3. following sections provide background information and descriptions for each of the sites, followed by a summary of remedial response objectives and cleanup criteria, general identification response actions, and screening of technologies and process options, remedial alternative development, and preliminary screening of remedial alternatives.

3.2 Site 05 - Transformer Oil Disposal Area

3.2.1 Site Location and Description

Site 05 is located east of Building 37 and adjacent to Camp Avenue. The approximately 1,500 square foot (Hart, 1984a) disposal area is in the vicinity of an overgrown dirt road, outside the NCBC fence line, but within Navy property. The area east of the dirt road becomes wooded with small trees. Although the site itself is relatively flat, local topography slopes upward to the east. A site map is provided in Figure 3-3.

3.2.2 Site History Overview

In 1968 or 1969, approximately 30 gallons of oil containing PCBs at unknown concentrations were reportedly drained from a transformer and poured onto the ground at the Site 05 location.

3.2.3 Geology, Hydrogeology and Hydrology

No subsurface borings have been drilled nor have any monitoring wells been installed at Site 05. The glacially-derived soils at Site 05 are expected to consist of fine to coarse sand with some silt overlying fine to coarse sand with a trace of silt which then grades into silt and fine sand (Schafer, 1961). The depth to bedrock should range from 10 to 30 feet below the ground surface (Johnson and Marks, 1959). Based on data from Site 06 (1,400 feet to the northwest) and existing topographical conditions, the water table is expected to be 4 to 6 feet below the ground surface, with flow to the northeast, toward Hall Creek (see Figure 1-7).

3.2.4 Summary of Contamination

A composite soil sample (6 inches deep) was obtained from Site 05 by Navy personnel on October 23, 1984 and was analyzed for PCBs. Laboratory analysis reported the sample to contain 6 mg/kg (parts per million or ppm) of PCBs.

During the Confirmation Study, 16 additional soil samples were collected from a depth of 6 to 12 inches at Site 05 by TRC and analyzed for PCBs. There were no PCBs detected in any of the samples. However, chemicals similar in composition to PCBs, namely DDT, DDE, and DDD, were detected and quantified during the QA/QC check at one sample location in the central portion of the site. A second round of composite surface soil samples was collected in March 1986 to verify the results of previous testing. Again, no PCBs were detected, but DDE, DDD and DDT were identified. DDT was detected at levels up to 16 ppm.

The RI investigation consisted of the collection of ten surface soil samples and eight subsurface soil samples (depths of 2 to 4 feet) along a 20 foot grid at Site 05. RI sample locations are provided in Figure 3-4. Low concentrations (1 to 140 parts per billion or ppb) of acetone, chloroform,

carbon tetrachloride and methylene chloride were detected sporadically across the site in both surface and subsurface soils. Concentrations of individual PAH compounds of up to 4,300 ppb were detected in surface soil samples collected from the site. PAHs were detected in only one subsurface soil sample, collected at the same location (S5-10) where the greatest surficial concentration of PAHs was detected. Pesticides, including beta-BHC, 4,4'-DDT, 4,4'-DDE, and 4,4'-DDD were detected in eight surface soil samples and one subsurface soil sample at concentrations ranging from 22 ppb to 3,300 ppb. Only one soil sample collected during the RI, S5-5, contained detectable levels of PCBs (330 ppb). Arsenic, beryllium, chromium, copper, nickel and zinc were detected at each surface soil sample location. Lead was also detected in all ten of the surface soil samples at concentrations ranging from 30.1 ppm to 303 ppm, and in all eight subsurface soil samples at concentrations ranging from 6.9 ppm to 10.6 ppm. The greatest concentrations of metals were detected at location S5-4. Metals concentrations decreased with the depth of the sample.

3.2.5 Summary of Contaminant Fate and Transport

A contaminant fate and transport analysis was conducted as part of the Phase I RI. That analysis is summarized below. For more information, refer to the Phase I RI Report (TRC, 1991).

The primary contaminant migration pathways at Site 05 include surficial erosion or leaching of contaminants through the soil column to the ground water. Site 05 is relatively flat, and wooded to the east of the dirt road. The direction of ground water flow in the vicinity of Site 05 is assumed to be toward Hall Creek or Davol Pond. Hall Creek is approximately 500 feet east-northeast of Site 05 and is likely a gaining stream (sink) most of the

year. Heavy precipitation/snow melt during spring may reverse ground water flow, causing Hall Creek to recharge and become a losing stream. The regional ground water flow direction is to the northeast, toward Davol Pond (approximately 1,500 feet from Site 05).

Volatile Organic Compounds

Volatile organic compounds such as acetone, chloroform, carbon tetrachloride, and methylene chloride were detected infrequently in surface and subsurface soils at low concentrations (less than 140 ppb). These VOCs are highly volatile, soluble in water, and unlikely to be significantly sorbed to soils. The potential for the VOCs to be leached to the ground water is considered to be minimal based on the generally low contaminant concentrations and their potential for volatilization. Although TCLP analysis detected the presence of ethylbenzene, toluene, styrene, acetone, 2-butanone and xylene, it is not considered likely that significant concentrations will migrate to the ground water.

Polycyclic Aromatic Hydrocarbons

Polycyclic aromatic hydrocarbons (PAHs) were commonly detected in surface soil samples, but generally were not present in subsurface soils. Several PAHs were detected in surface soil samples, with the most frequently detected PAHs being benzo(a)anthracene, chrysene, fluoranthene, phenanthrene and pyrene. Of these PAHs, benzo(a)anthracene is classified as a probable human carcinogen, with limited evidence suggesting the carcinogenicity of chrysene. Given that the detected PAHs have moderate to high tendencies to sorb to soils (as indicated by their high organic carbon partition coefficients [Koc values]), it is expected that the PAHs will generally remain bound to soils.

The general absence of PAHs in subsurface soils supports this premise. PAHs were not identified as a result of the TCLP analysis.

Other Semi-Volatile Organic Compounds

Other semi-volatile organic compounds (SVOCs) were detected in surface soils at Site 05, including bis(2-ethylhexyl)phthalate (BEHP) and benzoic acid. BEHP has a low tendency to volatilize from soil. It is relatively insoluble in water and thus is unlikely to be leached from soils by precipitation and transported to ground water. With an octanol/water partition coefficient (log $K_{\rm OW}$) in excess of 4, BEHP tends to sorb to soil material. Benzoic acid can potentially migrate from soils to ground water due to its high solubility in water. Neither BEHP nor benzoic acid was identified in subsurface soil samples obtained at Site 05; therefore, it is considered unlikely that either has migrated to the ground water.

Pesticides/PCBs

Pesticides (beta-BHC, 4,4'-DDT, 4,4'-DDE, and 4,4'-DDD) were identified in eight surface soil samples; 4,4'-DDT was also identified in one subsurface soil sample. Given that the detected pesticides have a low to moderate tendency to volatilize from soil, low water solubilities and moderate to high K_{OC} values, it is likely that they will remain bound to soils and will not be transported to ground water. Although the pesticides could be transported with suspended sediments via surface water runoff, the topography of Site 05 is relatively flat and wooded or grass-covered; therefore migration off-site is not considered likely.

PCB-1248 was detected in one surface soil sample and was not detected in any subsurface soil samples. PCBs have a tendency to sorb to soils and have

low water solubilities; therefore, PCBs will tend to remain bound to soils and will not tend to be transported to ground water. Similar to pesticides, PCBs could be transported with suspended sediments via surface water runoff, but due to topography and surficial grass at Site 05, it is not considered likely that PCBs will migrate off-site.

Metals

Elevated concentrations (i.e., greater than three times surrounding concentrations) of arsenic, chromium, copper, and lead were identified at an isolated location (S5-4), confined to the immediate surface. Many metals have an affinity for soils (particularly clay particles and organic matter in soils) which reduce their mobility. TCLP results indicate that the metals are leachable under the acidic conditions of the TCLP analysis. TCLP metals concentrations are comparable to total metals concentrations at most NCBC-Davisville sites for which ground water data are available (no background levels were defined in the Phase I RI; background sampling will be conducted in the Phase II RI).

3.2.6 Summary of Human Health and Environmental Risk

Total current and future estimated excess lifetime cancer risks, as presented in the Phase I RI Report (TRC, 1991), associated with surface soil and subsurface soil exposure scenarios at Site 05 ranged from 2.28 x 10^{-7} to 7.5 x 10^{-5} . These risk values are driven by arsenic, beryllium, and PAHs. PCBs (PCB-1248 was detected in only one sample) were estimated to pose a worst-case cancer risk of 10^{-7} , which is below the point-of-departure risk level of 10^{-6} . Hazard indices for non-carcinogenic effects due to soil exposures were all less than one. No ground water sampling was conducted as part of the RI at Site 05.

The ecological risk assessment presented in the Phase I RI Report (TRC, 1991) concluded that no species of concern are likely to inhabit the immediate vicinity of Site 05. Risks to terrestrial receptors could be significant under a theoretical, worst-case scenario, based on detected metals levels at surface soil sample location S5-4. Ecological risks will be quantified in more detail through additional sampling and ecological characterization in the Phase II RI.

3.3 <u>Site 06 - Solvent Disposal Area</u>

3.3.1 Site Location and Description

Site 06 is a flat grassy area located between Buildings 67 and 38, covering roughly a quarter of an acre. It is bounded to the east by a fence, and to the west by a paved parking lot. Subsurface utilities such as a water main, storm drain, leach field, and a septic tank are present at Site 06. A site map is provided in Figure 3-5. Site 06 is located approximately 1,400 feet northwest of Site 05.

3.3.2 Site History Overview

Site 06 was reportedly used from 1970 to 1972 for the disposal of waste chlorinated hydrocarbon solvents. Personnel from the Refrigeration Mechanics Section of the Public Works Department reportedly drained over a dozen 5-gallon cans of various liquid wastes in this area, about once every three weeks, for an estimated total disposal volume of 1,750 gallons. Site 06 was a sandy area during the time of these disposal practices.

3.3.3 Geology, Hydrogeology and Hydrology

The stratigraphy of Site 06 indicates primarily fluvioglacial (outwash) deposits. Strata consist of a coarse sand and gravel layer 2 to 5 feet in

thickness, overlying a sequence of sand and silt with gravel, which grades coarser with depth. The estimated depth to bedrock ranges between 20 and 40 feet below the ground surface (Johnson and Marks, 1959).

An aquifer characteristic test was conducted at Site 06. Transmissivity and hydraulic conductivity were determined to be 116 gpd/ft and 21 gpd/sf, respectively. The depth to the water table is between 4 and 6 feet. The water table potentiometric surface is relatively flat across the site, with only 0.32 feet of elevation difference between the wells. When combined with water table information from Site 13 monitoring wells, located southwest of Site 06, a potential northern component of flow becomes evident (see Figure 3-6). However, additional water table information is required to confirm this flow direction. Given the shallow nature of the water table, buried utilities such as the storm drain, leach field, and septic tank could alter the flow locally by providing either preferential pathways or barriers to the northern component of flow in the shallow water table aquifer.

3.3.4 Summary of Contamination

Verification Step field investigations conducted at Site 06 included geophysical and OVA surveys, near-surface soil sampling, and ground water Soil sample analysis indicated the presence of petroleum-based hydrocarbons at a concentration of 124 ppm and volatile organics at about 5 ppm. Neither of these components was detected in the ground water sample. Field measurements indicated ground water is slightly acidic. conductance measurements indicated a moderately clean water quality. A second round of ground water and soil sampling identified no detectable volatile contaminants organic contamination and negligible levels of other 0.040 ppm, bis(2-ethylhexyl)phthalate at 0.051 (fluoranthene at

benzo(k)fluoranthene at 0.087 ppm and inorganics at concentrations ranging from non-detectable to 51 ppm [lead] and 54 ppm [zinc]). Volatile organics were not detected in the ground water sample.

The Phase I RI included a soil gas survey, collections of 3 surface and 3 subsurface soil samples (2 samples from each of 3 boring locations), as well as the installation and sampling of two ground water monitoring wells and the sampling of an existing on-site well (see Figure 3-7 for sample locations). Low concentrations of VOCs such as chloroform, acetone, and 2-butanone (1 ppb to 70 ppb) were detected in surface and subsurface soil samples. No VOCs were detected in ground water samples. The majority of semi-volatile organic compounds detected in soil samples consisted of compounds classified as PAHs. Individual PAH concentrations of up to 140 ppb were detected in surface soil samples. Although PAHs occurred primarily in surface soils, 2-methylnaphthalene, naphthalene, and dibenzofuran were present subsurface soil sample at concentrations of 1,600 ppb, 630 ppb, and 66 ppb, respectively. 2-Methylnaphthalene and naphthalene were also detected in one TCLP sample at concentrations of 19 ppb and 21 ppb, respectively. Bis(2ethylhexyl)phthalate (BEHP), a semi-volatile organic, was detected in the surface soil samples and one subsurface soil sample. Benzoic acid was detected at 26 ppb in one TCLP sample analysis. No semi-volatile organics were detected in ground water samples. No pesticides/PCBs were detected in soil samples, ground water samples or in the TCLP analysis of soil samples. Arsenic, chromium, lead, and zinc were common to surface soils and levels diminished with depth. Beryllium, copper, and nickel were present in ground water in addition to those metals identified in soils. Lead concentrations ranging from 5 ppm to 43.9 ppm were identified in surface and subsurface soils; lead levels in the ground water ranged as high as 63.2 ppb.

3.3.5 Summary of Contaminant Fate and Transport

A contaminant fate and transport analysis was conducted as part of the Phase I RI. That analysis is summarized below. For more information, refer to the Phase I RI Report (TRC, 1991).

The primary contaminant migration pathways at Site 06 include surficial erosion or leaching of contaminants through the soil to the ground water. Site 06 is relatively flat and grass-covered. It is located approximately 1,500 feet southwest of Davol Pond. Ground water flow direction is considered to be northeasterly toward Davol Pond at an estimated rate of about 3 ft/day.

Volatile Organic Compounds

Acetone and chloroform were the only VOCs detected frequently in soils at Site 06; 2-butanone was detected only in one subsurface soil sample. No VOCs were detected in the ground water. Acetone and 2-butanone are moderately volatile, whereas chloroform has a high tendency for volatilization from soils. All three VOCs have high water solubilities but would not be significantly sorbed to soil material, based on K_{OC} values. Migration of VOCs to ground water is not considered to be a major concern based on the low soil concentrations and lack of VOCs in the ground water samples.

Polycyclic Aromatic Hydrocarbons

The PAHs detected at Site 06 can be classified into two groups based upon their physical and chemical properties: those compounds which are similar to naphthalene and those which are similar to benzo(a)pyrene. Naphthalene has a moderately high tendency to volatilize from soil whereas benzo(a)pyrene has a low volatility. Although PAHs generally have low water solubilities, naphthalene-related PAHs are significantly more soluble than benzo(a)pyrene-

related compounds. Naphthalene and related compounds have higher tendencies than benzo(a)pyrene to leach from soil and be transported to ground water. Based on organic carbon partition coefficients, naphthalene-related compounds are moderately sorbed to soils, whereas benzo(a)pyrene-related PAHs are highly sorbed to soils. While TCLP results indicated the presence of 2-methylnaphthalene and naphthalene, no PAHs were detected in ground water samples, thereby supporting the conclusion that the detected PAHs at Site 06 are tending to sorb to soil materials.

Other Semi-Volatile Organic Compounds

BEHP, a semi-volatile organic compound, was detected in surface and subsurface soils, but was not identified in ground water. BEHP has a low tendency to volatilize from soil. It is relatively insoluble in water and thus is unlikely to be leached from soils by precipitation and transported to ground water. Based on its octanol/water partition coefficient, BEHP tends to sorb to soil material. The presence of BEHP in soils, and its absence in ground water, supports the physical and chemical characteristics that suggest BEHP will be bound to soils and will not be transported to ground water.

Metals

Arsenic, chromium, lead, and zinc were common to each of the surface soil sampling locations with concentrations decreasing with depth in the subsurface soil samples. Comparison of total metals concentrations in ground water samples to TCLP soil extraction results shows the presence of similar metals, the exceptions being that chromium and nickel were not leached by TCLP. Concentrations were similar between total ground water metals and soil extract. Metals extraction by TCLP is performed in an acidic environment to

simulate very favorable leaching conditions. The soils at Site 06 have a slightly acidic quality (pH ranging from 5.8 to 8.2), therefore on-site conditions are favorable to leaching. Thus, TCLP extract concentrations may be representative of the potential for metals to leach at Site 06 and, based on the detected metals levels in the ground water samples, metals may be leaching into the ground water from site soils. However, confirmation of this conclusion will require the characterization of background ground water quality, as to be conducted in the Phase II site investigations.

3.3.6 Summary of Human Health and Environmental Risk

The total excess cancer risks, as presented in the Phase I RI Report (TRC, 1991), associated with current and future soil exposures range from 3.93 x 10^{-8} (future) to 7.99 x 10^{-7} (current), with PAHs driving these risk values. Worst-case ground water ingestion risks were on the order of 1.10×10^{-3} . The carcinogens which contribute the most to this risk value are arsenic and beryllium. All estimated hazard index ratios were less than one except for the worst-case childhood ingestion of ground water scenario, where the hazard index value of 1.90 is driven by manganese.

The ecological risk assessment presented in the Phase I RI Report (TRC, 1991) concluded that, due to the level of development at and surrounding Site 06, terrestrial organisms are not expected to be exposed to or adversely effected by contamination. Further characterization of ground water flow regimes and surface water quality, as will be conducted during the Phase II RI, is required to assess potential risks to ground water/surface water receptors. The Phase II RI will also include additional ecological characterization.

3.4 Site 13 - Disposal Area Northwest

3.4.1 Site Location and Description

Site 13 is approximately 6 acres in size and consists of a large grassy field bounded on three sides by paved roads. There are three catch basins located in this area. A site map is provided in Figure 3-8. Site 13 is located approximately 1,500 feet west of Site 05, and 1,100 feet south-southwest of Site 06.

3.4.2 Site History Overview

From 1945 to 1955, the Construction and Equipment Department was located in Buildings W-3, W-4, and T-1. Overhaul and repair activities were conducted in these buildings, vehicles were stored in fields to the north and west, and drums of oils, thinners and solvents were stored adjacent to the buildings. Approximately 300 gallons of waste oils per month were reportedly spread on the fields northwest of the three buildings (Hart, 1984a).

3.4.3 Geology, Hydrogeology and Hydrology

The geologic conditions of Site 13 indicate a typical sequence of glacial outwash deposits similar to that of Site 06. The strata are well-sorted fine-grained sands with some silt, alternating with somewhat coarser sands. Bedding and laminae were evident in some strata. A thin layer of peat was present just below the ground surface in one of the borings drilled during the RI. The probable depth to bedrock ranges between 40 and 60 feet below the ground surface (Johnson and Marks, 1959).

The water table below the site, as defined by four existing monitoring wells, is relatively shallow and follows surface topography, ranging from 4 to 5 feet below ground surface. Triangulations of ground water data revealed a

north-northeast flow component (see Figure 3-6). The hydraulic gradient across the site approaches 0.

3.4.4 Summary of Contamination

The Verification Step field program consisted of OVA screening, a geophysical survey, collection of a composite surface soil sample, a soil boring, and ground water sampling. During a second field mobilization, a second surface soil sample was collected for analysis. The composite surface soil sample from the first round of sampling contained 193 ppm of petroleum hydrocarbons and 36 ppm of total volatile organics, although most of the volatile fraction was acetone, which could be a remnant from the decontamination procedure. No volatile organics were detected in the ground water, although about 0.5 ppm of petroleum hydrocarbons were detected. The measurement of pH indicated ground water is slightly acidic and specific conductance indicated a moderate water quality. Very low levels of organic contaminants were found in the second round soil sample.

The Phase I RI included a soil gas survey, collection and analysis of 13 surface soil samples (including 3 sediment samples from on-site catch basins) and 5 subsurface soil samples, drilling of 6 soil borings and associated subsurface soil sample collection, and the installation and sampling of 3 monitoring wells as well as sampling of an existing monitoring well (see Figure 3-9 for locations).

Four VOCs were detected in soils at low concentrations (1 - 29 ppb): acetone, chloroform, 1,1,1-trichloroethane (TCA), and xylenes. Semi-volatile organic compounds (SVOCs) were infrequently detected in the soils at Site 13 (only soil boring samples were analyzed for SVOCs). Subsurface soils contained SVOC compounds such as benzoic acid, benzo(a)anthracene,

benzo(b)fluoranthene, benzo(k)fluoranthene, bis(2-ethylhexyl)phthalate (BEHP), chrysene, fluoranthene, 2-methylnaphthalene, phenanthrene, and pyrene. Ground water was found to contain BEHP, 2-methylnaphthalene and naphthalene. the exception of benzoic acid and BEHP, these compounds are classified as PAHs. PCBs such as PCB-1260, PCB-1254, and PCB-1248 were detected in catch basin sediment samples at concentrations ranging from 1,300 to 6,500 ppb. High levels of PCBs (greater than 1 ppm) were also detected in surface soil samples collected from areas of surface staining. Additionally, the pesticide 4,4'-DDD was identified in one of the catch basin sediment samples. pesticides or PCBs were detected in ground water samples. Only soil boring and ground water samples were analyzed for inorganics. Arsenic, chromium, and copper were detected at all surface and subsurface soil boring sampling locations. Lead was also detected at all of the surface and subsurface soil boring sample locations at concentrations ranging from 2.5 ppm to 64.1 ppm. Chromium and zinc were the predominant metals detected in ground water at Site 13, although numerous other inorganics, including lead, were detected in the ground water samples. Lead concentrations identified in ground water samples ranged from 14 ppb to 158.5 ppb.

3.4.5 Summary of Contaminant Fate and Transport

A contaminant fate and transport analysis was conducted as part of the Phase I RI. That analysis is summarized below. For more information, refer to the Phase I RI Report (TRC, 1991).

The primary contaminant migration pathways at Site 13 include surficial erosion, transport via on-site storm sewers, or leaching of contaminants through the soil column to the ground water. Site 13 is relatively flat and sparsely vegetated, with several catch basins on-site. Site 13 is located

approximately 2,500 feet southwest of Davol Pond. Ground water flow direction is northeasterly toward Davol Pond. A negligible hydraulic gradient probably results in limited subsurface flow. The presence of the storm drains could play a role in intercepting ground water and any associated contamination.

Volatile Organic Compounds

Laboratory analyses did not indicate the presence of significant volatile organic contamination in an area identified as a "hotspot" by the soil gas Low concentrations of chloroform, 1,1,1-trichloroethane (TCA), acetone, and xylenes were identified in surface soils of Site 13. Of these VOC's, only acetone was identified in subsurface soils. In ground water, trace concentrations (1 to 2 ppb) of 1,2-dichloroethane and xylenes were detected. While acetone and xylenes are moderately volatile, chloroform and TCA have high tendencies to volatilize from soil. With the exception of xylenes which have moderate water solubilities, the VOCs have high water solubilities, and therefore have a tendency to be leached by precipitation and transported to ground water. Based on the organic carbon partition coefficients, acetone, chloroform, and TCA are not likely to be significantly sorbed to soil material. It is expected that the absence of chloroform and TCA in subsurface soils and ground water and their tendency to volatilize indicate that these compounds have not migrated to ground 1,2-Dichloroethane (a degradation product of TCA, and more mobile than TCA) was, however, detected in ground water at a low concentration (2 ppb). installation and sampling of deep wells during Phase II site investigations will indicate if chlorinated hydrocarbons are present in the deeper portions of the aquifer. Acetone is significantly more mobile in soils than chloroform or TCA, as evidenced by its presence in subsurface soils. The lack of acetone

in ground water samples may be due to the low soil concentrations. Xylenes, which have a moderate affinity for soils, were detected at low concentrations (1 ppb) in both a single soil sample and a single ground water sample.

Polycyclic Aromatic Hydrocarbons

As many as eight individual PAHs were detected in subsurface soils, but very few were identified in ground water at Site 13. PAHs detected at Site 13 classified either as 2-methylnaphthalene-related compounds or can be fluoranthene-related compounds. 2-Methylnaphthalene-related PAHs have a high tendency to volatilize from the soil, whereas fluoranthene-related PAHs have low volatilities. Although PAHs generally have low water solubilities, 2-methylnaphthalene-related PAHs are significantly more soluble and have a higher tendency to leach from soil than fluoranthene-related PAHs. Based on organic carbon partition coefficients, 2-methylnaphthalene-related compounds are moderately sorbed to soils, whereas fluoranthene-related compounds are highly sorbed to soils. Only the most mobile PAH compounds (naphthalene and 2-methylnaphthalene) were detected in ground water. trace concentrations (up to 5 ppb) detected in the ground water are not expected to increase on the basis of the relative absence of these compounds in the soil samples.

Other Semi-Volatile Organic Compounds

Other semi-volatile organic compounds (SVOCs) detected in surface and subsurface soils at Site 13 include benzoic acid and bis(2-ethylhexyl)-phthalate (BEHP). Ground water was also found to contain BEHP. Benzoic acid can potentially migrate from soils to ground water due to its high solubility in water. Its absence in ground water samples may be attributable to the

relatively low levels (71 to 590 ppb) at which it was detected in soils. BEHP has a low tendency to volatilize from soil, is relatively insoluble in water and is highly sorbed to soil material; therefore it is unlikely for BEHP to be leached from soils by precipitation and transported to ground water. BEHP is considered a common laboratory contaminant and is widespread in the environment (ATSDR, 1989). Since only trace levels were detected in both soils and ground water, and BEHP has a low water solubility and a high affinity for soils, it is expected that ground water concentrations will not significantly increase over time.

Pesticides/PCBs

PCBs such as PCB-1260, PCB-1254, and PCB-1248 were detected in catch basin sediment samples. High levels of PCBs (1,100 ppb to 1.2%) were also detected in surface soil samples collected from areas of surface staining. PCBs have high tendencies to volatilize from soil, low propensities to be leached by precipitation and transported to ground water, and high affinities for soil; therefore, PCBs will tend to remain bound to soils and will not tend to be transported to ground water at Site 13. These compounds have the potential to be transported with suspended sediments via surface water runoff. The topography of Site 13 is relatively flat, however, and PCBs were only identified in central areas of the site, limiting the potential for off-site transport of contaminated surface soils. The on-site catch basin provides a preferential pathway of PCB migration, which is evident by the concentrations of PCBs identified in the surface soil samples obtained from the catch basins. Catch basin contamination could be attributable to on-site runoff or a potential upgradient, off-site source.

Metals

Arsenic, chromium, copper and lead were commonly detected in surface and subsurface soils. TCLP soil extraction results revealed that arsenic, beryllium, copper, lead and zinc were leachable. Soil pH ranges from 6.4 to 7.8, indicating a neutral quality. The ground water concentrations of copper, lead and zinc are comparable to the TCLP results. Leached metals will tend to migrate with ground water flow to the north-northeast.

3.4.6 Summary of Human Health and Environmental Risk

The predominant current cancer risk at Site 13, as presented in the Phase I RI Report (TRC, 1991), is the worst-case risk estimate of 2.53 x 10^{-3} , associated with exposure to the maximum concentration of PCB-1260 in surface soil. Most-probable current cancer risk estimates ranged from 1.49 x 10^{-7} to 6.37 x 10^{-7} . The most-probable and worst-case future ground water cancer risk values ranged from 4.72 x 10^{-4} to 3.93 x 10^{-3} , with arsenic and beryllium driving the risk. Total cancer risks due to exposures to both soil and ground water under the future residential use scenario ranged from 4.75 x 10^{-4} for the most-probable scenario to 1.56 x 10^{-2} for the worst-case scenario.

An increased potential for noncarcinogenic effects is indicated as a result of exposure to Site 13 contaminants based on hazard index values exceeding one under the worst-case current use scenarios and greatly exceeding ten under a worst-case future residential use scenario. These risk estimates are driven by the maximum detected levels of PCBs in surface soils. Hazard index values also exceeded ten for a small child exposed to ground water (specifically, antimony, arsenic, cadmium, and manganese) under the worst-case scenario. Hazard index values under the most-probable scenario were less than one, with the exception of future ground water ingestion under the residential use scenario.

The ecological risk assessment presented in the Phase I RI Report (TRC, 1991) concluded that, due to the level of development at and surrounding Site 13, terrestrial receptors will be limited. The PCBs present in surface soils and storm drains on-site may pose a potential risk to terrestrial receptors, should any be exposed. Further characterization of ground water and surface water (storm drain) flow regimes and surface water quality, as will be conducted during the Phase II RI, is required to assess potential risks to ground water/surface water receptors. The Phase II RI will also include additional ecological characterization.

3.5 Remedial Response Objectives and Cleanup Criteria

Remedial response objectives are developed in order to set goals for protecting human health and the environment early in the alternative development process. The goals should be as specific as possible but should not unduly limit the range of alternatives that can be developed. For the Group I sites, the results of the RI have been used to define specific contaminants of interest and allowable exposures based on the risk assessment and ARARS/TBCs.

3.5.1 Comparison to Contaminants to ARARs/TBCs

Based on the results of the RI, a summary of surface soil and ground water contaminants and a comparison of their detected levels to ARARs/TBCs are provided below. The identification of remedial response objectives, presented in Section 3.5.3, will be based on this evaluation.

In evaluating surface soil contaminant levels, state and federal standards were used as ARARs. Only a limited number of standards are applicable to soil contamination. Since no ARARs/TBCs were identified for other soil

contaminants, standards and guidance levels applicable to PCB and lead contamination in soils were used as the basis for this evaluation. At Site 05, lead was detected at a level which exceeded the state guidance level. Lead was detected at a level of 303 ppm (see Figure 3-10) in one surface soil sample (S5-04), which exceeds the Rhode Island guidance level of 300 ppm but is within the federal guidance level range for lead. At Site 13, only PCBs exceeded state and federal guidance levels. PCBs were detected at concentrations ranging from 1.1 ppm to 4,563 ppm (see Figure 3-11). surface soil samples (S13-06, S13-08, and S13-09) and three catch-basin sediment samples (S13-11, S13-12, and S13-13) exceeded the historic RIDEM cleanup standard of 1 ppm. One sample, S13-09, exceeded both the new definition for solid waste (wastes containing a concentration of 10 ppm or greater PCBs) included in RIDEM's Proposed Amendments to the Rules and Regulations for Solid Waste Management Facilities and the new definition for hazardous waste (Type 6 - extremely hazardous waste includes wastes containing a concentration of 50 ppm or greater PCBs) included in RIDEM's Proposed Amendments to the Rules and Regulations of Hazardous Waste Management. sample also exceeds the 10 ppm cleanup level specified under TSCA, which may not be applicable to this release but may be relevant and appropriate. No other state or federal action levels were exceeded by any detected contaminant levels at Sites 05, 06, or 13. See Tables 3-1, 3-2, and 3-3 for a comparison of soil contaminant levels to associated action levels for each of these sites, respectively.

In evaluating ground water contaminant levels, state and federal standards (i.e., Maximum Contaminant Levels (MCLs), Maximum Contaminant Level Goals (MCLGs), Secondary Maximum Contaminant Levels (SMCLs) and Rhode Island Ground Water Quality Standards) were used as ARARs/TBCs. Of the Group I sites, Site

13 and Site 06 were the only sites at which ground water was sampled. Each site exhibited ground water contaminants which exceeded MCLs. At Site 06, beryllium and lead were present at levels which exceed MCLs or federal action levels. Total chromium was detected at a maximum level which was less than the MCL and the proposed Ground Water Quality Standard for total chromium but which exceeded the Ground Water Quality Standard for hexavalent chromium. The contaminants at Site 13 that exceeded MCLs or federal action levels were bis(2-ethylhexyl)phthalate, antimony, arsenic, beryllium, cadmium, chromium, lead, and nickel. With respect to non-enforceable SMCLs, iron, manganese and aluminum were detected at both Sites 06 and 13 at levels which exceed SMCLs. No other contaminants exceeded the ARAR/TBC contaminant levels at the Group I sites. Table 3-4 presents a comparison of the ground water contaminants detected at Site 06 to state and federal standards, and Table 3-5 summarizes the same information for Site 13. Figure 3-12 indicates which ARARS/TBCs were exceeded at each well location at Sites 06 and 13.

3.5.2 Risk-Based Considerations

described in National Contingency CFR λs the Plan 300.43(e)(2)(i)(A)(2)], "The 10^{-6} risk level shall be used as the point of departure for determining remediation goals for alternatives when ARARs are not available...". The 10^{-6} starting point indicates U.S. EPA's preference for setting cleanup levels at the more protective end of the acceptable 10^{-4} to 10^{-6} risk range for Superfund remedial actions. Site-specific and remedy-specific factors are then taken into consideration in the determination of where within the 10^{-4} to 10^{-6} risk range the cleanup standard for a given contaminant will be established. For the purposes of this evaluation, the risk-based cleanup levels which correspond to a 10^{-6} risk are calculated.

Site-specific and remedy-specific factors which may effect the determination of the final cleanup level will be addressed in subsequent portions of this document.

Those surface soil and ground water contaminants which contribute an individual cancer risk of greater than 1×10^{-6} to the overall cancer risk estimate under the reasonable maximum exposure scenario for future residential use, as presented in the risk assessment portion of the Phase I RI Report (TRC, 1991), were evaluated to determine if there are any for which an ARAR/TBC has not been identified. A similar evaluation was conducted for contaminants which contribute an individual noncarcinogenic hazard index ratio greater than one to the overall noncarcinogenic risk. For the contaminants identified by this evaluation, risk-based cleanup levels were calculated assuming future residential site use.

PAHs drove the carcinogenic risk estimates associated with exposures to surface soil at Sites 05 and 06, while arsenic drove the carcinogenic risk estimate at Site 13. Arsenic and beryllium also were found to pose a cancer risk greater than 1 x 10⁻⁶ at Site 05. Surface soil cleanup levels were calculated for these contaminants based on the 1 x 10⁻⁶ cancer risk, as presented in Table 3-6. As stated previously in Sections 3.2.6, 3.3.6, and 3.4.6, no individual hazard index values greater than unity were calculated for noncarcinogens in surface soils at Sites 05 and 06 in the risk assessment presented in the Phase I RI Report (TRC, 1991). At Site 13, only PCBs presented a potential noncarcinogenic risk but there are ARARs/TBCs available for the evaluation of PCB remediation. Therefore, no risk-based cleanup levels were calculated for noncarcinogens in the surface soil. For subsurface soils, risks posed by the detected contaminants did not exceed the point of departure (a 10-6 carcinogenic risk or a hazard index value of unity) and,

therefore, no risk-based cleanup levels were calculated for subsurface soil contaminants. Additional information used in the development of risk-based cleanup levels is presented in Appendix A.

The surface soil contaminant levels for each of the surface soil sample locations were compared to the risk-based cleanup levels as presented in Table 3-6. All of the PAHs which were detected at Site 05 were detected at concentrations exceeding the risk-based cleanup level in at least one sample, with the exception of indeno(1,2,3-cd)pyrene (see Figure 3-13). Four of ten surface soil samples had concentrations of PAHs above the cleanup levels, with the highest concentrations found at sample S5-10 (470 ppb to 1,800 ppb). PAHs were detected in all three surface soil samples at Site 06, but no concentrations exceeded the developed cleanup levels. PAHs did not present a risk greater than 10-6 at Site 13. It should be noted that for all SVOC analyses of surface soil samples, detection limits exceeded risk-based cleanup levels for PAHs. Therefore, there is a degree of uncertainty associated with the evaluation of the extent of PAH contamination at levels exceeding risk-based cleanup levels.

For inorganics, arsenic and/or beryllium were detected in each of the surface soil samples at Site 05 at levels exceeding risk-based cleanup levels (see Figure 3-13). At Site 13, a risk-based cleanup level was developed only for arsenic. One of the six surface soil samples exceeded the cleanup level for arsenic, with 1.6 ppm found at B13-04 (see Figure 3-14).

As indicated in Table 3-6, the greatest calculated reasonable maximum soil exposure risk under the future residential use scenario for an individual compound is 3.5×10^{-5} . Therefore, calculated risk levels exceed 10^{-6} but fall within the acceptable risk range of 10^{-4} to 10^{-6} applicable to remedial actions.

In ground water, as stated in Sections 3.3.6 and 3.4.6, manganese at Site 06 and Site 13 exhibited a hazard index ratio greater than unity. Therefore, a noncarcinogenic cleanup level was calculated for manganese and is presented in Table 3-7 and indicated in Figure 3-15. At Site 06, manganese exceeded the risk-based cleanup level in all six samples (two rounds of analyses), with a maximum detected concentration of 2,680 ppb. At Site 13, manganese also exceeded the cleanup level in all of the ground water samples collected, with a maximum concentration of 2,170 ppb at GW13-04B.

3.5.3 Remedial Response Objectives

Based on the information presented above as well as a consideration of potential ecological risks, the remedial action objectives for surface soil are as follows:

- Minimize current and future exposures to surficial soil contaminants at levels which exceed ARARs/TBCs, as presented in Tables 3-1 and 3-3, or which pose unacceptable risks to human health and the environment; and
- Minimize off site migration of surface soil contaminants.

The remedial response objectives for ground water are as follows:

- Prevent exposure, due to ground water ingestion, to contaminants at levels exceeding acceptable ARARs/TBCs as indicated in Tables 3-4 and 3-5, or which pose unacceptable risks to human health and the environment; and
- Minimize migration of ground water contaminants and any associated environmental impacts.

3.6 General Response Actions

General response actions are those remedial actions which will satisfy the remedial objectives. General response actions for Group I sites were formulated based on the results of the Remedial Investigation.

The first step in determining appropriate general response actions for a given media is an initial determination of the areas or volumes to which the general response actions may be applied, as described below. In determining these volumes/areas of media, consideration has been given to site conditions, the nature and extent of contamination, acceptable exposure levels and potential exposure routes. As previously presented in Section 3.5, remediation limits will depend upon the level of risk determined to be acceptable for the sites.

Soil

In order to provide a preliminary estimate of the volume of soil requiring remediation, the extent of soil contamination at levels exceeding ARARs/TBCs and risk-based cleanup levels must be evaluated. Two remedial scenarios have been developed for the Group I sites. The first scenario involves remediation of soils/sediments which exceed current action levels and the 10^{-6} risk level. The second scenario addresses only soils/sediments which are contaminated at levels exceeding ARARs/TBCs.

The areas or volumes of media which would require remediation under the first scenario (remediation to meet action levels and risk-based cleanup levels) are discussed below.

- Site 05 surface soil would require remediation due to the presence of PAHs, lead, arsenic and beryllium. The estimated areal extent of contamination is illustrated on Figure 3-13. The contaminated area covers 19,000 ft², and assuming a thickness of 2 ft, the volume requiring remediation is 1,400 yd³.
- No surface soil would require remediation at Site 06.
- At Site 13, the total surface soil area which would require remediation is 50,000 ft², as indicated on Figure 3-14. Using a thickness of two feet, the volume requiring remediation is estimated at 3,700 yd³.

The areas or volumes of media which would require remediation under the second scenario, remediation to meet action levels (namely, a lead cleanup level of 300 ppm and a PCB cleanup level of 1 ppm) are provided below.

- Only lead would require remediation at Site 05 under the second scenario. The area of surficial contamination is estimated at 1,350 ft² (see Figure 3-10). Using a thickness of two feet, the volume of soil requiring remediation is estimated at 300 yd³.
- No surface soil at Site 06 would require remediation.

Only PCBs would require remediation at Site 13 under the second scenario. The area of surficial contamination is estimated at $45,000~\rm{ft}^2$ (see Figure 3-11). Using a thickness of two feet, the volume of soil requiring remediation is estimated at $3,300~\rm{yd}^3$.

It should be noted that, if the proposed RIDEM Amendments to the Rules and Regulations for Solid Waste Management Facilities are promulgated, the area of surficial contamination could further decrease under the proposed definition of solid waste, which includes any soil with a concentration of PCBs of 10 ppm or greater. Soil containing 50 ppm or greater of PCBs would require handling as a hazardous waste under the Proposed Amendments to the Rules and Regulations for Hazardous Waste Management.

A listing of general response actions developed for the remediation of soil is provided below.

Soil:

No Action
Institutional Control
Containment
Treatment/Disposal

Ground Water

In order to provide a preliminary estimate of the volume of ground water requiring remediation, the extent of ground water contamination at levels

exceeding ground water ARARs/TBCs and risk-based cleanup standards must be evaluated. While contaminant levels exceed MCLs and risk-based cleanup levels at Sites 06 and 13, insufficient information exists to clearly define the area of ground water contamination. The contaminated ground water plume cannot be accurately defined without the presence of additional wells to delineate the boundaries of the plume. Similarly, while the ground water flow direction can be interpolated based on wells located at each site (see Figure 3-6), additional wells are needed to further define the flow direction and thereby allow for a detailed evaluation of potential remedial alternatives. Therefore, the Feasibility Study for the Group I sites will be developed using a phased approach, by dividing the sites into operable units. Two distinct operable units will be created, with surface soil/sediment contamination addressed within this operable unit, and ground water contamination to be addressed in the future, within a separate operable unit. Surface soils and sediments will be addressed in this Initial Screening of Alternatives, but the development of ground water remediation alternatives will proceed when information generated during the Phase II remedial investigation is available for incorporation.

3.7 Identification and Screening of Technologies and Process Options

The general response actions are developed further through the identification and screening of remedial technologies which could potentially meet the remedial action objectives and cleanup criteria. Following a screening of the remedial technologies on the basis of technical implementability, the process options associated with each technology are screened based on effectiveness, implementability and cost. Representative process options are chosen for inclusion in the remedial alternatives developed for the sites.

3.7.1 Technology Screening

A combined technology screening was performed for all the sites addressed within the ISA. The technology screening for soils/sediments is presented in Table B-l of Appendix B. The table includes brief descriptions of the individual technologies or process options, comments on their general applicability, limiting characteristics which prevent their application to certain sites, and a summary of whether they are screened or retained for the various sites. The technologies or technology process options which do not pass the screening process on the basis of technical implementability will not be retained for further consideration.

As mentioned in Section 3.6, under either site remediation scenario evaluated, soils at Site 06 do not require remediation. In conducting the technology screening for soils and sediments at Sites 05 and 13, technologies were evaluated for their technical ability to address PAHs, PCBs, and inorganic contaminants in surface soils, as well as their ability to be applied to the site-specific conditions at Sites 05 and 13. Because Site 05 is very limited in areal extent, some technologies could not physically be employed on-site; however, certain technologies which could be physically employed at Site 13 were retained for further consideration for Site 05 on the sites could assumption that both be remediated concurrently contaminated soils could be transported from Site 05 to Site 13 for treatment). The technologies which were screened from further analysis at Sites 05 and 13 include on-site landfilling, mechanical/thermal aeration, slurry phase biodegradation, in situ biodegradation, radio frequency heating, in situ vitrification, solidification/stabilization, and steam injection/vacuum extraction. desorption, dechlorination and fungal degradation were screened from further

analysis for Site 05 only. Technologies and process options which passed the technology screening for Sites 05 and 13 are summarized in Table 3-8.

3.7.2 Process Option Screening

Upon identification of those technologies which are implementable, the process options are further evaluated to allow the selection of a representative process option for each technology type. process options are evaluated on the basis of effectiveness, implementability, and cost. Process option evaluations for soil/sediment are presented in Table B-2 of Appendix B. Because the main risks currently identified for Sites 05 and 13 are associated with direct contact with or ingestion of contaminated surface soils, the process options associated with each technology were evaluated to determine their effectiveness in addressing this risk. institutional control technologies, both deed restrictions and fencing were selected as representative process options. For the capping technology, a RCRA Subtitle D soil cap was determined to provide protection against exposures to contaminated surface soils while also being implementable and cost-effective. For excavation and disposal, off-site landfilling was the only process option retained for analysis. For excavation and treatment technologies, stabilization/solidification, on-site incineration, off-site incineration, acid extraction and solvent extraction were selected to be representative process options for Sites 05 and 13. The selected representative process options are indicated with a bullet in Table 3-8 for Sites 05 and 13.

3.8 Remedial Alternative Development

The technologies and process options developed in Section 3.7 are combined in this section to form remedial alternatives. The range of alternatives

which is developed is intended to provide varying degrees of site cleanup. The alternatives presented herein have been developed consistent with criteria mandated by the National Contingency Plan (NCP, 40 CFR 300). NCP criteria require the consideration of the following:

The no action alternative.

For alternatives which provide control of the source of contamination, the alternatives should include:

- One or more alternatives that involve little or no treatment, but provide protection of human health and the environment primarily by preventing or controlling exposure to hazardous substances through engineering controls (caps, slurry walls, etc.) and/or institutional controls (land use restrictions, etc.).
- Alternatives in which a principal element is treatment that reduces the toxicity, mobility, or volume of hazardous substances. This range should include an alternative that removes or destroys hazardous substances to the maximum extent feasible, thereby eliminating or minimizing the need for long-term management.
- The development of one or more innovative treatment technologies for further consideration.

As indicated in Table 3-9, a total of four alternatives have been developed for addressing soil/sediment contamination at Sites 05 and 13. These alternatives include a no action alternative (I-1), a limited action alternative (I-2), a containment alternative (I-3), and an active restoration alternative (I-4). Four treatment/disposal options were evaluated under Alternative I-4. Specifically, the remedial alternatives include deed restriction/fencing (I-2), a RCRA Subtitle D soil cap (I-3), off-site landfilling or off-site incineration (Option A, I-4), on-site incineration (Option B, I-4), stabilization/solidification (Option C, I-4), and acid extraction/solvent extraction (Option D, I-4).

Site 06 exhibited no surface soil or sediment contaminants at levels exceeding ARARs or TBCs or risk-based cleanup levels and is not addressed

under either remedial scenario, as previously described in Section 3.6. Therefore, Site 06 will be considered a no action site and will be discussed under the no action alternative only. If additional information gained during the Phase II RI indicates that soil contamination is impacting ground water quality or other environmental media, the remediation of Site 06 soils will be re-evaluated at that time.

Sites 05 and 13 are addressed under both the remedial scenario where the sites are remediated to address ARARs/TBCs and the remedial scenario where the sites are remediated to address both ARARs/TBCs and risk-based cleanup levels.

3.9 Definition and Preliminary Screening of Remedial Alternatives

For each of the remedial alternatives developed, such information as the location and extent of excavation and containment as well as the volumes of soil to be collected, excavated or treated are described. The thought process used in the development of alternatives is also presented. A preliminary screening is performed after the individual description of each alternative.

The objective of the preliminary screening process is to reduce the number of alternatives that will be evaluated in the Detailed Analysis of Alternatives. This screening aids in streamlining the feasibility study process while ensuring that the most promising alternatives are being considered. A range of treatment alternatives from no action to site restoration is typically retained, where practicable, throughout the initial screening process. The comparisons between alternatives in this section typically focus on similar alternatives, the most promising of which is carried forward for further analysis.

The preliminary screening consists of an evaluation of the effectiveness, implementability, and cost of the alternative. The effectiveness screening

evaluates the ability of each alternative to protect human health and the environment through a reduction in the toxicity, mobility or volume of contaminated material. Both longand short-term effectiveness considered. The implementability screening takes into consideration the technical and administrative feasibility of constructing, operating, and maintaining the alternative. The final evaluation criterion, cost, involves the estimation of both capital and operation and maintenance (O&M) costs associated with each alternative. Preliminary cost estimates are provided in Appendix C. Due to the level of refinement of the alternatives at this point in the Feasibility Study, cost estimates may not be as accurate as those developed during the detailed analysis of alternatives conducted during the Detailed Analysis of Alternatives. However, estimates are comparative in terms of relative accuracy to allow cost decisions to be made at this point.

Those alternatives which pass the preliminary screening process will be evaluated further in the Detailed Analysis of Alternatives.

3.9.1 Alternative I-1 - No Action

3.9.1.1 Description

The no action alternative would involve no remedial response activities for soils at the Group I sites. No removal or treatment of contaminated surface soil/sediment would be conducted. No component of the no action alternative minimizes any potential risks that may be associated with direct contact with on-site contaminants. In accordance with requirements specified in the NCP, a review of the no action decision would be conducted in five years for any site at which it was determined that unlimited future use would not be protective of human health. Consideration of the no action alternative is required under the NCP.

3.9.1.2 Evaluation

<u>Effectiveness</u> - The no action alternative would provide no reduction in the toxicity, mobility or volume of contaminants in site soil/sediment. The short-term risks would be minimal, due to the lack of activities associated with its implementation. The long-term effectiveness is based on the levels of risk which existing contaminants pose to human health or the environment at each site.

- At Site 05, the concentration of lead detected in one surface soil sample exceeds RIDEM's action level of 300 ppm, and the no-action alternative would not be effective in addressing this contamination. For current use and future residential use, the existing risk levels are within the acceptable range for Superfund remedial actions; however, this alternative would not achieve the point of departure risk level of 1 x 10⁻⁶.
- No contaminants at Site 06 pose a threat to human health or the environment based on ARARs/TBCs or risk-based cleanup levels, so the no action alternative would be very effective in the long-term.
- At Site 13, the elevated levels of PCBs in site soils and sediments would limit the long-term effectiveness of the no action alternative. The PCB contamination would continue to pose a relatively high level of risk to human health and the environment.

<u>Implementability</u> - The no action alternative would require no implementation activities at any of the sites other than a five year review; therefore, it is easily implemented.

 $\underline{\text{Cost}}$ - A nominal cost would be associated with the preparation of the 5-year review.

3.9.2 Alternative I-2 - Fencing and Deed Restrictions

3.9.2.1 Description

This limited action alternative would involve no remedial response activities for soil/sediment at Sites 05 and 13, although it would include both the construction of a perimeter site fence and implementation of deed

restrictions. A six-foot high chain link fence would be placed around the contaminated areas at both Sites 05 and 13. Placement of hazard warning signs on the fences would also be included in this alternative. The proposed locations of the fences are shown in Figures 3-16 and 3-17.

This limited action alternative would also include implementation of land use deed restrictions. These restrictions, which would limit allowable future site use and development, have been included to provide an added measure of long-term protection of human health through minimizing potential future exposures to contaminated site surface soil/sediment. The deed restrictions could limit future residential development of Site 05 and Site 13, thereby eliminating the future use scenario where the 10^{-6} risk level was exceeded (see Section 3.5.2).

In contrast to Alternative I-1, which was required to be considered under the NCP, this alternative has been developed to provide an increased level of protection of human health through fencing and land use restrictions while providing no action to reduce the toxicity, mobility or volumes of contaminated surface soil at Sites 05 or 13.

3.9.2.2 Evaluation

Effectiveness - This alternative would provide no reduction in the toxicity, mobility or volume of contaminated soils at Sites 05 and 13. It would also provide no direct protection of human health or the environment. Through fencing and deed restrictions, it would limit potential exposures due to direct contact with contaminated surface soil/sediment and would limit future site use. Proper maintenance of the perimeter fence and compliance with deed restrictions would be required to maintain the alternative's long-term effectiveness at both sites. However, due to the scheduled base

closure, long-term maintenance and enforcement of this alternative could be difficult to implement. Minimal short-term risks would be associated with its implementation. Therefore, it would also be effective in the short-term.

Implementability - This alternative would involve the placement of land use deed restrictions on a property controlled by the federal government. Implementation of these deed restrictions should be relatively easy. The placement of the perimeter fence should not be difficult given the lack of active use of each site. Overall, this alternative would be easy to implement although it may be difficult to enforce over the long-term due to scheduled base closure.

<u>Cost</u> - Costs associated with this alternative would be those associated with perimeter fence construction and establishing land use restrictions.

The cost of this no action alternative is initially estimated based on an assumed 30-year maintenance period for the perimeter fence. The present worth value for Alternative I-2 at Sites 05 and 13 is \$45,000. See Appendix C for preliminary cost estimates.

3.9.3 Alternative I-3 - RCRA Subtitle D Soil Cap/Deed Restrictions

3.9.3.1 Description

This alternative was developed to meet the NCP's requirement for consideration of an alternative which utilizes containment with little or no treatment. Alternative I-3 incorporates the capping or covering of Sites 05 and 13 with a RCRA Subtitle D cap consisting of a minimum 18-inch infiltration layer topped by a minimum 6-inch erosion layer. The infiltration layer would be constructed to provide a permeability less than or equal to the natural subsoils or a permeability no greater than 1 x 10^{-5} cm/sec, whichever is less. The erosion layer would consist of a minimum of 6 inches of earthen material capable of sustaining native plant growth. The selected cap design

meets remedial objectives by limiting future exposure to surficial contamination and minimizing erosion. At Site 13, the cap would be designed to direct drainage away from the catch basins and the catch basins would be covered to prevent drainage and access into the basins.

The capping alternative would cover the entire contaminated area for each site. Two capping options were developed:

- Option A Capping of all surface soils which exceed ARARs/TBCs and risk-based cleanup levels (19,000 ft² at Site 05 and 50,000 ft² at Site 13).
- Option B Capping of all surface soils which exceed ARARs/TBCs (1,350 ft² at Site 05 and 45,000 ft² at Site 13).

The physical limits of the capping options would consist of the shaded areas shown in Figures 3-13 and 3-14 for Option A and in Figures 3-10 and 3-11 for Option B. The soil cap would minimize potential risks associated with direct contact with contaminated surface soils/sediments.

In addition to the Subtitle D soil cap, deed restrictions would be placed on the sites to limit future site use and development. The deed restrictions would aid in the long-term protection of human health.

3.9.3.2 Evaluation

Effectiveness - Alternative I-3 would provide no reduction in the toxicity or volume of site contaminants but it would limit exposure to surficial contamination and the potential migration of surficial contaminants due to erosion. By limiting potential exposure pathways, this alternative would provide a degree of protection of human health and the environment. Short-term effectiveness would be impacted by the disruption of surficial materials required to cap each site, especially at Site 05 where surficial vegetation (light woods) would require clearing prior to cap construction.

The cap and deed restrictions would be effective in addressing the areas of concern. Long-term effectiveness depends upon maintenance of the cap's integrity and the effectiveness of the deed restrictions.

At Site 13, capping would not prevent migration of existing PCB contamination via the catch basins unless both the catch basins themselves and the upgradient end of the drainage pipe are also capped.

Implementability - Alternative I-3 would be relatively easy to implement. It would require the construction of a soil cap. This activity employs commonly used and widely accepted construction equipment and techniques. Site 13 is flat and covered with grass which minimizes the need for extensive site preparation. Site 05 would require clearing of existing vegetation prior to cap construction. Administrative implementation of land use deed restrictions would be relatively easy to undertake given the present ownership of the sites by the federal government. The overall implementability of Alternative I-3 is good, although long-term maintenance of this alternative will be complicated by the scheduled base closure.

 $\underline{\text{Cost}}$ - The main cost factor associated with Alternative I-3 is the construction of the RCRA Subtitle D soil cap. The initial estimates of the present worth cost for Alternative I-3 are:

- Option A \$160,000
- Option B \$110,000

See Appendix C for preliminary cost estimates.

3.9.4 Alternative I-4 - Soil Disposal/Treatment

3.9.4.1 Description

Alternative I-4 consists of active site restoration, and includes the consideration of a number of treatment/disposal technologies for contaminated

surface soil at Sites 05 and 13. This alternative requires the removal of contaminated soils and sediments. The period of restoration will be dependent upon the technologies included in the final alternative. This analysis is intended to provide the basis for a general comparison between Alternatives I-1, I-2, I-3 and I-4. Preliminary analyses of the effectiveness, implementability and costs of the individual technology options are presented in Sections 3.9.5 through 3.9.8.

3.9.4.2 Evaluation

Effectiveness - For soils, Alternative I-4 would provide a reduction in the mobility or toxicity of soil contaminants through either excavation and disposal or excavation and treatment. By removing and treating or disposing of the contaminated material, this alternative would be protective of human health and the environment. Short-term effectiveness would be impacted by the disruption of the soils during excavation, but personnel protective measures could be taken during the removal to protect on-site workers and dust minimization controls could be used as necessary to minimize off-site migration of any airborne particulates. The removal of the contaminated soils could be completed within a relatively short time frame. The degree of toxicity reduction and the reliability of the remedial action (and, therefore, the long-term effectiveness) would be dependent upon the individual disposal or treatment technology selected. In general, by excavating and treating or disposing of the contaminated soils, the long-term effectiveness of this alternative would be considered greater than that of the previously evaluated no action, minimal action and containment alternatives.

Implementability - Alternative I-4 is implementable, although its implementability would be highly dependent upon the individual technologies

included in the alternative. The removal of contaminated sediments from the catch basins may be somewhat difficult to implement.

Cost - As with implementability, cost would be highly dependent upon the individual technologies included in the alternative. In general, Alternative I-4 would cost significantly more than Alternatives I-1, I-2, and I-3 due to the active restoration activities involved in its implementation.

3.9.5 <u>Alternative I-4 - Option A - Off-Site Landfill/Off-Site Incineration</u>

3.9.5.1 Description

This option would involve excavation and off-site transportation of soil/sediment to a suitable landfill. Disposal of contaminated soil/sediment at an off-site landfill would eliminate the need for long-term management of the soil/sediment on-site. Prior to landfilling, the excavated soil must be characterized to determine if it meets the definition of hazardous waste and if it falls under land disposal restrictions. Soil samples from Sites 05 and 13 were analyzed for TCLP parameters during the Phase Ι Remedial Investigation. No samples exceeded TCLP limits, thus the surface soil/sediment at Site 05 is assumed to be non-hazardous. worst-case scenario involving off-site disposal as a hazardous waste will be assumed for costing purposes.

At Site 13, federal land disposal restrictions (40 CFR Parts 261 and 268), which prohibit the acceptance of certain waste types at landfills, must be evaluated. Restricted waste types include solvent-, dioxin-, and California-list-contaminated soils and soils contaminated with listed or characteristic hazardous wastes. Restricted wastes under the California-list include non-liquid hazardous wastes containing halogenated organic compounds (including PCBs) in total concentrations greater than or equal to 1,000 ppm.

In one sample at Site 13 (S13-09), PCBs were detected at a concentration of 4,563 ppm. To satisfy the federal land disposal restrictions, the volume of surface soil with PCB concentrations greater than 1,000 ppm will not be landfilled. Additional sampling will be conducted to segregate this highly contaminated soil and it will be sent to an off-site TSCA-approved incinerator. The remainder of the PCB-contaminated soil will be disposed of in an off-site chemical waste landfill in accordance with TSCA requirements that soils with PCB concentrations greater than or equal to 50 ppm be disposed of in a chemical waste landfill. Off-site incineration involves excavation and transportation of the soil to a suitable incinerator. Excavated soils would require drumming prior to off-site transport in accordance with incinerator acceptance requirements.

Based on these considerations, preliminary costs for this alternative have been prepared for the scenarios listed below:

- Scenario 1 The surface soil from Site 05 (1,400 yd³) exceeding ARARs/TBCs and risk-based cleanup levels and soil/sediment from Site 13 with PCB and inorganic concentrations exceeding ARARs/TBCs and risk-based cleanup levels but less than 1,000 ppm (3,200 yd³) will be shipped to a chemical waste landfill. The soil from the PCB hotspot with PCB concentrations of 1,000 ppm or greater (500 yd³) will be sent to an off-site incinerator.
- <u>Scenario 2</u> The surface soil from Site 05 (300 yd³) exceeding ARARs/TBCs (specifically, the RIDEM action level for lead) and soil/sediment from Site 13 with PCB concentrations greater than 1 ppm but less than 1,000 ppm (2,800 yd³) will be shipped to a chemical waste landfill. The soil from the PCB hotspot with PCB concentrations of 1,000 ppm or greater (500 yd³) will be sent to an off-site incinerator.

3.9.5.2 Evaluation

Effectiveness - Overall, the off-site landfill/off-site incineration option described above would reduce the mobility, volume, and toxicity of the PCB-hotspot of contaminated surface soil at Site 13. It would reduce the

mobility, but not the volume or the toxicity of the remainder of the contaminated soil/sediment from Sites 05 and 13, which would be landfilled. The alternative would be protective of human health by addressing the main exposure pathways of concern.

Long-term effectiveness would depend upon the facilities receiving the waste. The long-term operating and maintenance procedures at the receiving landfill and the degree of contaminant destruction available in the incinerator and the long-term operation and maintenance of the ash disposal facility will affect the long-term effectiveness. Both hazardous material incineration and landfill facilities are commonly utilized waste management options.

In the short-term, exposures to remedial workers during soil/sediment excavation could be minimized through the use of appropriate health and safety equipment. No off-site impacts are anticipated in the short-term.

Implementability - Implementability of off-site landfill disposal would be directly related to the availability of a suitable landfill of adequate capacity to accept the type of material generated from the site. The off-site incineration component of the alternative would be relatively easy to implement, since several commercial incinerators can accept the type of waste from Site 13. Due to incinerator demand and capacity limitations, delays in the incinerator's acceptance of the waste for treatment are possible.

<u>Cost</u> - Factors which are considered in the cost evaluation of this alternative include the replacement and compaction of clean back-fill in excavated areas and the off-site disposal/incineration costs. The preliminary estimates for the cost of each of the disposal scenarios are:

Alternative I-4, Option A - Off-Site Landfill/Off-Site Incineration

- Scenario 1 - Sites 05 and 13 - 4,600 yd³ to a chemical waste landfill and 500 yd³ to a TSCA-approved incinerator - \$7,100,000

- Scenario 2 - Site 13 - 3,100 yd^3 to a chemical waste landfill and 500 yd^3 to a TSCA-approved incinerator - \$5,800,000

Preliminary cost estimates are presented in Appendix C.

3.9.6 Alternative I-4 - Option B - On-Site Incineration

3.9.6.1 Description

The on-site incineration alternative was developed as an option which reduces the toxicity, mobility, or volume of hazardous substances as a principal element. This alternative consists of the excavation and incineration of contaminated soils/sediments in an on-site incinerator. This option has been proposed for the following scenarios.

• Scenario 1 - All contaminated surface soil/sediment exceeding ARARs/TBCs and risk-based cleanup levels at Site 05 (1,400 yd³) and at Site 13 (3,700 yd³) would be excavated and incinerated. The incinerator would be mobilized at Site 13; therefore the soil from Site 05 will be transported to Site 13 for incineration.

Scenario 2 - Only the contaminated surface soil/sediment exceeding ARARs/TBCs at Site 05 (300 yd^3) and Site 13 (3,300 yd^3) would be excavated and incinerated at an on-site incinerator.

Based on the estimated volume, a medium-sized rotary kiln incinerator with a capacity of approximately 3 to 5 yd³/hour would be most cost effective for these sites. Following the excavation and incineration, the ash would require testing and handling in accordance with federal and state regulations. For the Scenario 2 soils, the PCBs should be destroyed to a level which would enable the ash to be backfilled on-site. Incineration will not treat all inorganic contaminants, however. Arsenic, which was detected at Site 13 at levels exceeding risk-based cleanup levels, and the lead contamination at Site 05 would either volatilize or remain in the residual ash. The ash could potentially require stabilization before replacement on the site.

3.9.6.2 Evaluation

Effectiveness - Alternative I-4, Option B would provide a reduction in the mobility, volume, and toxicity of contaminants. Organic contaminants would be destroyed in the incineration process. Inorganics would either volatilize in the incineration process (volatile toxic metals include mercury, selenium, arsenic, antimony, cadmium and lead) and be removed in the air treatment system, or would remain in the ash residue. Due to the destruction of organic contaminants by this treatment process, the long-term effectiveness of this alternative would be good. If the residual ash is stabilized and placed on-site, however, long-term monitoring could be required. Short-term effectiveness would be limited by the site disruption which would occur during excavation and incineration activities.

Implementability - Several vendors supply medium-sized, mobile rotary kiln incinerators. This option would be implementable although it does require significant site preparation and regulatory approvals. The administrative implementability would be dependent on the ability of the system to meet the federal and state requirements applicable to the operation of incinerators, including regulations applicable to the destruction of PCBs. Also, the potential local public opposition to such a remedial response is unknown.

Cost - The main costs associated with the incineration of contaminated soils at the Group I sites relate to the mobilization and operation of an on-site incinerator, as well as the potential cost associated with the stabilization of ash residuals. The costs associated with each scenario are provided below.

- Scenario 1 Sites 05 and 13 Incineration of 5,100 yd³ of contaminated soils - \$5,000,000
- Scenario 2 Sites 05 and 13 Incineration of 3,600 yd³ of contaminated soils - \$3,500,000

Appendix C includes preliminary cost estimates associated with Alternative I-4, Option B.

3.9.7 Alternative I-4, Option C - Stabilization/Solidification

3.9.7.1 Description

Option C consists of the excavation and stabilization of contaminated surface soils and sediments at Sites 05 and 13. The solidification/ stabilization process, sometimes referred to as immobilization, fixation, or encapsulation, uses additives or processes to physically or chemically immobilize the hazardous constituents of a contaminated soil. The soils would be stabilized by mixing with a cementing material and water. As the mixture hardens, the hazardous constituents are encapsulated within the solid matrix which is formed. Following stabilization, the stabilized material would require testing and handling in accordance with federal and state regulations. Due to the limited sizes of Sites 05 and 13, it is assumed that the stabilized material would be disposed of off-site as a non-hazardous waste.

Based on these considerations, preliminary costs for this option have been prepared using the two scenarios described below.

- Scenario 1 All surface soil/sediment exceeding ARARs/TBCs and/or risk-based cleanup levels at Site 05 (1,400 yd³) and at Site 13 (3,700 yd³) would be excavated, stabilized, and disposed of off-site.
- Scenario 2 Only the contaminated surface soils exceeding ARARs/TBCs at Site 05 (300 yd³) and Site 13 (3,300 yd³) would be excavated, stabilized, and disposed of off-site.

3.9.7.2 Evaluation

Effectiveness - Alternative I-4, Option C would be effective in immobilizing the soil contaminants through stabilization processes. While

solidification/stabilization has primarily been applied to soils contaminated with metals and other inorganics, the process has also been proven applicable to semivolatile and nonvolatile organic compounds such as PAHs and PCBs. The process would be effective in treating the volumes of contaminated material within a relatively short time frame. The main exposure pathways identified during the human health risk assessment would be addressed by this alternative. Short-term effectiveness would be limited by the site disruption which would occur during excavation and stabilization activities. These risks could be limited through the use of appropriate personnel protection equipment. Long-term effectiveness would be good since the stabilized material would be disposed of off-site.

Implementability - The technical implementability of this alternative would be expected to be good, with stabilization services available from numerous vendors. Mobile stabilization units are available in which the stabilization area is truck-mounted and requires no on-site construction of mixing pits. The administrative implementability would be dependent on the ability of the system to treat the soils sufficiently to meet the substantive requirements applicable to land disposal of the treated material. An off-site disposal site which could accept the stabilized material would have to be identified prior to implementation of this alternative.

<u>Costs</u> - The major costs associated with this option are those associated with the implementation of the soil stabilization process. Preliminary estimates of the present worth costs for the two scenarios are:

- Scenario 1 \$3,300,000
- Scenario 2 \$2,300,000

See Appendix C for preliminary cost estimates.

3.9.8 Alternative I-4, Option D - Acid Extraction and Solvent Extraction

3.9.8.1 Description

Option D consists of the excavation of contaminated surface soils and sediments at Sites 05 and 13 followed by treatment using acid extraction and solvent extraction, as applicable.

Acid extraction is a technology currently being developed for application to soils contaminated with inorganics. In most acid extraction processes, the soils are washed with a leaching solution which removes the inorganics into solution. The treated soils are then neutralized while the leaching solution undergoes additional treatment. Acid extraction has been proven for the removal of lead and arsenic from soils.

Solvent extraction is also a technology which is currently being developed to remediate organic contaminants in soils. It has been proven effective in the removal of PAHs and PCBs from soils. In most solvent extraction processes, the excavated soil is mixed with a solvent. The contaminants dissolve within the solvent and are extracted from the soil. Any residual solvent within the soil is then removed using thermal treatment. The solvent extraction solution may undergo additional treatment or disposal.

Both treatment processes may require removal of any large particle fraction prior to treatment through auxiliary screening or crushing processes. Soils could be segregated during excavation, based on the type of contamination, and treated within one or both treatment processes. Following treatment, the residual soil would require testing and handling in accordance with federal and state regulations. For the purpose of this evaluation, it is assumed that the treated soils could be placed back on-site at Site 13.

Based on these considerations, preliminary costs for this option have been prepared using the two scenarios described below.

- Scenario 1 All surface soil/sediment exceeding ARARs/TBCs and/or risk-based cleanup levels at Site 05 (1,400 yd³) and at Site 13 (3,700 yd³) would be excavated, treated and disposed of on-site at Site 13. It is assumed that one tenth of the contaminated soils at Site 05 (140 yd³) would require solvent extraction for treatment of PAHs and all 1,400 yd³ would require acid extraction for treatment of inorganics. At Site 13, it is assumed that all 3,700 yd³ would require solvent extraction for treatment of PCBs and only 400 yd³ would require acid extraction for treatment of inorganics.
- Scenario 2 Only the contaminated surface soils exceeding ARARs/TBCs at Site 05 (300 yd³) and Site 13 (3,300 yd³) would be excavated, treated, and disposed of on-site at Site 13. It is assumed that all 300 yd³ of surface soil from Site 05 would require acid extraction for treatment of inorganics. At Site 13, it is assumed that all 3,300 yd³ would require solvent extraction for treatment of PCBs.

3.9.8.2 Evaluation

Effectiveness - Alternative I-4, Option D is expected to be effective in treating the soil contaminants and thereby reducing the potential risks to human health posed by the contaminants. Both acid extraction and solvent extraction are treatment processes which are under development and not widely proven. Short-term effectiveness would be limited by the site disruption which would occur during excavation and treatment activities. These risks could be limited through the use of appropriate personnel protection equipment. Long-term effectiveness would be expected to be good, due to the lack of residual contamination remaining on-site. Both treatment processes would be able to treat the estimated volumes of material requiring treatment within a relatively short time frame.

Implementability - The technical implementability of this alternative may be limited by the limited number of vendors offering proven, full-scale treatment systems. Treatability study testing may be required prior to implementation. The administrative implementability would be dependent on the

ability of the system to treat the soils sufficiently to meet the substantive requirements applicable to land disposal of the treated material.

<u>Costs</u> - The major costs associated with this option are those associated with the treatment processes. Preliminary estimates of the present worth costs for the two scenarios are:

Scenario 1 - \$4,800,000

• Scenario 2 - \$3,100,000

See Appendix C for preliminary cost estimates.

3.10 Selection of Alternatives for Detailed Analysis

A comparative analysis of the individual alternatives based on the three evaluation criteria is conducted to allow the elimination of selected alternatives from the detailed analysis process.

3.10.1 Effectiveness

With respect to long-term effectiveness, those alternatives which involve reductions in the toxicity, mobility or volume of contamination and contaminant sources will provide the greatest protection. The effectiveness of an alternative in handling the contaminated media and its reliability are also considered under this criterion. With respect to short-term effectiveness, those alternatives which are protective during the construction and implementation period, and which achieve remedial response objectives within a timely manner, are most effective.

Alternative I-4, excavation and treatment/disposal of surface soil/sediment provides the greatest long-term effectiveness by treating or disposing of the contaminated soil/sediment. Due to the removal/treatment of contaminated soils and waste materials, this alternative typically results in

a short-term disruption of the waste materials; however, resultant risks can be controlled through proper excavation techniques and personnel protection. Off-site landfilling/incineration (Option A) offers the greatest long-term effectiveness by treating both PCBs and semi-volatile organics and by removing the contaminated soil off-site for treatment, with no placement of treatment residuals back on-site. It is effective and reliable in treating the contaminated media and achieves remedial objectives in a timely manner. Option C, stabilization/solidification, is also expected to provide a reduction in the mobility of both organic and inorganic soil contaminants but requires on-site treatment which may present an increase in short-term risks over an off-site treatment option. It is followed by on-site incineration (Option B), which provides on-site treatment of PCBs and other organic contaminants but which does not treat inorganics, results in increased short-term risks due to the on-site treatment process and potentially requires long-term maintenance of treatment residuals. Option D, acid extraction and solvent extraction, treats the PCBs, PAHs and inorganics but its effectiveness in achieving cleanup goals is not as well proven as other alternatives.

Alternative I-3, a RCRA Subtitle D soil cap, provides the next level of long-term effectiveness through a reduction in risks associated with direct contact with contaminated surficial soils/sediments. It is effective in handling the contaminated media and is reliable with respect to long-term performance. The cap could be constructed in a timely manner. Minimal short-term impacts would be associated with possible contact with contaminated surface soil during cap construction. Alternative I-2, no action with fencing and deed restrictions, provides limited long-term effectiveness. It limits potential exposures to soil/sediment contamination through fencing and deed restrictions. Short-term impacts associated with implementation would be

minimal, as would be the construction time frame. Alternative I-1, no action, provides the least protection against surface soil contaminants but could be considered to be effective in both the short- and long-term for Sites 05 and 06, especially for future non-residential site uses, based on site risk evaluations.

3.10.2 Implementability

Implementability is a measure of the technical and administrative feasibility of constructing, operating, and maintaining a remedial action Alternative I-1, no action, alternative. is the most implementable soil/sediment remedial alternative from a construction standpoint due to the lack of implementation activities associated with it. Alternative I-2, limited action, is also fairly readily implemented, involving only limited construction activities (i.e., installation of fencing). Alternative I-3, capping, is next in terms of implementability based on the relatively simple nature of cap construction. While easy to implement in the short-term, long-term maintenance of Alternatives I-2 and I-3 could be difficult to implement due to the scheduled base closure. Alternative I-4, excavation and treatment/disposal of surface soil and sediment, is the least implementable option in the short-term, requiring excavation and off-site treatment or disposal or on-site treatment, but due to the removal or treatment of contaminants, is most easily maintained in the long-term. Removal sediments from catch basins could be difficult to implement. soil/sediment treatment options, off-site landfilling, Option A, is the most implementable, followed by Options C (solidification/stabilization), B (on-site incineration) and D (acid extraction and solvent extraction).

3.10.3 Cost

Alternative I-1, no action, is the lowest cost alternative, closely followed by Alternative I-2, limited action. The RCRA Subtitle D soil cap alternative (I-3) costs \$160,000 and \$110,000 for Option A and Option B, respectively. The excavation and treatment/disposal of subsurface soil and sediment (Alternative I-4) costs are the most expensive, ranging from \$2,300,000 to \$7,100,000, for the various treatment options.

3.10.4 Selection of Alternatives for Further Consideration

Based on the comparative analysis presented in the previous section, no alternatives and no options are proposed to be eliminated from the range of alternatives undergoing detailed analysis. However, one of the remedial scenarios which was evaluated under Alternative I-3 and the Alternative I-4 treatment/disposal options will be deleted from further consideration. Under these alternatives, the scenario under which all soils which exceed ARARs/TBCs and risk-based cleanup levels are remediated (Scenario 1) will be eliminated. The scenario under which only soils which exceed ARARs/TBCs are remediated (Scenario 2) will be retained for further consideration. This determination is based on the uncertainties associated with the calculation of the risk-based cleanup levels or the applicability of the calculated risk-based cleanup levels to the associated sites. These uncertainties impact the alternatives' effectiveness evaluation in terms of the ability of the alternatives to meet the cleanup level objectives and to provide greater protection of human health and the environment by achieving risk-based cleanup levels as compared to achieving ARARs/TBCs only.

PAHs, arsenic and beryllium were detected in surface soils at Site 05 at levels exceeding risk-based cleanup levels while arsenic was the only

contaminant detected in surface soils/sediments at Site 13 at levels exceeding risk-based cleanup levels. With respect to PAHs, as noted previously in Section 3.5.2, in all SVOC analyses of surface soil samples at Site 05, detection limits exceeded the calculated risk-based cleanup levels for PAHs. Therefore, the areas at Site 05 which have been identified as containing PAHs at levels exceeding risk-based cleanup levels were identified on the basis of qualified data (i.e., samples where PAHs were detected at J-qualified or estimated levels). For the arsenic and beryllium which were detected at Sites 05 and 13 at levels exceeding risk-based cleanup levels, the calculated risk-based cleanup levels are less than the geometric mean concentration for background soils in the eastern U.S. (USGS, 1984). Site-specific background soil concentrations require further definition, as will be done in the Phase II RI, before the applicability of the calculated risk-based cleanup levels can be determined. If the Phase II RI results confirm that potential unacceptable risks to human health or the environment are associated with PAHs and inorganics at these sites and that detected contaminant levels are attributable to the sites and are not naturally occurring, this remedial scenario will be reconsidered.

Further supporting the elimination of Scenario 1 is the cost associated with implementation. For most alternatives, implementation of Scenario 1 is significantly more costly than the implementation of Scenario 2.

All of the alternatives, technology options and remaining remedial scenarios will be retained for detailed analysis. This will allow for the further consideration of a wide variety of remedial options providing a range in the degree of treatment for the contaminated media at Sites 05, 06 and 13.

4.0 GROUP II SITES - SITE 08 - DPDO FILM PROCESSING AREA

4.1 Introduction

The Group II sites consist solely of Site 08 - Defense Property Disposal Office (DPDO) Film Processing Area. The following sections provide a site description, summary of remedial response objectives and cleanup criteria, general response actions, identification and screening of technologies and process options, remedial alternative development, and preliminary screening of remedial alternatives.

4.2 Site 08 - DPDO Film Processing Area

4.2.1 Site Location and Description

Site 08 is a flat, grassy area located to the east of Building 314 at West Davisville. A general site location map is provided in Figure 4-1. The study area is defined as approximately a 1,600 square foot area which is likely to have received runoff from an adjacent paved area where wastes were reportedly discharged. A fence delineating the NCBC-Davisville property line forms the eastern border of the study area and immediately to the west of the grassy area is a paved road which runs adjacent to Building 314. Sandhill Brook crosses the developed area of West Davisville within a buried culvert which passes to the east of Site 08 (see Figure 1-7). The area to the east of the property line is overgrown and slopes gradually away from the site. Several warehouses are located to the west of Site 08. The nearest warehouse, Building 314, is currently not in use.

4.2.2 Site History Overview

For a six-month period during 1973, the DPDO recovered silver from photographic wastes. Waste liquids from this recovery process were discharged

on the pavement outside of Building 314 and allowed to runoff during rainfall events (Hart, 1984a). This silver recovery operation was operated as a batch system with a 15- to 20-gallon capacity. The waste liquids which were generated consisted of photographic compounds, such as sodium thiosulfate and hydroquinone, and liquids containing small concentrations of formaldehyde, acetic acid, potassium hydroxide and sulfuric acid. No information on the frequency or total quantity of discharge was available from interviews or record searches; however, the amounts were reportedly small (Hart, 1984a).

4.2.3 Geology, Hydrogeology and Hydrology

No subsurface borings were drilled at Site 08 during any of the site investigations. The glacially-derived soils should consist of sand and gravel near the surface, grading downward into sand with some silt (Schafer, 1961). The depth to bedrock should be from 20 to 40 feet below the ground surface (Johnson and Marks, 1959).

The depth to the water table is probably 3 to 10 feet below the ground surface (Johnson and Marks, 1959). The direction of flow, based on the surface topography, is estimated to be to the northeast, towards the discharge point of the Sandhill Creek culvert approximately 2,000 feet away.

4.2.4 Summary of Contamination

Field investigations conducted during the Confirmation Study in 1985 included surface soil sampling. The analytical results for the single composite surface soil sample collected indicated that silver was present at a concentration (0.15 ppm) similar to naturally occurring levels in soil. In addition, a grab surface soil sample was collected in March 1986 for full EPA Priority Pollutant analysis. The results of the analysis indicated no elevated levels of EPA Priority Pollutants.

The Phase I RI included the collection and analysis of 10 surface soil samples and 5 subsurface (2.5 to 3 feet) soil samples at randomly-generated sample locations, as indicated in Figure 4-2. Samples were analyzed for the full Target Compound List (TCL)/Target Analyte List (TAL). organic analyses indicated that acetone was present in two surface soil samples (S8-8 and S8-10), while estimated concentrations of chloroform were detected in three surface soil samples (S8-7, S8-8 and S8-10). Xylenes and an estimated concentration of ethylbenzene were detected in the sample collected at a depth of 3 feet at location S8-9. PAHs were detected in every surface soil sample, but were identified at only two of the five subsurface sampling locations (S8-5 and S8-9). Bis(2-ethylhexyl)phthalate was detected in every The 3-foot deep sample collected at location S8-9 exhibited elevated semivolatile detection limits (720 to 3,500 ppb) and elevated concentrations of fluorene (1,100 ppb) and 2-methylnaphthalene (2,400 ppb). PCB-1260 was detected in surface soils at four adjacent sampling locations (S8-3, S8-4, S8-6) and S8-7) at concentrations ranging from 190 to 1,400 ppb. Metals found to be common to each surface and subsurface soil sampling location included arsenic, beryllium, chromium, copper, lead, and zinc. Lead concentrations ranged from 2.6 ppm to 171 ppm. Samples from the center of the site exhibited concentrations of copper, lead, and zinc that were five times greater than those concentrations in surrounding soils. Silver was detected in one sample, S8-4, at a concentration of 28 ppm. The average concentrations of several metals (e.g., arsenic, copper and lead) are greater in the surface soils than in the subsurface soils.

TCLP results indicate that low levels of xylene may be leached from the soil. TCLP extraction results also revealed that chromium, copper, lead, nickel, and zinc were leachable from the soils. Gamma-BHC (Lindane) was

detected in one TCLP extract sample at Site 08, at a level near the detection limit (0.21 ppb).

4.2.5 Summary of Contaminant Fate and Transport

A contaminant fate and transport analysis was conducted as part of the Phase I RI. That analysis is summarized below. For more information, refer to the Phase I RI Report (TRC, 1991).

The primary contaminant migration pathways at Site 08 include surficial erosion or leaching of contaminants through the soil column to the ground water. Site 08 is relatively flat and, for the most part, grass-covered. Contaminant migration via surface water runoff would generally be towards the east, toward a currently undeveloped area. Sandhill Brook crosses the developed area of West Davisville within a buried culvert. The culvert passes to the east of Site 08, as indicated in Figure 1-7. The brook discharges into Saw Mill Pond, which is located approximately 3,000 feet northeast of the site. The ground water flow direction in the vicinity of Site 08 is expected to be towards the east.

Only surface and near-surface soil samples were collected at Site 08. The volatile organics detected in the surface soil samples included acetone and chloroform. With vapor pressures (at approximately 20° C) of 270 and 151 mm Hg respectively, the principal mechanism for natural removal is volatilization. Acetone has a relatively high solubility and could migrate with precipitation. Xylenes and ethylbenzene, both detected at a depth of 3 feet, have relatively high organic carbon partition coefficients ($K_{\rm OC}$ values) and would be expected to adsorb to the soils. Xylene was present at low levels (26 ppb) in the TCLP soil extraction results, indicating that it may be leached to ground water.

Semi-volatile organic compounds, particularly PAHs, are persistent in the environment due to their complex chemical nature. In general, PAH compounds related to 2-methylnaphthalene are more volatile and more soluble than those related to benzo(a)pyrene. Therefore, PAH compounds related to 2-methylnaphthalene are more likely to migrate from the surface soils. An elevated level of 2-methylnaphthalene was detected in one subsurface soil sample collected at a depth of 3 feet (S8-9). In general, PAH levels decreased with depth. TCLP analysis did not indicate a potential for significant leaching of PAH compounds from the soil.

Bis(2-ethylhexyl)phthalate was detected in all soil samples. Phthalate compounds are considered to be common laboratory contaminants and are widespread in the environment (ATSDR, 1989). They generally exhibit low solubility and high $K_{\rm OC}$ values, and so would not be particularly amenable to water transport.

Benzoic acid was detected in three surface soil samples at concentrations ranging from 49 to 130 ppb. Benzoic acid is highly soluble in water (greater than 1,000 mg/l), and could be amenable to water transport.

PCBs, which were detected in four surface soil samples, have a high Henry's Law Constant (greater than 10^{-3}), low water solubility (less than 100 mg/l), and high K_{OC} (greater than 100,000 ml/g). Therefore, PCBs have a tendency to volatilize from the surface soil but also have an affinity for organics in soil which tends to render them immobile. Because the site is covered by grass and is only slightly graded to the east, transport via erosion is expected to be minimal.

Based on the TCLP extraction results, chromium, copper, lead, nickel and zinc are leachable from the soils. Silver, which was detected in the TAL analysis of only one sample, was not leached from the soils. Concentrations

of inorganics in the TCLP leachate were generally similar to those detected in ground water samples collected at other NCBC-Davisville sites during the Phase I RI. Lead and nickel were present in the leachate at concentrations greater than typical NCBC-Davisville ground water concentrations. Background water quality will be defined during the Phase II RI, allowing further evaluation of the significance of the TCLP results with respect to ground water quality at Site 08.

4.2.6 Summary of Human Health and Environmental Risk

Current carcinogenic risks for Site 08, as presented in the Phase I RI Report (TRC, 1991), were at or below the 10^{-6} target risk level. Carcinogenic risks associated with future soil exposures were slightly higher at 3.14 x 10^{-5} for the worst-case scenario. The carcinogens driving these risk values are PAHs, PCBs, bis(2-ethylhexyl)phthalate, arsenic, and beryllium. Both current and future exposure scenario hazard indices were less than one, suggesting that no adverse acute or chronic noncarcinogenic effects are expected as a result of exposure to the detected contaminants at Site 08. Ground water sampling was not conducted at Site 08 during the RI.

The ecological risk assessment presented in the Phase I RI Report (TRC, 1991) concluded that, due to the level of development at and surrounding Site 08, risks to terrestrial receptors will be negligible. Further characterization of ground water flow regimes, and surface water quality, as will be conducted during the Phase II RI, is required to assess potential risks to ground water/surface water receptors. The Phase II RI will also include additional ecological characterization.

4.3 Remedial Response Objectives and Cleanup Criteria

Remedial response objectives are developed in order to set goals for protecting human health and the environment early in the alternative development process. The goals should be as specific as possible but should not unduly limit the range of alternatives that can be developed. For the Site 08 FS, the results of the RI have been used to define specific contaminants of interest and allowable exposures based on the risk assessment and ARARS/TBCs.

4.3.1 Comparison of Contaminants to ARARs/TBCs

Surface soil samples exhibited contaminants at levels exceeding ARARs and/or TBCs in the RI sampling at Site 08. A summary of surface soil contaminants and a comparison of their detected levels to ARARs/TBCs are provided below, followed by an evaluation of risk-based cleanup levels. The identification of remedial response objectives will be based on this evaluation.

In evaluating surface soil contaminant levels, available state and federal standards were used as ARARs/TBCs. Only a limited number of standards are applicable to soil contamination. Since no ARARs/TBCs were identified for other soil contaminants, standards and guidance levels applicable to PCB and lead contamination in soils were used as the basis for this evaluation. At Site 08, only PCBs exceeded state action levels. PCBs were detected in one sample in the southwest corner of Site 08. In sample S8-6, PCBs were detected at a level of 1.4 ppm from the 0- to 2-foot interval (see Figure 4-3). This value exceeds the historic RIDEM Cleanup Standard of 1 ppm but not the new definition for solid waste (which includes wastes containing a concentration of 10 ppm or greater PCBs) included in RIDEM's Proposed Amendments to the

Rules and Regulations for Solid Waste Management Facilities. No other state or federal action levels were exceeded by any detected contaminant levels at Site 08. See Table 4-1 for a comparison of soil contaminant levels to associated action levels.

4.3.2 Risk-Based Considerations

As described in the National Contingency [40 Plan CFR 300.43(e)(2)(i)(A)(2), "The 10^{-6} risk level shall be used as the point of departure for determining remediation goals for alternatives when ARARs are not available...". The 10^{-6} starting point indicates U.S. EPA's preference for setting cleanup levels at the more protective end of the acceptable 10^{-4} to 10^{-6} risk range for Superfund remedial actions. Site-specific and remedy-specific factors are then taken into consideration in the determination of where within the $10^{-4}\ \text{to}\ 10^{-6}\ \text{risk}$ range the cleanup standard for a given contaminant will be established. For the purposes of this evaluation, the risk-based cleanup levels which correspond to a 10^{-6} risk are calculated. Site-specific and remedy-specific factors which may affect the determination of the final cleanup level will be addressed in subsequent portions of this document.

Those surface soil contaminants which contribute an individual cancer risk of greater than 1 x 10^{-6} to the overall cancer risk estimate under the reasonable maximum exposure scenario for future residential use, as presented in the risk assessment portion of the Phase I RI Report (TRC, 1991), were evaluated to determine if there are any for which an ARAR/TBC has not been identified. Arsenic, beryllium, and PAHs drove the carcinogenic risk estimates associated with exposures to surface soil. Surface soil cleanup levels were calculated for these contaminants based on the 1 x 10^{-6} cancer risk, as presented in Table 4-2. As presented previously in Section 4.2.6, no

individual hazard index values greater than unity were calculated for noncarcinogens in the risk assessment presented in the Phase I RI Report (TRC, 1991). Therefore, no risk-based cleanup levels were calculated for noncarcinogens. Similarly, risks posed by subsurface contaminants did not exceed the point of departure (a 10^{-6} carcinogenic risk or a hazard index value of unity). Additional information used in the development of risk-based cleanup levels is presented in Appendix A.

The surface soil contaminant levels for each of the surface soil sample locations were compared to the risk-based cleanup levels presented in Table 4-2. PAHs (benzo(b/k)fluoranthene and chrysene) were detected in one surface soil sample, S8-3, at levels exceeding the risk-based cleanup levels (see Figure 4-4). Arsenic exceeded the risk-based cleanup level at sample locations S8-7 and S8-9 while beryllium exceeded the risk-based cleanup level at sample locations S8-1, S8-2, S8-3, S8-4, S8-7 and S8-8. It should be noted that for all SVOC analyses of surface soil samples, detection limits exceeded risk-based cleanup levels. Therefore, the identification of PAH levels exceeding risk-based cleanup levels has a degree of uncertainty associated with it since the detected levels are all estimated ("J" qualified) data.

As indicated in Table 4-2, the greatest calculated reasonable maximum exposure risk under the future residential use scenario presented for an individual compound is 2.6×10^{-6} . Therefore, calculated risk levels exceed 10^{-6} but fall within the acceptable risk range of 10^{-4} to 10^{-6} applicable to remedial actions.

4.3.3 Remedial Response Objectives

Based on the information presented above, as well as a consideration of potential ecological risks, the remedial action objectives for soil are as follows:

- Minimize current and future exposures to surficial soil contaminants at levels which exceed ARARs/TBCs, as presented in Table 4-1, or which pose unacceptable risks to human health and the environment; and
- Minimize off-site migration of surface soil contaminants.

4.4 General Response Actions

General response actions are those remedial actions which will satisfy the remedial objectives. General response actions for Site 08 were formulated based on the results of the Remedial Investigation.

The first step in determining appropriate general response actions for a given media is an initial determination of the areas or volumes to which the general response actions may be applied, as described below. In determining these volumes/areas of media, consideration has been given to site conditions, the nature and extent of contamination, acceptable exposure levels and potential exposure routes.

In preparing a preliminary estimate of the volume of soil potentially requiring treatment, the extent of soil requiring remediation must be defined. As previously presented in Section 4.3, final remediation limits will be dependent on the level of risk determined to be acceptable for the site.

Two remedial scenarios have been evaluated for Site 08. The first scenario involves remediation of soils which exceed current ARARs/TBCs and the 10^{-6} risk level. Under this scenario, almost all of the surface soils at Site 08 would require remediation due to the presence of PAHs, PCBs, arsenic and/or beryllium. The estimated areal extent of contamination is indicated in Figure 4-4. Based on a remedial area of 2,500 square feet and a surficial soil thickness of two feet, the estimated volume of soil requiring remediation under this scenario is 5,000 cubic feet or 185 cubic yards. If the top two

feet of soil were remediated, existing subsurface soil contaminant levels as defined in the Phase I RI would also exceed risk-based surface soil cleanup levels. By following soil removal with the placement of clean backfill potential exposures to contaminated subsurface soil would be addressed.

Under the second remedial scenario, only the soils which are contaminated at levels exceeding ARARs/TBCs would be remediated. Only surface soil sample S8-6 contained PCBs at a level exceeding the current RIDEM cleanup standard of 1 ppm. Assuming contamination extends beyond this sampling point approximately half the distance to adjoining sample locations (see Figure 4-3), the contaminated area covers 150 square feet. At a depth of 2 feet, the soil volume requiring remediation is 300 cubic feet or 11 cubic yards. It should be noted that this soil potentially would not require remediation under the proposed PCB limit of 10 ppm for solid wastes, which is included in RIDEM's Proposed Amendments to the Rules and Regulations for Solid Waste Management Facilities.

General response actions applicable to the remediation of soils under the two scenarios described above include the following:

- No Action
- Institutional Control
- Containment
- Treatment/Disposal

4.5 Identification and Screening of Technologies and Process Options

The general response actions are developed further through the identification and screening of remedial technologies which could potentially meet the remedial response objectives and cleanup criteria. Following a screening of the remedial technologies on the basis of technical implementability, the process options associated with each technology are

screened based on effectiveness, implementability and cost. Representative process options are chosen for inclusion in the remedial alternatives developed for the site.

4.5.1 Technology Screening

A combined technology screening was performed for all the sites addressed within this ISA. The technology screening for soils/sediments is presented in Table B-1 of Appendix B. The table includes brief descriptions of the individual technologies or process options, comments on their general applicability, limiting characteristics which prevent their application to certain sites, and a summary of whether they are screened or retained for the various sites. The technologies or technology process options which do not pass the screening process on the basis of technical implementability will not be retained for further consideration. In conducting the technology screening for soils at Site 08, technologies were evaluated for their technical ability to address PAHs, PCBs, and inorganic contaminants in surface soils, as well as their ability to be applied to the site-specific conditions at Site 08. Because Site 08 is very limited in areal extent, some technologies could not physically be employed on-site; these technologies were screened from further consideration. The technologies which were screened from further analysis at Site 08 include on-site landfilling, on-site incineration, mechanical/thermal aeration, soil washing, landfarming, slurry phase biodegradation, solvent extraction, in situ biodegradation, soil venting, radio frequency heating, in solidification/stabilization, situ vitrification, in situ and injection/vacuum extraction. Technologies and process options which passed the technology screening for Site 08 are summarized in Table 4-3.

4.5.2 Process Option Screening

those technologies which are technically identification of implementable, the process options are further evaluated to allow selection of a representative process option for each technology type. process options are evaluated on the basis of effectiveness, implementability, and cost. Process option evaluations for soil remediation are presented in Table B-2 of Appendix B. Because the main risks currently identified for Site 08 are associated with direct contact with or ingestion of contaminated surface soils, the process options associated with each technology were evaluated to determine their effectiveness in addressing this risk. considered in the process option screening were the very limited volumes of soil to be addressed at Site 08 (185 yd3 to meet both risk-based cleanup levels and ARARs/TBCs and 11 yd3 to meet only ARARs/TBCs), and the viability of mobilizing an on-site treatment system to remediate such limited volumes. For institutional control technologies, both deed restrictions and fencing were selected as representative process options. For the capping technology, a RCRA Subtitle D Soil Cap was determined to provide protection against exposures to contaminated surface soils while also being implementable and cost-effective. For excavation and disposal, off-site landfilling was the only process option retained for analysis. For excavation and treatment technologies, off-site incineration was selected to be a representative process option, while fungal degradation was selected as a representative in situ treatment process option. The selected treatment technologies could be readily applied to a limited soil volume. The selected representative process options are indicated with a bullet in Table 4-3.

4.6 Remedial Alternative Development

The technologies and process options developed in Section 4.5 are combined in this section to form remedial alternatives. The range of alternatives which is developed is intended to provide varying degrees of site cleanup. The alternatives presented herein have been developed consistent with criteria mandated by the National Contingency Plan (NCP, 40 CFR 300), as previously described in Section 3.8.

As indicated in Table 4-4, a total of four alternatives have been developed for addressing soil contamination at Site 08. These alternatives include a no action alternative (II-1), a limited action alternative (II-2), a containment alternative (II-3) and an active restoration alternative (II-4). Three treatment/disposal options were evaluated under Alternative II-4. Specifically, the alternatives include deed restriction/fencing (II-2), a RCRA Subtitle D soil cap (II-3), off-site landfill disposal (II-4, Option A), off-site incineration (II-4, Option B), and fungal enzyme degradation (II-4, Option C).

4.7 Definition and Preliminary Screening of Remedial Alternatives

Each of the alternatives listed in Table 4-4 for the Group II site are further defined and then undergo a preliminary screening in this section. The screening process was previously described in Section 3.9. Following the evaluation of individual alternatives, a comparative analysis is conducted between alternatives. Those alternatives that pass the preliminary screening process will be evaluated in the Detailed Analysis of Alternatives.

4.7.1 Alternative II-1 - No Action

4.7.1.1 Description

The no action alternative would involve no remedial response activities for soils at Site 08. No removal or treatment of surface soil would be conducted. No component of the no action alternative minimizes any potential risks that may be associated with direct contact with on-site contaminants. If unlimited future use of the site was determined to not be protective of human health, a review of the no action decision would be required under the NCP in five years. Consideration of the no action alternative is required under the NCP.

4.7.1.2 Evaluation

Effectiveness – The no action alternative would provide no reduction in the toxicity, mobility or volume of contaminants in site soil. However, based on the risk assessment conducted for this site, cancer risks under most current and future land use scenarios are less than 10^{-5} . Even under the future residential use scenario, the greatest risk posed by an individual contaminant under the reasonable maximum exposure scenario is within the acceptable risk range for remedial measures of 10^{-4} to 10^{-6} . The short-term risks would also be minimal due to the lack of activities associated with the implementation of this alternative.

Implementability - The no action alternative would require no implementation activities other than a five year review; therefore, it is easily implemented.

<u>Cost</u> - A nominal cost would be associated with the preparation of the 5-year review.

4.7.2 Alternative II-2 - Fencing and Deed Restrictions

4.7.2.1 Description

This limited action alternative would involve no removal or treatment of contaminated soil at Site 08, although it would include both the construction of a perimeter site fence and implementation of deed restrictions. A six-foot-high chain link fence would be placed around Site 08. Placement of hazard warning signs on the fence would also be included in this alternative. The proposed location of the fence is shown in Figure 4-5.

This limited action alternative would also include implementation of land use deed restrictions. These restrictions, which would limit allowable future site use and development, have been included to provide an added measure of long-term protection of human health through minimizing potential future exposures to contaminated site surface soil. The deed restrictions could limit future residential development of the site, thereby eliminating the future use scenario where the 10^{-6} risk level was exceeded (see Section 4.3.2).

In contrast to Alternative II-1, which was required to be considered by the NCP, this alternative has been developed to provide an increased level of protection of human health through fencing and land use restrictions although it involves no action to reduce the toxicity, mobility or volumes of contaminated surface soil on-site.

4.7.2.2 Evaluation

<u>Effectiveness</u> - This alternative would provide no reduction in the toxicity, mobility or volume of contaminated soils on-site. It would also provide no direct protection of human health or the environment. Through fencing and deed restrictions, it would limit potential exposures due to direct contact with and ingestion of contaminated surface soil and would limit

future site use. Maintenance of the perimeter fence and compliance with deed restrictions would be required to maintain the alternative's long-term effectiveness. However, due to the scheduled base closure, long-term maintenance and enforcement of this alternative could be difficult to implement. Minimal short-term risks would be associated with implementation.

Implementability - This alternative would involve the placement of land use deed restrictions on a property controlled by the federal government. Implementation of these deed restrictions should be relatively easy. The construction of the perimeter fence should not be difficult given the lack of active use of the majority of the site. Overall, this alternative would be easy to implement, although it may be difficult to enforce over the long-term due to scheduled base closure.

<u>Cost</u> - Costs associated with this alternative would be those associated with perimeter fence placement and maintenance, and the costs to establish land use restrictions.

The cost of this limited action alternative is initially estimated at a present worth value of \$4,200, assuming a 30-year maintenance period for the perimeter fence (see Appendix D).

4.7.3 Alternative II-3 - RCRA Subtitle D Soil Cap/Deed Restrictions

4.7.3.1 Description

This alternative was developed to meet the NCP's requirement for consideration of an alternative which utilizes containment with little or no treatment. Alternative II-3 incorporates the capping or covering of the site with a RCRA Subtitle D cap which would limit future exposures to surficial contamination and minimize erosion. The soil cap would consist of a minimum

18-inch infiltration layer topped by a minimum 6-inch erosion layer. The infiltration layer would be constructed to provide a permeability less than or equal to the natural subsoils or a permeability no greater than 1×10^{-5} cm/sec, whichever is less. The erosion layer would consist of a minimum of 6 inches of earthen material capable of sustaining native plant growth. Due to the limited areal extent of the cap and the main objectives of minimizing direct exposure to surface soil contamination and erosion, the RCRA Subtitle D cap design was selected.

The capping alternative would cover approximately 2,500 ft², covering the entire site. This area would be capped to cover surface soils which exhibited risks exceeding the 10⁻⁶ point of departure risk, as discussed in Section 4.4. It would also cap those soils which contain PCBs at a level which exceeds the current RIDEM cleanup standard. The proposed physical limits of the cap are shown on Figure 4-6. The soil cap would minimize potential risks associated with direct contact with contaminated surface soils and erosion.

In addition to the RCRA Subtitle D soil cap, deed restrictions would be placed on the site to limit future site use and development. The deed restrictions would aid in the long-term protection of human health by minimizing potential disruption of the cap and preventing future residential use of the site.

4.7.3.2 Evaluation

<u>Effectiveness</u> - Alternative II-3 would provide no reduction in the toxicity or volume of surface soil contaminants but it would be protective of human health and the environment by limiting exposure to surficial contamination and the potential migration of surficial contaminants due to erosion. The cap and deed restrictions would be effective in addressing the

area of concern, although they would require long-term maintenance to ensure continued effectiveness. Short-term effectiveness would be minimally impacted by the slight disruption of surficial materials required to cap the site. Protection would be achieved within a relatively short time frame.

Implementability - Alternative II-3 would be relatively easy to implement. It would require the construction of a soil cap. This activity employs commonly used and widely accepted construction equipment and techniques. The site is flat and covered with grass which minimizes the need for extensive site preparation. Administrative implementation of land use deed restrictions would be relatively easy to undertake given the present ownership of the site by the federal government. The overall implementability of Alternative II-3 is good.

<u>Cost</u> - The main cost associated with Alternative II-3 is that associated with the construction and long-term maintenance of the RCRA Subtitle D soil cap. An initial estimate of the present worth cost for Alternative II-3 is \$7,700 (see Appendix D).

4.7.4 Alternative II-4 - Soil Treatment/Disposal

4.7.4.1 Description

Alternative VI-4 consists of active site restoration, and includes the consideration of several treatment/disposal technologies for contaminated surface soil. This analysis is intended to provide the basis for a general comparison between Alternatives II-1, II-2, II-3 and II-4. Preliminary analyses of the effectiveness, implementability and costs of the individual treatment/disposal options considered are presented in Sections 4.7.5 through 4.7.7.

4.7.4.2 Evaluation

Effectiveness - For surface soils, Alternative II-4 would provide a reduction in the mobility or toxicity of soil contaminants through either excavation and disposal and treatment or through in situ treatment. It would provide for the remediation of the site to meet risk-based cleanup levels based on future residential use of the site or the remediation of surface soils which exceed federal or state ARARs/TBCs. The degree of toxicity reduction and the reliability of the remedial action (and, therefore, the long-term effectiveness) would be dependent upon the individual disposal or treatment technology selected. In general, by excavating and treating or disposing of the contaminated soils, the long-term effectiveness of this alternative would be considered greater than that of the previously evaluated minimal action and containment alternatives. effectiveness of those treatment options which require excavation would be impacted by the disruption of the soils during the excavation activities, but personnel protective measures could be taken during the removal to protect on-site workers and dust minimization controls could be used as necessary to minimize off-site migration of any airborne particulates. Removal activities could be completed within a relatively short time frame.

<u>Implementability</u> - Alternative II-4 is implementable, although its implementability would be highly dependent upon the individual technology option included in the alternative.

<u>Cost</u> - As with implementability, cost would be highly dependent upon the individual technology option included in the alternative. In general, Alternative II-4 would cost more than Alternatives II-1, II-2, and II-3 due to the active restoration activities involved in its implementation.

4.7.5 Alternative II-4 - Soil Treatment/Disposal, Option A - Off-Site Landfill

4.7.5.1 Description

This option would involve excavation and off-site transportation of soil to a suitable landfill. Disposal of contaminated soil at an off-site landfill would eliminate the need for long-term management of the soil on-site. Prior to landfilling, the excavated soil must be characterized to determine if it meets the definition of a hazardous waste and if it falls under land disposal restrictions. Federal land disposal restrictions (40 CFR Parts 261 and 268) prohibit the acceptance of certain waste types at landfills. Restricted waste types include solvent-, dioxin-, and California-list-contaminated soils and soils contaminated with listed or characteristic hazardous wastes. Soil samples were analyzed for TCLP parameters for the Phase I Remedial Investigation. Although no samples exceeded TCLP limits, a worst-case scenario will be assumed in which the excavated soil will be disposed of hazardous waste.

Based on these considerations, preliminary costs for this option have been prepared using the three scenarios described below.

Scenario 1 - All surface soils (185 cubic yards - see Figure 4-4 for areal extent) are excavated, transported, and disposed of at a secure hazardous waste landfill.

Scenario 2 - The PCB-contaminated surface soils (11 cubic yards - see Figure 4-3 for areal extent) are excavated, transported, and disposed of at a secure hazardous waste landfill.

Scenario 3 - Same as Scenario 2 but the remainder of the site is covered with a RCRA Subtitle D soil cap, as described in Section 4.7.3.1.

4.7.5.2 Evaluation

<u>Effectiveness</u> - Overall, the off-site landfill option described above provides for a reduction in the mobility, but not the volume or the toxicity

of contaminants. Off-site landfilling, a commonly employed waste management option, provides no treatment of contaminants. It would reduce the volume of contaminated soil on-site and would also tend to reduce the ultimate mobility of the contaminants through placement of the soil in a secure landfill. Protection of human health would be achieved by the removal of potential exposure pathways. Long-term effectiveness would be dependent on the long-term operating and maintenance procedures at the receiving landfill and, in the case of Scenario 3, on the long-term maintenance of the on-site cap. Due to the relatively low risks posed by the existing contamination, long-term effectiveness is expected to be good.

In minimizing residual risks, Scenario 1, disposal of all soils off-site, would be most effective, followed by Scenario 3 (off-site PCB disposal and capping) and Scenario 2 (off-site PCB disposal only).

In the short-term, exposures to remedial workers during soil excavation could be minimized through the use of appropriate health and safety equipment. No off-site impacts are anticipated in the short-term.

Implementability - Implementability of off-site landfill disposal would be directly related to the availability of a suitable landfill with adequate capacity to accept the type of material generated from the site. Soil can only be disposed of at the State's Central landfill if it is permitted to accept the material. Closure of the lined area of the landfill is scheduled for 1994. For Scenario 3, capping is easily implemented.

Cost - Factors which are considered in the cost evaluation of this alternative include the replacement and compaction of clean back-fill in excavated areas and the off-site disposal costs. The preliminary estimates for the cost of each of the disposal scenarios are:

Alternative II-4, Option A - Off-Site Landfill:

- Scenario 1 \$160,000
- Scenario 2 \$ 10,000
- Scenario 3 \$ 20,000

See Appendix D for preliminary cost estimates.

4.7.6 Alternative II-4 - Soil Treatment/Disposal, Option B - Off-Site Incineration

4.7.6.1 Description

This option provides for the transportation of the contaminated surface soil to an off-site facility for incineration. The alternative will eliminate or reduce the toxicity, mobility, and volume of the contaminated surface soil through thermal destruction. Off-site incineration would involve excavation and transportation of the soil to a suitable incinerator. Excavated soils would require drumming prior to off-site transport in accordance with incinerator acceptance requirements. This option would eliminate the need for long-term management of the soil on-site.

Three scenarios have been developed for Option B, as listed below:

Scenario 1 - All surface soil (185 cubic yards - see Figure 4-4 for areal extent) is excavated, transported to, and incinerated at a commercial incineration facility.

Scenario 2 - The PCB-contaminated surface soil (11 cubic yards - see Figure 4-3 for areal extent) is excavated, transported to, and incinerated at a commercial incineration facility.

 Scenario 3 - Same as Scenario 2 but remaining surface soils are covered with a RCRA Subtitle D soil cap, as described in Section 4.7.3.1.

4.7.6.2 Evaluation

Effectiveness - Option B would provide a reduction in the mobility, volume, and toxicity of contaminants. While incineration would destroy

organic materials, it does not destroy inorganic constituents. They would either volatilize in the incineration process or would remain in the ash which would require disposal in a landfill. Potential exposure pathways and associated site-related risks would be addressed by this alternative. Long-term effectiveness would depend on the degree of contaminant destruction achievable in the incinerator and the long-term operation and maintenance of the ash disposal facility. Both hazardous material incinerators and chemical waste landfill facilities are commonly utilized waste management options. Because this alternative utilizes off-site treatment, it is appropriate for the minimal volumes of soil to be treated at Site 08. In minimizing residual risks, Scenario 1, off-site incineration of all soils, would be more effective than Scenario 3, incineration of PCB-contaminated soils and capping or Scenario 2, off-site incineration of PCB-contaminated soils. effectiveness would be affected by exposure to the surface soil during excavation and drumming activities. In the short-term, exposures to remedial workers during soil excavation could be minimized through the use of appropriate health and safety equipment. No off-site impacts are anticipated in the short-term.

Implementability - Off-site incineration would be relatively easy to implement. Several commercial incinerators can accept the type of waste from Site 08. The volume of contaminated surface soil is small, simplifying the excavation, packaging, and transportation of the soil. Due to incinerator demand and capacity limitations, delays in the incinerator's acceptance of the waste for treatment are possible.

<u>Cost</u> - The main costs associated with the incineration of soils at Site 08 relate to the excavation, transportation, and incineration of the surface soil. An estimate of the costs for each scenario is provided below.

- Scenario 1 \$1,200,000
- Scenario 2 \$ 74,000
- Scenario 3 \$ 84,000

Costs associated with the various options of Alternative II-5 are presented in Appendix D.

4.7.7 <u>Alternative II-4 - Soil Treatment/Disposal, Option C - Fungal Enzyme</u> Degradation

4.7.7.1 Description

This alternative utilizes fungal enzyme degradation to treat surface soil contaminants. Enzymes produced by various forms of fungi have the ability to degrade many hazardous organic compounds via an oxidation reaction. End products are simple compounds, primarily CO₂ and H₂O, leaving free radicals such as chlorine to evolve or combine in very low concentrations. While bacteria degrade contaminants by producing enzymes which break down the bonds between elements in a carbon chain, the enzymes are typically specific to certain organic compounds and are intracellular, requiring that the contaminants be soluble enough to enter the bacterial cell for degradation to occur. The enzymes produced by fungi, however, are often non-specific and extracellular. Therefore, they are more effective in treating a greater range of contaminants and the fungi need only to be in close proximity to the contamination to be effective (Hicks, 1992). This alternative meets the NCP criterion for the consideration of an innovative treatment alternative.

Since the contamination at Site 08 is limited to the surface soil, the technology would be applied in-situ. Fungal enzymes would be produced on a solid substrate or as a dry fungal powder and introduced into the contaminated soil along with soil conditioners, if necessary. Treatment can be conducted in situ or in above ground treatment cells. Fungi are naturally occurring

microorganisms which are non-toxic, and are selected by screening various isolated strains for optimum contaminant degrading properties. While the actual treatment may be inexpensive, the development of an optimal, site-specific treatment methodology may be expensive.

The technology would primarily apply to the PCB contamination at Site 08 and could potentially provide some treatment of PAHs. It would not address the inorganic contamination. One scenario exists for this treatment; the PCB-contaminated surface soil (11 cubic yards) would be treated with white-rot fungal enzymes.

4.7.7.2 Evaluation

Effectiveness - Option C is expected to provide protection of human health through a reduction in the toxicity of surface soil contaminants. The treatment process, if effective, would reduce the contaminants to simple compounds. The time required to meet cleanup objectives is difficult to estimate. Treatability studies would be required to determine if a site-specific fungal strain would need to be developed. In historic applications at other sites, order-of-magnitude reductions in contaminant concentrations have been achieved within a period of three to eight weeks (Mycotech Corporation, 1992). Fungal degradation is an innovative technology and, therefore, its reliability in achieving the cleanup level objectives is not well proven. In the short-term, risks posed by application of the fungal powder and conditioners to the contaminated soils could be minimized through the use of proper personnel protection equipment.

<u>Implementability</u> - Option C could be somewhat difficult to implement. Studies must be conducted to determine the optimum treatment methodology for the site. The ability to produce or manufacture sufficient quantities of

fungi for wide-scale use is currently under development; therefore, the availability of the fungi may be limited. The actual implementation of the technology is relatively easy, with the fungal substrate introduced to the soil with a roto-tiller or similar machine. No excavation or off-site transportation is necessary.

<u>Cost</u> - The main cost related to Option C is the cost for the development of the specific fungal enzyme and associated treatability studies. Due to its innovative nature, no cost data were available for this treatment option.

4.8 Selection of Alternatives for Detailed Analysis

A comparative analysis of the individual alternatives based on the three evaluation criteria is conducted to allow the elimination of selected alternatives from the detailed analysis process.

4.8.1 Effectiveness

Those alternatives which provide protection of human health and the environment, and which involve reductions in the toxicity, mobility or volume of contamination and contaminant sources, thereby decreasing the inherent risks associated with the hazardous material, typically provide the greatest long-term effectiveness. With respect to short-term effectiveness, those alternatives which are protective during the construction and implementation period and which achieve remedial response objectives within a timely manner are most effective. The ability of an alternative to handle the contaminated media and its reliability are also considered in the effectiveness analysis.

A significant consideration in the evaluation of long-term effectiveness for soil remedial alternatives at Site 08 is the potential risk to human health and the environment posed by the site. Estimated risks under the

future residential use scenario are on the order of 10^{-5} , and, therefore, fall within the acceptable risk range for remedial actions under the requirements of the NCP. Considering the adjacent warehouse structures, the most probable future use of Site 08 is industrial; therefore, remediation of the site to a 1×10^{-6} risk-based cleanup level based on future residential use may not be appropriate. Additional assessment of potential environmental receptors and the risks the site may pose to them will be conducted as part of the Phase II RI.

Potential risks associated with the presence of PCBs at one surface soil sample location at a level greater than 1 ppm must be considered. The risk assessment identified no significant risks associated with the presence of the PCBs, but the detected PCB level of 1.4 ppm slightly exceeds the historic RIDEM cleanup standard, providing the basis for the evaluation of remedial options for treating the associated area of soil contamination. TSCA cleanup levels, which are not applicable but may be relative and appropriate, were not exceeded at Site 08. Also to be considered is the proposed RIDEM definition of solid waste as including soils with concentrations of PCBs greater than 10 ppm (proposed Amendments to the Rules and Regulations for Solid Waste Management Facilities). The existing PCB levels at Site 08 are less than this proposed definition and, therefore, potentially may not meet the definition of a solid waste.

When evaluating the soil remedial alternatives based on reductions in the toxicity, mobility or volume of contamination, Alternative II-4, soil treatment/disposal, provides the greatest long-term effectiveness, due to the excavation and treatment/disposal of contaminated soils. Due to the required disruption of the contaminated soils, implementation of this alternative results in increased short-term effects which can be controlled through proper

personnel protection measures and construction techniques. Alternative II-4, Option A, off-site landfilling, and Option B, soil incineration, would remediate the site such that residual risk levels would be less than 1 x 10^{-6} under the future residential use scenario (for reasonable maximum exposures) and unlimited future development of the site could occur. Both of these alternatives are reliable and effective in treating the identified volumes of soil contamination. Option C, fungal degradation, is expected to provide treatment of PCB-contaminated soils but may not treat PAH contaminants and will not address inorganic contaminants. Therefore, it could provide compliance with state and federal ARARs/TBCs but may not achieve 1 x 10^{-6} risk-based cleanup levels under the future residential use scenario. Due to the fact that fungal degradation is a developing technology, it may not be as reliable or effective as the other treatment technologies evaluated.

Alternative II-3, RCRA Subtitle D soil cap/deed restrictions, provides the next level of long-term effectiveness by reducing the risks associated with direct contact with contaminated surface soils. It could have short-term impacts due to possible contact with surface soil during cap construction, although these impacts could be minimized through the use of appropriate personnel protection equipment. Capping would be an effective means of handling the contaminated media and would be effective in the long-term, providing it is maintained.

Alternative II-2, no action with fencing and deed restrictions, would also provide long-term effectiveness through the limitation of potential exposures to soil contamination through fencing and deed restrictions, although long-term maintenance and enforcement would be required. Short-term impacts associated with fence construction are minimal. Alternative II-1, no action, does not meet the point of departure risk level of 1 x 10^{-6} for future

residential use but could potentially be considered to be protective of human health and the environment under other future use scenarios.

4.8.2 Implementability

Implementability is a measure of the technical and administrative feasibility of constructing, operating, and maintaining a remedial action alternative. Alternative II-1, no action, is the most implementable remedial alternative from a construction standpoint due to the lack of implementation activities associated with it. Alternative II-2, limited action, is also fairly readily implemented involving only limited construction activities (i.e., installation of fencing) and implementation of deed restrictions. However, maintenance of this alternative over the long-term would be complicated by the scheduled base closure. Alternative II-3, RCRA Subtitle D soil cap/deed restrictions, is next in terms of implementability based on the relatively simple nature of the proposed cap construction, but it too would require long-term maintenance. Alternative II-4, excavation and treatment/ disposal or in situ treatment of surface soils is the most complicated alternative to implement, requiring excavation and off-site treatment or disposal, or on-site treatment, but has minimal long-term maintenance requirements. Of the treatment options, off-site landfilling, Option A, is the most implementable, followed by Options B, (off-site incineration), and C (fungal enzyme degradation).

4.8.3 <u>Cost</u>

Alternative II-1, no action, is the lowest cost alternative. Alternative II-2, limited action, and the containment alternative, Alternative II-3, are comparable, with costs ranging from \$4,200 to \$7,700. The excavation and

treatment/disposal of surface soil (Alternative II-4) costs are typically the most expensive, ranging from \$10,000 to \$1,200,000 for the various treatment/disposal options. Due to its innovative nature, no costs were available for the fungal degradation option.

4.8.4 Selection of Alternatives for Further Consideration

Based on the comparative analysis presented in the previous section, as well as the individual alternative/option analyses presented in Sections 4.7.1 through 4.7.7, no alternatives are proposed to be eliminated from the range of alternatives undergoing detailed analysis.

The remaining alternatives and technology options will be retained for detailed analysis. This will allow for the further consideration of a wide variety of remedial options providing a range in the degree of treatment for the various media at the site.

However, further evaluation of the applicability of the calculated risk-based cleanup levels in determining the area of remediation is recommended. This recommendation is based on the uncertainties associated with the calculation of the risk-based cleanup levels and the applicability of the calculated risk-based cleanup levels to Site 08. These uncertainties impact the effectiveness evaluation with respect to the ability of the alternatives to meet the cleanup level objectives and to provide greater protection of human health and the environment.

PAHs, arsenic and beryllium were detected in surface soils at Site 08 at levels exceeding risk-based cleanup levels. With respect to PAHs, as noted previously in Section 4.3.2, in all SVOC analyses of surface soil samples at Site 08, detection limits exceeded the calculated risk-based cleanup levels for PAHs. Therefore, the area which has been identified as containing PAHs at

levels exceeding risk-based cleanup levels was identified on the basis of qualified data (i.e., samples where PAHs were detected at J-qualified or estimated levels). For the arsenic and beryllium, the calculated risk-based cleanup levels are less than the geometric mean concentration for background soils in the eastern U.S. (USGS, 1984). The presence or absence of PAHs in surface soils and site-specific background soil concentrations require further definition, as will be done in the Phase II RI, before the applicability of the calculated risk-based cleanup levels can be further evaluated.

5.0 GROUP III SITES - SITE 12 - BUILDING 316, DPDO TRANSFORMER OIL SPILL AREA, SITE 14 - BUILDING 38, TRANSFORMER OIL LEAK AREA

5.1 Introduction

Group III Sites consist of Site 12 - Building 316, DPDO Transformer Oil Spill Area, and Site 14 - Building 38, Transformer Oil Leak Area. The following sections provide a site description, summary of remedial response objectives and cleanup criteria, general response actions, identification and screening of technologies and process options, remedial alternative development, and preliminary screening of remedial alternatives.

5.2 Site 12 - Building 316, DPDO Transformer Oil Spill Area

5.2.1 Site Location and Description

Site 12, located within Building 316, contained the Defense Property Disposal Office. This building, situated between Buildings 317 and 315, was used to store electrical transformer units. Site 12 is located in a region called West Davisville, located west of the CBC Davisville Main Center. Site 12 is bordered to the west by Conrail tracks, to the east by Mike Road, and to the south by a gravel road. A site location map is provided in Figure 5-1.

5.2.2 Site History Overview

In 1977, a transformer containing PCB oil was accidentally punctured with a forklift in Building 316. The spill area on the concrete floor was contained and cordoned off, and the spill was cleaned up by NCBC-Davisville personnel. In October 1984, as a result of recommendations within the IAS, NCBC personnel collected composite concrete samples from the oil spill area for PCB analysis. The results indicated the presence of PCB contamination in the concrete (Aroclor 1260 at 91 ppm). In March 1986, additional samples were collected from the spill area as part of the Confirmation Study (CS). Fifteen

wipe samples were collected from the spill area for PCB analysis. The laboratory analysis detected concentrations of Aroclor 1254 in the wipe samples ranging from 0.4 to 3.0 μ g/sq. in.

A remedial action was conducted in early 1991 which involved the removal and disposal of PCB-contaminated concrete and subgrade materials from the floor in Building 316. The removal area consisted of a concrete pavement area approximately 20 feet square and a contiguous area approximately 4 feet by 5 feet (see Figure 5-2). The pavement consisted of a six-inch concrete slab. The pavement plus six inches of subgrade were removed. In April, TRC conducted post-removal verification sampling in order to confirm and document the decontamination of the area. The sampling included the collection of concrete chip samples, wipe samples, soil samples and associated quality control (QC) samples. Four concrete chip samples and two wipe samples were collected around the perimeter of the excavation, and four soil samples were collected within the excavation area. The soil samples were collected from a depth of 0- to 2-inches below grade while the chip samples were collected from a depth of approximately 0- to 1/2-inch below grade. Wipe sample W-1 was collected off of a column adjacent to the excavation while wipe sample W-2 was collected off of the concrete floor outside of the excavation area. Sampling locations and detected PCB concentrations are indicated in Figure 5-3. Chip samples collected from the concrete surface surrounding the removal area exhibited PCB concentrations ranging from 2.3 to 5.9 ppm.

In September 1991, the U.S. EPA conducted additional sampling at Building 316 to further define the horizontal extent of PCB-contaminated concrete flooring. Chip samples were collected from the area surrounding the removal area, with the objective being to collect samples at locations successively further from the removal area perimeter in each direction until two

consecutive chip sample results were less than 1 μ g/g (ppm) PCBs. Chip sample locations are indicated in Figure 5-4. The chip samples were screened in the field to provide identification of PCB contamination. Quantitation was conducted in accordance with the objective of the sampling. For example, if a sample analysis indicated a PCB concentration much greater than 1 μ g/g, instead of diluting and re-running the sample to get a quantitation peak on-scale, quantitation was performed on a secondary (less intense) on-scale peak. While the secondary peak quantitation can result in reported values lower than the true values, the project objective of identifying areas with concentrations greater than 1 μ g/g was still achieved.

5.2.3 Summary of Contamination

The confirmation sampling conducted following concrete removal activities indicated that residual PCB contamination remains. The analytical results of TRC's April 1991 sampling were presented in a letter report submitted to the U.S. EPA by the U.S. Department of the Navy on June 11, 1991. The analytical results of the U.S. EPA's September 1991 sampling were presented in a letter report submitted to the U.S. Department of the Navy by the U.S. EPA on October 22, 1991. PCB levels as great as 1200 µg/g were measured in chip samples collected from the remaining concrete materials. In general, the majority of the remaining contamination was detected in samples collected south of the removal area. Since the U.S. EPA sampling encompassed the extent of the TRC sampling effort, the measured contaminant levels from the U.S. EPA sampling program are indicated in Figure 5-4.

5.2.4 Summary of Contaminant Fate and Transport

PCBs tend to adsorb to organic matter and will volatilize into the atmosphere. Most available fate and transport information regarding PCBs is

relative to their presence in water, sediments or the atmosphere, not relative to their presence adsorbed to concrete. However, concrete's porous nature tends to result in the absorption of PCBs and their long-term retention. Principal transport mechanisms could be through volatilization or tracking off-site.

5.2.5 Summary of Human Health and Environmental Risk

No human health or environmental risk assessment has been conducted for Site 12. The building is currently locked and not in use. The contaminated areas within the building are identified by perimeter taping. Any future use of the building would most likely be industrial. Potential human exposure routes include dermal absorption or inhalation.

5.3 Site 14 - Building 38, Transformer Oil Leak Area

5.3.1 Site Location and Description

Site 14, located within Building 38, represents an area where electrical transformers were stored. Prominent features near Site 14 include railroad tracks (federally owned) and Davisville Road to the north, Davol Pond to the east, and Site 6 (Solvent Disposal Area) to the south. A site location map is provided in Figure 5-5.

5.3.2 Site History Overviews

In 1981, oil spillage was noted in warehouse Building 38 where electrical transformers were stored. The events surrounding the spill are unknown. The spill on the asphalt floor of the building is believed to have been cleaned up by NCBC-Davisville personnel as directed by the Northern Division Naval Facilities Engineering Command. No written report of any cleanup action is available.

In October 1984, as a part of the IAS, NCBC personnel collected composite asphalt samples from the oil spill area in the building for PCB analysis. sample analysis results indicated the presence of PCB contamination in the asphalt within the spill area (Arclor 1260 at 6690 ppm). In March 1986, under the CS, fifteen wipe samples were collected from the spill area for PCB analysis. The wipe sample analysis results indicated the presence of Arclor 1260 at concentrations ranging from 0.7 to 17,000 µg/sq. in. In early 1991, PCB-contaminated asphalt materials were removed from the floor of Building The removal area consisted of an asphalt pavement area approximately 40 feet by 17 feet in area, and a contiquous area approximately 5 feet square (see Figure 5-6). The pavement consisted of three inches of asphalt. pavement plus six inches of subgrade were removed. In April 1991, conducted post-removal verification sampling to confirm the complete removal of PCB-contaminated media from the site. The sampling included the collection of asphalt chip samples, wipe samples, soil samples and associated quality control (QC) samples. Three asphalt chip samples were collected around the perimeter of the excavation, and five soil samples were collected within the excavation area. Two wipe samples were collected from the asphalt floor outside of the excavation area. The soil samples were collected from a depth of 0- to 2-inches below grade while the chip samples were collected from a depth of approximately 0- to 1/2-inch below grade. Sample locations and detected PCB concentrations are indicated in Figure 5-7. Chip samples collected from the asphalt surface surrounding the removal area exhibited PCB concentrations ranging from 1.9 to 56 ppm.

In September 1991, the U.S. EPA conducted additional sampling at Building 38 to further define the horizontal extent of PCB-contaminated asphalt flooring. Initially, asphalt surface wipe samples were collected at 5-foot intervals around the perimeter of the removal area, with additional wipe

samples to be collected further from the removal area in each direction until the wipe sample results were less than 10 micrograms per 100 square centimeters (10 μ g/100 cm²). Where wipe samples were less than 10 μ g/100 cm², a surface chip sample would be collected. Chip samples would then be collected at locations successively further from the removal area perimeter in each direction until two consecutive chip sample results were less than 1 μ g/g PCBs. When preliminary screening results from the chip samples indicated that there was poor correlation between the wipe sample results and the chip sample results, the wipe sampling was discontinued. Wipe sample locations are indicated in Figure 5-8 and chip sample locations are indicated in Figure 5-9.

As discussed previously in Section 5.2.3, the wipe and chip samples were screened in the field to provide identification of PCB contamination. Quantitation was conducted in accordance with the objective of the sampling. While the reported values could, in some cases, be lower than the true values, the project objective of identifying areas with concentrations greater than 1 $\mu g/g$ was achieved.

5.3.3 Summary of Contamination

The confirmation sampling conducted following concrete removal activities indicated that residual PCB contamination remains. The analytical results of TRC's April 1991 sampling were presented in a letter report submitted to the U.S. EPA by the U.S. Department of the Navy on June 11, 1991. The analytical results of the EPA's September 1991 sampling were presented in a letter report submitted to the U.S. Department of the Navy by the U.S. EPA on October 22, 1991. PCB levels as great as 150 μ g/g were measured in the remaining asphalt flooring. In general, contamination was detected along the traffic lane which connects the access doors of the building and to the northwest and west of the

removal area. The measured contaminant levels are indicated at the sample locations in Figures 5-8 and 5-9 for the wipe sampling and chip sampling, respectively.

5.3.4 Summary of Contaminant Fate and Transport

PCBs tend to adsorb to organic matter and will volatilize into the atmosphere. Most available fate and transport information regarding PCBs is relative to their presence in water, sediments or the atmosphere, not relative to their presence adsorbed to concrete. However, the porous nature of asphalt as well as its organic constituents tends to result in the absorption of PCBs and their long-term retention. Principle transport mechanisms could be through volatilization or tracking off-site.

5.3.5 Summary of Human Health and Environmental Risk

No human health or environmental risk assessment has been conducted for Site 14. The building is currently locked and not in use. The contaminated areas within the building are identified by perimeter taping. Any future use of the building would most likely be industrial.

5.4 Summary of Remedial Response Objectives and Cleanup Criteria

Remedial response objectives are developed in order to set goals for protecting human health and the environment early in the alternative development process. The goals should be as specific as possible but should not unduly limit the range of alternatives that can be developed. For the Group III Sites, Site 12 and Site 14, the results of the verification sampling conducted by TRC and the U.S. EPA after the removal action was completed have been used to define potential remedial response objectives based on ARARS/TBCs.

5.4.1 Comparison of Contaminants to ARARs/TBCs

In evaluating building surface and soil contaminant levels, state and federal standards and guidance were used as ARARs/TBCs. For PCBs, regulations (40 CFR 761.120) developed under the Toxic Substances Control Act (TSCA) are not applicable to site contamination since they apply only to spills occurring after May 4, 1987, but cleanup levels specified under 40 CFR 761.125 may be relevant and appropriate to remediation of Sites 12 and 14. These regulations specify cleaning of indoor solid surfaces to 10 µg/100 cm² and remediating soils to 10 ppm by weight for spills in nonrestricted areas. The spills at Sites 12 and 14 responsible for the detected contamination occurred in 1977 and 1981, respectively. Spills occurring before May 4, 1987 are considered existing or old spills for which EPA establishes cleanup standards on a "case-by-case" basis. However, for comparison purposes, the specified cleanup levels will be used. RIDEM has historically applied a cleanup standard of 1 ppm to PCB spills. Rhode Island's Proposed Amendments to the Rules and Regulations for Solid Waste Management Facilities define solid wastes as including wastes which contain a concentration of 10 ppm or greater PCBs or 2 µg/100 cm² or greater. The Proposed Amendments to the Rules and Regulations of Hazardous Waste Management define Type 6 - extremely hazardous waste as including wastes which contain a concentration of 50 ppm or greater PCBs or 10 μ g/100 cm² as measured by a standard wipe test.

For Site 12, numerous site-wide concrete chip samples exceeded a 1 ppm standard and TRC wipe samples exceeded the 2 μ g/100 cm² proposed RIDEM solid waste level and the 10 μ g/100 cm² TSCA level and proposed RIDEM hazardous waste level in the area immediately adjacent to the previous excavation area. U.S. EPA concrete chip sample locations, which cover a greater extent of the Site 12 floor surface area than the TRC samples, and their detected concentrations are shown in Figure 5-4. Numerous asphalt chip samples also

exceeded the 1 ppm historic cleanup level at Site 14 and U.S. EPA and TRC wipe samples exceeded the 2 μ g/100 cm² RIDEM solid waste level and the 10 μ g/100 cm² TSCA and proposed RIDEM hazardous waste level. U.S. EPA asphalt chip and wipe sample locations also cover a greater extent of the Site 14 floor surface area than TRC samples, and their detected concentrations are shown in Figures 5-8 and 5-9, respectively.

The RIDEM historic cleanup standard of 1 ppm was considered in evaluating soil directly below building flooring. In TRC sampling and analysis, no soil samples at Site 12 and one soil sample at Site 14 exceeded this standard.

Tables 5-1 and 5-2 present a comparison of the maximum detected PCB levels in soil, wipe or chip samples to associated ARARs/TBCs for Sites 12 and 14, respectively.

5.4.2 Remedial Response Objectives

Based on the information presented above, the remedial response objective for Sites 12 and 14 is as follows:

 Prevent exposures to PCB-contaminated surfaces and soils at Buildings 316 and 38 at levels which exceed ARARs/TBCs, as presented in Tables 5-1 and 5-2.

5.5 General Response Actions

General response actions are those remedial actions which will satisfy the remedial objective. The first step in determining appropriate general response actions for a given media is an initial determination of the areas or volumes to which the general response actions may be applied, as described below. In determining these volumes/areas of media, consideration has been given to site conditions, the nature and extent of contamination, acceptable exposure levels and potential exposure routes.

In preparing a preliminary estimate of the volume of media potentially requiring treatment at the Group III sites, the extent of media requiring remediation must be defined. The remediation of PCB-contaminated concrete from Site 12 and PCB-contaminated asphalt and soil from Site 14 will be considered together. Two remedial scenarios have been developed for the Group The first scenario involves remediation of surface materials and soils with PCB concentrations greater than 1 ppm, the historic RIDEM cleanup standard, and the second scenario involves the remediation of surface materials and soils with PCB concentrations greater than 10 ppm or 2 $\mu g/100$ cm², the proposed RIDEM solid waste definition levels and the TSCA 10 ppm and 10 μg/100 cm² requirements for decontaminating spills in nonrestricted areas. Wipe samples collected by TRC and U.S. EPA at Site 14 generally fell within the limits of the more extensive chip sampling conducted by U.S. EPA. area exhibiting 10 ppm or greater PCBs in chip samples at this site encompasses those areas where PCBs were detected in wipe samples at concentrations equal to or greater than the proposed RIDEM solid waste level of 2 ug/100 cm². Since wipe sampling was abandoned by U.S. EPA during their field sampling efforts due to the relative lack of coordination between wipe sample results and chip sample results, only chip sample results were available for use in determining the general remediation area at Site 12.

In developing estimates of areas and volumes of materials requiring remediation, it was assumed that contamination is generally limited to the flooring material (the concrete or asphalt) and has not permeated the floor to contaminate subgrade materials. Confirmatory sampling conducted during the remedial action could verify this assumption. For removal actions, removal of the top six inches of subgrade has been included to address any subgrade contamination which could occur during the floor removal activities.

The areas or volumes of media which would require remediation under the first scenario (remediation to meet the historic RIDEM 1 ppm cleanup standard) are as follows:

• At Site 12, based on existing sampling results, the estimated areal extent of contamination exceeding a 1 ppm standard is illustrated on Figure 5-10. The contaminated area is estimated to cover approximately 13,000 ft². Based on a 6-inch thick concrete slab thickness, the volume of concrete requiring remediation is approximately 240 yd³. For removal actions in which contamination of underlying soil could result, it has been assumed that the top 6 inches of subgrade also requires remediation. Therefore, an additional 240 yd³ of soil would also be remediated. At Site 12 one chip sample collected by U.S. EPA contained 1,200 ppm PCBs, which exceeds the land disposal restriction level for total halogenated organics (HOC) of 1,000 ppm. Therefore, it is estimated that an area of 1,000 ft² exceeds this level, and of the total volume of concrete to be remediated, approximately 19 yd³ will fall under land ban restrictions.

At Site 14, the estimated asphalt surface area which is contaminated with PCBs at a level exceeding 1 ppm is approximately 15,000 $\rm ft^2$, as indicated on Figure 5-11. Based on an asphalt thickness of 3 inches, the volume of asphalt requiring remediation is estimated at 140 $\rm yd^3$. For removal actions in which contamination of the underlying subgrade could result, it has been assumed that the top 6 inches of subgrade also requires remediation. Therefore, an additional 280 $\rm yd^3$ of soil would be remediated. No samples collected at Site 14 exceeded the 1,000 ppm total HOC land ban restriction level.

At Site 14, one soil sample collected from the area in which asphalt pavement has already been removed exhibited a concentration of PCBs at 1.6 ppm, which exceeds the RIDEM 1 ppm cleanup level. The total volume of soil associated with this sample which will require remediation is estimated to be $4~\rm yd^3$.

The areas or volumes of media which would require remediation under the second scenario (remediation of materials at or exceeding the 10 ppm and 2 μ g/100 cm² proposed RIDEM solid waste levels and TSCA 10 μ g/100 cm² remediation level for nonrestricted areas) are provided below.

• At Site 12, based on existing sampling results, the estimated areal extent of contamination at or exceeding a 10 ppm or 2 μ g/100 cm² standard is illustrated on Figure 5-10. The contaminated area is estimated to cover approximately 1,750 ft². Based on a 6-inch

thick concrete slab thickness, the volume of concrete requiring remediation is approximately 32 yd 3 . For removal actions in which contamination of underlying soil could result, it has been assumed that the top 6 inches of subgrade also requires remediation. Therefore, an additional 32 yd 3 of soil would also be remediated. As previously discussed above, one chip sample at Site 12 contained 1,200 ppm PCBs, which exceeds the land disposal restriction level for total halogenated organics (HOC) of 1,000 ppm. Therefore, it is estimated that an area of 1,000 ft 2 exceeds this level, and of the total volume of concrete to be remediated, approximately 19 yd 3 will fall under land ban restrictions.

At Site 14, the estimated asphalt surface area which is contaminated with PCBs at a level at or exceeding 10 ppm or 2 µg/100 cm² is approximately 3,000 ft², as indicated on Figure 5-11. Based on an asphalt thickness of 3 inches, the volume of asphalt requiring remediation is estimated at 28 yd³. For removal actions in which contamination of the underlying subgrade could result, it has been assumed that the top 6 inches of subgrade also requires remediation. Therefore, an additional 55 yd³ of soil would be remediated. No samples collected at Site 14 exceeded the 1,000 ppm total HOC land ban restriction level.

A listing of general response actions developed for the remediation of building surfaces is provided below.

Building Media:

- No Action
- Institutional Control
- Removal
- Decontamination

Because remediation of soil is addressed only under flooring material removal actions and, in the case of the first remedial scenario, also includes the removal of a very limited amount of soil in the previous remedial area at Site 14, an analysis of general response actions and remedial technologies will not be conducted for soils. It is proposed that the PCB-contaminated soil be disposed of at a TSCA-permitted off-site landfill. In the case of flooring material removal actions, this would be consistent with the flooring remedial action. For other remedial actions evaluated under the first remedial scenario, remediation of the limited volume of soil (4 yd³) in the

previous removal area at Site 14 does not justify a detailed analysis of soil remedial technologies. Most treatment technologies could not cost-effectively be implemented based on this limited soil volume.

5.6 Identification and Screening of Technologies and Process Options

The general response actions are developed further through the identification and screening of remedial technologies which could potentially meet the remedial response objectives and cleanup criteria. Following a screening of the remedial technologies on the basis of technical implementability, the process options associated with each technology are screened based on effectiveness, implementability and cost. Representative process options are chosen for inclusion in the remedial alternatives developed for the sites.

5.6.1 Technology Screening

A combined technology screening was performed for all the sites addressed within the ISA. The technology screening for building surfaces is presented in Table B-5 of Appendix B. The table includes brief descriptions of the individual technologies or process options, comments on their general applicability, limiting characteristics which prevent their application to certain sites, and a summary of whether they are screened or retained for the various sites. The technologies or technology process options which do not pass the screening process on the basis of technical implementability will not be retained for further consideration. In conducting the technology screening for PCB-contaminated materials at Sites 12 and 14, technologies were evaluated for their technical ability to address PCBs in building materials and soils, as well as their ability to be applied to the site-specific conditions at

Sites 12 and 14. The technologies which were screened from further analysis at Sites 12 and 14 include grit blasting and acid etching, both of which are limited in terms of the depth of contamination which they can remove. Technologies and process options which passed the technology screening for Site 12 and Site 14 are summarized in Table 5-3.

5.6.2 Process Option Screening

identification technologies which are technically Upon of those implementable, the process options are further evaluated to allow selection of a representative process option for each technology type. process options are evaluated on the basis of effectiveness, implementability, and cost. Process option evaluations for building surfaces are presented in Table B-6 of Appendix B. The process options associated with each technology were evaluated to determine their effectiveness in addressing the potential risks associated with the presence of PCB contamination of the building materials at Sites 12 and 14. Also considered in the process option screening were the impacts on future site use. For institutional control technologies, both deed and access restrictions were selected as representative process options. For physical removal technologies, floor removal was selected over entire building demolition due to the potential for re-use of the structure following remediation. For treatment technologies, surface sealing and solvent washing were selected as representative process options which could be effective in treating the contamination while also being implementable and allowing for future site re-use. The selected representative process options are indicated with a bullet in Table 5-3.

5.7 Remedial Alternative Development

The technologies and process options developed in Section 5.6 are combined in this section to form remedial alternatives. The range of alternatives which is developed is intended to provide varying degrees of site cleanup. The alternatives presented herein have been developed consistent with criteria mandated by the National Contingency Plan (NCP, 40 CFR 300), as previously described in Section 3.8.

As indicated in Table 5-4, a total of five alternatives have been developed for addressing building surface contamination at Sites 12 and 14. These alternatives include a no action alternative (III-1), a limited action alternative (III-2), a containment alternative (III-3), removal action alternative (III-4), and a decontamination alternative (III-5). Specifically, the remedial alternatives include deed restriction/access restrictions (III-2), sealing (III-3), floor removal with subsequent disposal/incineration (III-4), and solvent washing (III-5).

5.8 Definition and Preliminary Screening of Remedial Alternatives

Each of the alternatives listed in Table 5-4 undergo a preliminary screening in this section. The screening process was previously described in Section 3.9. Following the evaluation of individual alternatives, a comparative analysis is conducted between alternatives. Those alternatives that pass the preliminary screening process will be evaluated in the Detailed Analysis of Alternatives.

5.8.1 Alternative III-1 - No Action

5.8.1.1 Description

The no action alternative would involve no remedial response activities for PCB-contaminated surfaces and soil at the Group III sites. No removal or

treatment of contaminated surfaces or soil would be conducted. Potential risks associated with direct contact with PCB contamination are not addressed by this alternative. Due to the presence of contamination which does not allow for unlimited future use, a review of the no action decision would be conducted in five years. Consideration of the no action alternative is required under the NCP.

5.8.1.2 Evaluation

Effectiveness - The no action alternative would provide no reduction in the toxicity, mobility or volume of PCB-contaminated material on site surfaces or in site soil. The short-term risks would be minimal due to the lack of activities associated with this alternative's implementation. At Sites 12 and 14, the remaining PCB contamination would continue to pose a potential risk to human health and the environment; therefore the no action alternative would not be effective in the long-term.

<u>Implementability</u> - The no action alternative would require no implementation activities other than a five year review; therefore, it is easily implemented.

 $\underline{\operatorname{Cost}}$ - A nominal cost would be associated with the preparation of the five-year review.

5.8.2 Alternative III-2 - Deed and Access Restrictions

5.8.2.1 Description

This limited action alternative would involve no remedial response activities for building surfaces or soils at Sites 12 and 14, although it would include implementation of deed restrictions and maintenance of site access restrictions. Deed restrictions would limit allowable future site use

and development, and have been included to provide a measure of long-term protection of human health by minimizing potential future exposures to contaminated site structures. Similarly access restrictions, including restrictions already in-place such as warning signs and locked accessways, provide a barrier to potential future human exposures.

In contrast to Alternative III-1, the no action alternative, this alternative has been developed to provide an increased level of protection of human health through site use restrictions while providing no reduction in the toxicity, mobility or volumes of contaminated surfaces or soil on-site.

5.8.2.2 Evaluation

Effectiveness - This alternative would provide no reduction in the toxicity, mobility or volume of surface material or soil contaminants at Sites 12 and 14. Deed and access restrictions would limit potential exposures due to direct contact with contaminated surfaces and would limit future site use. The long-term effectiveness of this alternative would be dependent on the long-term maintenance of deed and access restrictions. Due to the scheduled base closure, long-term maintenance and enforcement of this alternative could be difficult to implement. While offering potential long-term effectiveness, this alternative limits any future use of the contaminated areas. Protection of human health would be provided only as long as deed and access restrictions are enforced. No additional short-term risks other than those which currently exist would be associated with its implementation.

Implementability - This alternative would involve the placement of land use deed restrictions on property controlled by the federal government. Implementation of these deed restrictions should be relatively easy. Maintenance of access restrictions would require long-term monitoring to

ensure barriers to access are maintained. Overall, this alternative would be relatively easy to implement, although it may be difficult to enforce over the long-term due to scheduled base closure.

<u>Cost</u> - Costs associated with this limited action alternative would be those associated with administrative costs to establish site use restrictions and maintenance of access restrictions. Provision of a security guard for 30 years has been assumed.

The cost of this limited action alternative is initially estimated at a present worth value of \$540,000 (see Appendix E for preliminary cost estimates).

5.8.3 <u>Alternative III-3 - Sealing</u>

5.8.3.1 Description

This alternative was developed to meet the NCP's requirement for consideration of an alternative which utilizes containment with little or no treatment. Alternative III-3 incorporates sealing or covering of site contaminants, thereby limiting potential future exposure the Through sealing, the contaminated surface is physically contamination. separated from adjacent areas, thereby preventing any exposure to or migration of contamination. The sealing system for Sites 12 and 14 is assumed to consist of the following:

- 1/4" layer of epoxy grout
- 4" top layer of reinforced concrete

For the two remedial scenarios considered for Sites 12 and 14, the following remedial options have been developed:

 Scenario 1 - To address PCB contamination exceeding 1 ppm, the areas of encapsulation at Sites 12 and 14 would be 13,000 ft², and 15,000 ft², respectively, as previously described in Section 5.5. This option would also include the removal of 4 yd³ of soil at Site 14 which exceeds the 1 ppm PCB cleanup standard.

Scenario 2 - To address PCB contamination at or exceeding 10 ppm and 2 μ g/100 cm², the areas of encapsulation at Sites 12 and 14 would be 1,750 ft², and 3,000 ft², respectively, as previously described in Section 5.5.

In addition to sealing, deed restrictions would be placed on Sites 12 and 14 to limit future site use and development. The deed restrictions would aid in the long-term protection of human health by minimizing potential disruption of the encapsulated areas.

5.8.3.2 Evaluation

Effectiveness - Alternative III-3 would provide no reduction in the toxicity or volume of site contaminants but it would limit exposure to building structure contamination and the potential migration of the contamination and could be implemented in a timely manner. By limiting exposures to the PCB contamination, protection of human health would be provided. In the short-term, the alternative should be effective since it requires minimal disruption of surficial materials. Long-term effectiveness depends upon the permanence of the encapsulation techniques and the effectiveness of the deed restrictions. Long-term maintenance of the surface seal would be required.

Implementability - Sealing of surfaces would be relatively easy to implement and can be applied to all building materials. This activity employs commonly used and widely accepted construction equipment and techniques. Administrative implementation of deed restrictions would be relatively easy to undertake given the present ownership of the site by the federal government. The overall implementability of Alternative III-3 is good. The scheduled base closure could make long-term maintenance of the seal coat difficult to implement.

<u>Cost</u> - The main cost associated with Alternative III-3 is that associated with the sealing process. Initial estimates of the present worth cost for each option considered under Alternative III-3 are as follows:

- Scenario 1 \$370,000
- Scenario 2 \$71,000

See Appendix E for preliminary cost estimates.

5.8.4 Alternative III-4 - Removal with Off-Site Disposal/Incineration

5.8.4.1 Description

Removal and disposal of PCB-contaminated building surfaces and/or soils at an off-site landfill would eliminate the need for long-term management of PCB contaminants. For both Sites 12 and 14, this alternative would involve removal of the surficial concrete/asphalt and excavation of six inches of the subgrade soil with off-site disposal at a landfill permitted to accept PCB-contaminated wastes. Soil sampling during remediation would determine final disposal requirements.

As previously described in Section 5.5, one asphalt sample collected at Site 12 was characterized as containing 1,200 ppm of PCBs. Federal land disposal restrictions (40 CFR Parts 261 and 268), restrict land disposal of soils which contain halogenated organic compounds (including PCBs) in total concentrations greater than or equal to 1,000 ppm. To satisfy the land disposal restrictions, the volume of asphalt containing PCBs at greater than 1,000 ppm will not be landfilled but will be transported off-site to a TSCA-permitted incinerator.

For the two remedial scenarios considered for Sites 12 and 14, the following remedial scenarios have been developed:

Scenario 1 — To address PCB contamination exceeding 1 ppm, the volumes of concrete/asphalt and soil removal at Sites 12 and 14 would be 480 yd³, and 420 yd³, respectively, as previously described in Section 5.5. This option would also include the removal of 4 yd³ of soil at Site 14 which exceeds the 1 ppm PCB cleanup standard. An estimated volume of 19 yd³ of concrete would be transported off-site for incineration while the remainder of the material would be landfilled.

• Scenario 2 - To address PCB contamination at or exceeding 10 ppm or 2 μ g/100 cm², the volumes of concrete/asphalt and soil removal at Sites 12 and 14 would be 64 yd³, and 83 yd³, respectively, as previously described in Section 5.5. As with the previous option, 19 yd³ of concrete would be transported off-site for incineration while the remainder of the material would be landfilled.

5.8.4.2 Evaluation

<u>Effectiveness</u> - Overall, the off-site disposal/incineration option described above provides for a reduction in the mobility, but not the volume or the toxicity of contaminants, with the exception of the material which must be incinerated under federal land disposal requirements.

Off-site landfilling provides no treatment of contaminants. It would reduce the volume of contaminated building surfaces and/or soil on-site and would also tend to reduce the ultimate mobility of the contaminants through placement of the building surfaces and soil in a secure landfill. This alternative would be suitable for the volumes of waste to be generated. Long-term effectiveness at Sites 12 and 14 would be good, due to the removal of contaminated material and, therefore, elimination of unacceptable contaminant exposure pathways. The long-term effectiveness off-site at the disposal area would be dependent on the long-term operating and maintenance procedures at the receiving landfill.

The short-term effectiveness of Alternative III-4 would be hampered by the required excavation and disturbance of site contaminants. However, exposures to remedial workers during building material removal could be minimized

through the use of appropriate health and safety equipment. No off-site impacts are anticipated in the short-term.

Implementability - Implementability of off-site disposal/incineration would be directly related to the availability of a suitable landfill and incinerator of adequate capacity to accept the type of material generated from the site. In general, implementability is expected to be good.

<u>Cost</u> - The major costs associated with this alternative include the off-site transportation and disposal/incineration costs. Initial estimates of the present worth cost for each option considered under Alternative III-4 are as follows:

- Scenario 1 \$1,200,000
- Scenario 2 \$ 300,000

See Appendix E for preliminary cost estimates.

5.8.5 Alternative III-5 - Decontamination (Solvent Washing)

5.8.5.1 Description

Alternative III-5 provides for the decontamination of building materials through solvent washing. Solvent washing is a decontamination process whereby an organic solvent is circulated across the contaminated surface to solubilize contaminants. The contaminants are transferred from the contaminated surface to the solvent wash, which subsequently requires additional treatment such as filtration, neutralization and distillation. The primary difficulty with the process is achieving an inward flux of virgin solvent into the porous concrete, followed by an outward flux of contaminated solvent. There is a potential for the PCBs dissolved in the solvent to actually migrate deeper into the concrete slab. The system uses a circulation box with seals along the edges which is passed across the contaminated surface. Spent solvent

passes through the treatment unit and is recycled to the feed tank, from which it is pumped back to the circulation box. The residues from the solvent recovery system require disposal as hazardous wastes. Multiple applications of the solvent could be required to achieve cleanup levels. Residual solvent can be removed through water washing or heating to volatilize the residuals.

This technology is appropriate for the concrete floor at Site 12 but is not appropriate for asphalt materials, as at Site 14. Therefore, this alternative, if selected for Site 12, would have to be combined with another remedial alternative or technology at Site 14. The alternative will eliminate or reduce the toxicity, mobility, and volume of the contaminated building materials at Site 12.

For the two remedial scenarios considered for Site 12, the following remedial options have been developed:

Scenario 1 - To address PCB contamination exceeding 1 ppm, the area of concrete at Site 12 requiring treatment is estimated to be $13,000 \, \text{ft}^2$, as previously described in Section 5.5.

Scenario 2 - To address PCB contamination at or exceeding 10 ppm, the area of concrete at Site 12 requiring treatment is estimated to be $1,750 \, \text{ft}^2$, as previously described in Section 5.5.

5.8.5.2 Evaluation

Effectiveness - Alternative III-5 would provide a reduction in the mobility, volume, and toxicity of contaminants at Site 12. The efficiency of removal depends on the solvent-contaminant match and the ability of the system to recapture any PCBs dissolved in the solvent, without the solvent migrating deeper into the slab. A treatability test would be required to verify the effectiveness of the technology, which is not widely used or proven. If an effective removal system could be identified, the long-term effectiveness of the technology is anticipated to be good, providing protection of human

health. Solvent washing is a passive process but, due to the potential for explosion or fire hazards associated with many flammable solvents, use of appropriate personal protective equipment is required. Therefore, potential short-term risks are associated with its implementation, although no off-site impacts are expected in the short-term.

<u>Implementability</u> - Solvent washing would be relatively easy to implement. Time required for mobilization, demobilization and implementation of this technology may be fairly extensive, depending on the number of applications required.

<u>Cost</u> - The main costs associated with Alternative III-5 are the costs of the equipment, solvent feed, and residual disposal. Preliminary cost estimates are as follows:

Scenario 1 - \$69,000

• Scenario 2 - \$21,000

See Appendix E for preliminary cost estimates.

5.9 Selection of Alternatives for Detailed Analysis

A comparative analysis of the individual alternatives based on the three evaluation criteria is conducted to allow the elimination of selected alternatives from the detailed analysis process.

5.9.1 Effectiveness

Those alternatives which provide protection of human health and the environment, and which involve reductions in the toxicity, mobility or volume of contamination and contaminant sources, thereby decreasing the inherent risks associated with the hazardous material, typically provide the greatest long-term effectiveness. The effectiveness of an alternative in handling the

contaminated media and its reliability are also considered under this criterion. With respect to short-term effectiveness, those alternatives which are protective during the construction and implementation period and which achieve remedial response objectives within a timely manner are most effective.

For the building surfaces and soil remedial alternatives developed, Alternatives III-4 and III-5, removal with off-site disposal/incineration and solvent washing, provide the greatest long-term effectiveness, due to the treatment or disposal of contaminated soils and building surfaces. However, due to the required disruption of the contaminated building surfaces and soils, these alternatives also have increased short-term risks associated with their implementation.

Alternative III-4, removal with off-site disposal/incineration is the more effective of the two alternatives, since it employs proven waste management techniques, can easily be applied to the defined areas and volumes of contaminated materials, and can be conducted within a timely manner. The level of contaminant reduction is also more reliable with this alternative than with solvent washing (Alternative III-5), thereby providing greater protection of human health over the long-term. While dust is generated during the removal process, provisions can be taken to contain the removal area and to protect removal workers to limit any short-term impacts associated with implementation. Remedial objectives can be obtained within a relatively short time frame.

Solvent washing, while providing removal of the surficial PCB contamination from the flooring, is not a well-proven technology and may actually enhance the migration of contaminants deeper within the flooring. Its ability to meet cleanup objectives is not well-defined. Short-term risks may be associated with the handling of solvents in the removal process and the

removal time frame may be vary, depending on the actual effectiveness of the process.

Alternative III-3, surface sealing, provides the next degree of effectiveness by reducing the risks associated with direct contact with contaminated building surfaces, although no reduction in the toxicity or volume of contamination is realized. This alternative is easily applied to the area of contamination and can be implemented within a relatively short time frame. Short-term risks associated with its implementation would be minimal. Long-term protection of human health is dependent on the long-term maintenance of the surface coat.

Alternative III-2, no action with site access and deed restrictions, limits potential exposures to building surfaces and soil contamination through site access restrictions and restrictions on future site use. No reductions in contaminant toxicity, volume or mobility are provided by this alternative. Its long-term effectiveness and overall protection of human health are dependent on the long-term maintenance of the associated restrictions. This alternative could be implemented within a relatively short time frame, with minimal risks associated with implementation.

Alternative III-1, no action, would not be effective in treating the site contamination. It would provide no protection of human health or the environment.

5.9.2 Implementability

Implementability is a measure of the technical and administrative feasibility of constructing, operating, and maintaining a remedial action alternative. Alternative III-1, no action, is the most implementable remedial alternative from a construction standpoint due to the lack of implementation activities associated with it. Alternative III-2, limited action, is also

restrictions and implementation of deed restrictions. However, maintenance of these restrictions will be difficult upon completion of base closure. Alternative III-3, sealing, is next in terms of implementability based on the relatively simple nature of encapsulation. It too will require long-term maintenance, however. Alternative III-4, excavation and treatment/disposal is more difficult to implement compared to other options but is most implementable in the long-term, due to a lack of associated maintenance requirements. Alternative III-4 requires floor removal and soil excavation, and off-site disposal or incineration. Alternative III-5 is the least implementable of all of the alternatives, due to the limited number of vendors and the potential requirement of multiple applications to meet cleanup standards.

5.9.3 <u>Cost</u>

Alternative III-1, no action, is the lowest cost alternative. The solvent washing alternative, Alternative III-5, has the next highest estimated cost associated with implementation but it addresses contamination only at Site 12. The containment alternative, Alternative III-3 ranges in cost from \$71,000 to \$370,000, depending on the selected cleanup level (10 ppm versus 1 ppm). The removal/excavation and treatment/disposal of soil and building surfaces included in Alternative III-4 present the next highest potential costs at \$300,000 to \$1,200,000. Alternative III-2, limited action, can be implemented at a cost of \$540,000, based on the provision of manned site security for 30 years. A lesser degree of site security could be protective and more cost-effective.

5.9.4 Selection of Alternatives for Further Consideration

Based on the comparative analysis presented in the previous section, as well as the individual alternative/option analyses presented in Sections 5.8.1 through 5.8.5, no alternatives are proposed to be eliminated from the range of alternatives undergoing detailed analysis.

The remaining alternatives and technology options will be retained for detailed analysis. This will allow for the further consideration of a wide variety of remedial options providing a range in the degree of treatment for the various media at the site.

6.0 GROUP VI SITES - SITE 10 - CAMP FOGARTY DISPOSAL AREA

6.1 Introduction

The Group VI Sites consist solely of Site 10 - Camp Fogarty Disposal Area. The following sections provide a site description, summary of remedial response objectives and cleanup criteria, general response actions, identification and screening of technologies and process options, remedial alternative development, and preliminary screening of remedial alternatives.

6.2 <u>Site 10 - Camp Fogarty Disposal Area</u>

6.2.1 Site Location and Description

Camp Fogarty, is a 347-acre parcel of land, located about 3 miles west of the Main Center, in East Greenwich, Rhode Island. Camp Fogarty includes an active firing range; access to the entire area, including Site 10 is restricted by fences and facility personnel. This property is being excessed to the U.S. Army.

The Site 10 study area (the Camp Fogarty Disposal Area) is located in a depression west of a firing range, between the firing range berm(s) and a steeply-rising hill. A site map is provided in Figure 6-1. The vicinity of the study area is heavily wooded, interspersed with meadow areas. Seasonal flooding occurs in the low lying regions of Site 10 during periods of heavy rain.

6.2.2 Site History Overview

Cans of rifle- and weapon-cleaning oils and preservatives, as well as miscellaneous municipal-type garbage, were occasionally disposed of in a shallow, sandy excavation just west of the rifle ranges at Camp Fogarty. The disposal volume is estimated at 50,000 cubic feet in the IAS. Waste materials

noted during the IAS included rusted, empty paint cans, 55-gallon drums, and miscellaneous metal parts. Reportedly thousands of cans of rifle bore oils were removed from the site at one point and relocated at NCBC-Davisville.

6.2.3 Geology, Hydrogeology and Hydrology

No subsurface soil borings were drilled at Site 10 during the Verification Step while five soil borings were drilled during the Phase I RI. Borings drilled during the RI ranged in depth from 8 feet to 31 feet. Overburden deposits are predominantly a matrix of dense coarse to fine sands with a smaller percentage of boulders and cobbles. The depth to bedrock below the site was not confirmed during the RI. Auger refusal occurred at 7.2 feet in one of the borings.

The depth to the ground water table varies between 7 and 18 feet below the ground surface. The apparent direction of flow, based on a potentiometric map developed in the RI report and presented here as Figure 6-2, is to the east-southeast, with a hydraulic gradient of approximately 0.01.

6.2.4 Summary of Contamination

Verification Step field investigations consisted of two phases which included a site walk-over with an organic vapor analyzer (OVA), and surface soil sampling. A composite soil sample (collected from 4 sampling locations) contained less than 80 ppm of petroleum-based hydrocarbons and about 10 ppm of total volatile organic compounds, of which the major compound was not identified. Benzene, 1,2-dichloroethane, 1,1,2,2-tetrachloroethane, and 1,3-transdichloropropane were all detected at low levels. The EPA Priority Pollutant scan performed during the second round of sampling, which consisted of one surface soil sample, indicated slightly elevated levels of lead, toluene, and pyrene.

The Phase I RI included a limited soil gas survey, the collection of 6 surface soil samples, 2 soil borings, and the installation and sampling of 3 ground water monitoring wells. A sample location map is provided in Figure 6-3. Results of the RI indicated the presence of PAH contamination in surface soils. Laboratory analyses did not confirm the presence of volatile organic contamination in areas identified as having "slightly elevated" organic vapors during the soil gas survey. Metals were detected in both surface and subsurface soils at concentrations similar to those found at other sites at NCBC-Davisville. Metals (chromium and lead) were also detected in the site ground water at elevated concentrations. The predominant metals detected at the site include beryllium, chromium, copper, lead, and zinc.

6.2.5 Summary of Contaminant Fate and Transport

A contaminant fate and transport analysis was conducted as part of the Phase I RI. That analysis is summarized below. For more information, refer to the Phase I RI Report (TRC, 1991).

The primary contaminant migration pathways at Site 10 include surficial erosion or leaching of contaminants through the soil column to the ground water. While Site 10 is not flat, it is heavily vegetated, thereby minimizing surficial transport of contaminants. Site 10 (Camp Fogarty) lies about 3,500 feet west of the Hunt River. Ground water quality at Site 10 is classified as GAA Non-attainment; therefore potential migration of contaminants to the underlying aquifer is of concern.

Most surface soil sample locations at Site 10 exhibited a similar pattern of petroleum-related PAH contamination. PAHs were not observed in subsurface soils. No organic contaminants were detected in the ground water. PAH contaminants can be described in terms of those related to acenaphthene versus

those related to benzo(a)pyrene. Those related to acenaphthene are generally more mobile in the environment, with higher volatilities, higher solubilities and a greater tendency to leach from the soil. The majority of PAH contaminants detected in soils at Site 10 are those related to benzo(a)pyrene and are therefore likely to remain bound to soils, primarily because of their trace concentrations and their moderate to high tendencies to sorb to soils.

Metals common to surface and subsurface soils and ground water included beryllium, chromium, copper, lead, and zinc. No depth-specific differences in metal concentrations were observed in the soil samples. No TCLP analyses of soil samples were conducted at Site 10 but, in general, inorganic ground water concentrations were similar to those detected at other NCBC-Davisville sites. Further analysis of ground water quality at Site 10 will be conducted during the Phase II RI.

6.2.6 Summary of Human Health and Environmental Risk

Carcinogenic risk estimates, as presented in the risk assessment portion of the Phase I RI Report (TRC, 1991), ranged from 3.33 x 10^{-7} for the most-probable case current scenario to 2.63 x 10^{-6} for the worst-case current scenario, based on surface soil exposures. PAHs, arsenic, and beryllium are the carcinogens driving these risk values. Future risks associated with exposures to ground water at Site 10 ranged from 3.20 x 10^{-4} for the most probable case scenario to 7.17 x 10^{-4} worst-case scenario, with both risk estimates driven by the presence of arsenic. No organics were detected in Site 10 ground water. Total future residential carcinogenic risk estimates ranged from 3.34 x 10^{-4} for the most-probable case scenario to 7.44 x 10^{-4} for the worst-case scenario. Hazard index values estimated for all soil and ground water exposure scenarios were less than one.

The ecological risk assessment presented in the Phase I RI Report (TRC, 1991) concluded that, while current access restrictions tend to reduce exposures to most ecological receptors, the known breeding of two State Species of Concern, the marbled salamander and the four-toed salamander, within two miles of Camp Fogarty may justify further analysis of risks associated with site soils, with contaminants of possible concern including PAHs, arsenic and beryllium. Further characterization of ground water flow regimes, and surface water quality, as will be conducted during the Phase II RI, is required to assess potential risks to ground water/surface water receptors. The Phase II RI will also include additional ecological characterization.

6.3 Remedial Action Objectives and Cleanup Criteria

Remedial response objectives are developed in order to set goals for protecting human health and the environment early in the alternative development process. The goals should be as specific as possible but should not unduly limit the range of alternatives that can be developed. For Site 10, the results of the RI have been used to define specific contaminants of interest and allowable exposures based on the risk assessment and ARARS/TBCs.

6.3.1 Comparison of Contaminants to ARARs/TBCs

Based on the results of the RI, a summary of ground water and soil contaminants and a comparison of their detected levels to ARARs/TBCs are provided below, followed by an evaluation of risk-based cleanup levels. The identification of remedial response objectives, presented in Section 6.3.3, will be based on this evaluation.

For contaminated soils, constituents detected in soil samples were compared to federal and state action levels. Only a limited number of

standards are applicable to soil contamination. The only detected contaminant for which ARARs/TBCs were identified was lead. Lead was not present in surface or subsurface soil samples at levels which exceeded the guidance identified levels (see Table 6-1).

In evaluating ground water contaminant levels, state and federal standards (i.e., Maximum Contaminant Levels, Maximum Contaminant Level Goals, Secondary Maximum Contaminant Level Goals, and Rhode Island Ground Water Quality Standards) were used as ARARs/TBCs. Numerous inorganic constituents were present in ground water samples collected during the RI. The detected concentrations of beryllium and lead exceeded applicable standards, as indicated in Table 6-2. Specifically, a sample collected from monitoring well MW10-1, adjacent to the north-south trending firing range berm (see Figure 6-4), contained lead at a concentration of 24.5 ppb, which exceeds the U.S. EPA action level of 15 ppb. This sample also contained 80.8 ppb of total chromium which is greater than the RI Ground Water Quality Standard of 50 ppb for hexavalent chromium but is within the proposed RI Ground Water Quality Standard of 100 ppb for total chromium. Samples collected from monitoring well MW10-2, the westernmost well, exhibited beryllium at 5.3 ppb and lead at 140 ppb. The detected concentration of beryllium exceeds the federal MCL and MCLG for beryllium, which are both equal to 4 ppb. The RI Ground Water Quality Standard (50 ppb) as well as the U.S. EPA action level (15 ppb) for lead were also exceeded. In regard to the non-enforceable Secondary Maximum Contaminant Levels (SMCLs), samples from all three of the monitoring wells contained levels of iron, manganese, and aluminum which exceeded SMCLs. organic contaminants were detected in the ground water at Site 10.

6.3.2 Risk-Based Considerations

described in the National Contingency Plan [40 CFR As 300.43(e)(2)(i)(A)(2), "The 10^{-6} risk level shall be used as the point of departure for determining remediation goals for alternatives when ARARs are not available...". The 10^{-6} starting point indicates U.S. EPA's preference for setting cleanup levels at the more protective end of the acceptable 10^{-4} to 10^{-6} risk range for Superfund remedial actions. Site-specific and remedy-specific factors are then taken into consideration in the determination of where within the 10^{-4} to 10^{-6} risk range the cleanup standard for a given contaminant will be established. For the purposes of this evaluation, the risk-based cleanup levels which correspond to a 10⁻⁶ risk are calculated. Site-specific and remedy-specific factors which may affect the determination of the final cleanup level will be addressed in subsequent portions of this document.

Chemical constituents present in ground water or surface soils at Site 10 for which ARARs are not available include carcinogenic PAHs and inorganic compounds. The risks posed by these constituents under a reasonable maximum exposure scenario were evaluated to determine which constituents pose carcinogenic risks greater than 1 x 10^{-6} or noncarcinogenic risks, as measured by hazard index ratios, greater than unity. None of the ground water constituents for which no ARARs exist pose risks which exceed these point of departure risk levels.

For surface soil constituents, cancer risked-based cleanup levels were developed under the future residential use reasonable maximum exposure scenario for the following constituents for which there are no ARARs/TBCs but which pose carcinogenic risks greater than 1 x 10^{-6} : PAHs, arsenic and beryllium. Surface soil cleanup levels were calculated for these

contaminants, based on the 1×10^{-6} risk, as presented in Table 6-3. Because Site 10 is being excessed to the Army, the potential for future residential use of this site may be less than for other NCBC-Davisville sites. However, a conservative appoach, using future residential site use as the basis for calculation of risk-based cleanup levels, was used.

As previously discussed in Section 6.2.6, no individual hazard index values greater than unity were calculated for noncarcinogens in the risk assessment presented in the Phase I RI Report (TRC, 1991). Therefore, no risk-based cleanup levels were developed for noncarcinogens. Similarly, risks posed by subsurface contaminants did not exceed the point of departure (a 10⁻⁶ carcinogenic risk or a hazard index value of unity). Additional information used in the development of risk-based cleanup levels is presented in Appendix A.

Under the future residential use scenario, soil boring samples collected at the 0- to 2-foot interval (B10-01 and B10-02) and all of the surface soil samples with the exception of the background surface soil sample S10-01, contained beryllium at levels exceeding the risk-based cleanup level (see Figure 6-5). Arsenic was detected at levels exceeding the risk-based cleanup level at soil sample locations S10-01 (the background sample) and S10-03. benzo(a)anthracene, Estimated concentrations of benzo(a)pyrene, benzo(b)fluoranthene, and chrysene exceeded risk-based cleanup levels at soil sample location S10-03. It should be noted that for all SVOC analyses of surface and subsurface soil samples, detection limits exceeded risk-based cleanup levels. Therefore, the identification of sample S10-03 as the only sample with PAH levels exceeding risk-based cleanup levels on the basis of the estimated ("J" qualified) data for that sample has a significant level of uncertainty associated with it.

As indicated in Table 6-3, the greatest reasonable maximum exposure risk calculated for an individual compound under the future residential use scenario is 9.3×10^{-6} . Therefore, if no remediation of the site was conducted, calculated risk levels would be within the acceptable risk range of 10^{-4} to 10^{-6} applicable to remedial actions for the future use scenario.

6.3.3 Remedial Response Objectives

Based on the information presented above, as well as a consideration of potential ecological risks, the remedial action objectives for soil are as follows:

- Minimize current and future exposures to surficial soil contaminants at levels that pose unacceptable risks to human health and the environment;
- Minimize off-site migration of soil contaminants.

The remedial response objectives for ground water are as follows:

- Prevent exposure, due to ground water ingestion, to contaminants at levels exceeding acceptable ARARs/TBCs, as indicated in Table 6-2;
- Minimize migration of ground water contaminants and any associated environmental impacts; and

Restore contaminated ground water for future designated use.

6.4 General Response Actions

General response actions are those remedial actions which will satisfy the remedial response objectives. General response actions for Site 10 were formulated based on the results of the Remedial Investigation.

The first step in determining appropriate general response actions for a given media is an initial determination of the areas or volumes to which the

general response actions may be applied, as described below. In determining these volumes/areas of media, consideration has been given to site conditions, the nature and extent of contamination, acceptable exposure levels and potential exposure routes. As previously presented in Section 6.3.2, remediation limits will depend upon the level of risk determined to be acceptable for the site.

In order to provide a preliminary estimate of the volume of ground water and soil potentially requiring treatment, the extent of ground water contamination at levels exceeding ground water cleanup standards and MCLs, as well as soil contamination exceeding risk-based levels must be evaluated.

For soils, surface soil and soil boring (0- to 2-foot interval) samples collected from across the site have exhibited contamination in excess of cancer risk-based cleanup levels based on future residential site use. The total area associated with elevated contaminant levels potentially requiring remediation under the future residential use scenario is assumed to be approximately 25 acres (1,100,000 square feet), as indicated in Figure 6-5. Using a surface soil thickness of two feet (the general depth interval of surface soil samples) a total contaminated surface soil volume of approximately 80,000 cubic yards is estimated. Sample S10-01 has not been included within the estimated area because it was collected as a sample representative of background conditions. Further definition of background soil quality will be conducted in the Phase II RI.

As discussed previously in Section 6.3.1, inorganic constituents present in ground water samples from two monitoring wells exceed MCLs or federal action levels. Taking into account the three possible disposal areas on-site (see Figure 6-4), a ground water plume encompassing an area of approximately 16 acres (700,000 square feet) was estimated. Using an estimated average

saturated thickness of 14 feet (estimated depth from the water table to the bedrock surface) and assuming a conservative effective porosity of 30 percent, the volume of contaminated shallow ground water at Site 10 is on the order of 22,000,000 gallons. This is a very preliminary estimate which will be refined on the basis of proposed Phase II investigations.

Listings of general response actions developed for the remediation of soil and ground water, respectively, are provided below.

Soil:

- No Action
- Institutional Control
- Containment
- Treatment/Disposal

Ground Water:

- No Action
- Institutional Control
- Containment
- Extraction/Treatment/Discharge

6.5 Identification and Screening of Technologies and Process Options

actions are developed further through The general response identification and screening of remedial technologies which could potentially meet the remedial action objectives and cleanup criteria. Following a remedial technologies on basis of screening of the the implementability, the process options associated with each technology are screened based on effectiveness, implementability and cost. process options are chosen for inclusion in the remedial alternatives developed for the site.

6.5.1 Technology Screening

A combined technology screening was performed for all the sites addressed within this ISA. The technology screening for soils/sediments is presented in Table B-1 of Appendix B while the ground water technology screening is presented in Table B-3. The tables include brief descriptions of the individual technologies or process options, comments on their applicability, limiting characteristics which prevent their application to certain sites, and a summary of whether they are screened or retained for the various sites. The technologies or technology process options which do not pass the screening process on the basis of technical implementability will not be retained for further consideration. In conducting the technology screening for soils and ground water at Site 10, technologies were evaluated for their technical ability to address inorganic contaminants in the surface soils or ground water, as well as the technologies' abilities to be applied to the site-specific conditions at Site 10. Because Site 10 varies in elevation and because buried munitions and subsurface cobbles and boulders may exist at the site, some technologies could not physically be employed on-site; these technologies were screened from further consideration.

The soil remedial technologies which were screened from further analysis at Site 10 include on-site landfilling, on-site incineration, mechanical/thermal aeration, thermal desorption, landfarming, dechlorination, slurry phase biodegradation, solvent extraction, in situ biodegradation, soil venting, radio frequency heating, fungal degradation, in situ vitrification, in situ solidification/stabilization, and steam injection/vacuum extraction.

The ground water remedial technologies which were screened from further analysis at Site 10 include provision of an alternate water supply, construction of a vertical barrier using sheet piling, ground water treatment

at an off-site RCRA facility or on-site using a bioreactor, powdered activated carbon treatment (PACT™) system, air stripper, steam stripper, carbon adsorption unit, resin adsorption, UV oxidation or dehalogenation system, or in situ treatment using air sparging or biodegradation. Technologies and process options which passed the technology screening for Site 10 are summarized in Table 6-4.

6.5.2 Process Option Screening

identification of technologies which Upon those are technically implementable, the process options are further evaluated to allow the selection of a representative process option for each technology type. process options are evaluated on the basis of effectiveness, implementability, and cost. Process option evaluations are presented in Appendix B, Tables B-2 and B-4 for soil and ground water, respectively. Because the main risks currently identified for Site 10 are associated with direct contact with or ingestion of contaminated surface soils, and ingestion of contaminated ground water, process options associated with each technology were evaluated to determine their effectiveness in addressing these risks. Also considered in the process option screening were the volumes of soil to be addressed at Site 10, and, with respect to ground water contaminants, the potential for inorganics to be associated with suspended sediments or to be present as dissolved constituents.

For soil remediation, institutional control technology process options consisting of deed restrictions and fencing were selected as representative process options. For the capping technology, a RCRA Subtitle D Soil Cap was determined to provide protection against exposures to contaminated surface soils while also being implementable and cost-effective. For excavation and

disposal, off-site landfilling was the only process option retained for analysis. For excavation and treatment technologies, soil washing and stabilization/solidification were selected to be representative process options.

For ground water remediation, institutional control process options consisting of continued ground water monitoring and deed restrictions were selected as representative process options. For containment, a slurry wall was selected as a potentially appropriate means of providing containment. For ground water extraction, both extraction wells and interceptor trenches were selected while for treated water discharge, both discharge to ground water and surface water were selected, pending further definition of hydrologic and hydrogeologic site conditions. For ground water treatment technologies, ion exchange was selected as a representative process option capable of treated dissolved inorganic constituents, while membrane microfiltration was selected as a representative process option capable of treating undissolved metals. The selected representative process options are indicated with a bullet in Table 6-4.

6.6 Remedial Alternative Development

The technologies and process options developed in Section 6.5 are typically combined to form a range of remedial alternatives which address site cleanup to varying degrees and meet the criteria set forth in the NCP, as previously described in Section 3.8.

As indicated in Table 6-5, a total of four alternatives have been developed for addressing soil and/or ground water contamination at Site 10. These alternatives include a no action alternative (VI-1), a limited action alternative (VI-2) consisting of ground water monitoring, deed restrictions,

and fencing, a containment alternative (VI-3) consisting of a RCRA Subtitle D cap with or without a slurry wall, and an active restoration alternative (VI-4) consisting of soil and/or ground water treatment options. Individual remedial technologies for soil and ground water remediation will be retained throughout this FS to allow flexibility in the final remedial alternative selection process. Where appropriate, discussions of how the technologies could logically be combined to form remedial alternatives which offer various degrees of treatment will be presented.

6.7 Definition and Preliminary Screening of Remedial Alternatives

Each of the alternatives and technology options presented in Table 6-5 undergo a preliminary screening in this section. The screening process was previously described in Section 3.9. Following the individual screening and analysis, a comparative analysis is conducted between alternatives. Those alternatives that pass the preliminary screening process will be evaluated in the Detailed Analysis of Alternatives.

6.7.1 Alternative VI-1 - No Action

6.7.1.1 Description

The no action alternative would involve no remedial response activities at Site 10. No removal or treatment of contaminated ground water or surface soil would be conducted. Consideration of the no action alternative is required under the NCP. Because unlimited future use of the site would not be allowed under this alternative, a five-year review of the no action decision would be required. A round of ground water sampling would be conducted at the time of the five-year review to update existing ground water conditions.

6.7.1.2 Evaluation

<u>Effectiveness</u> - The no action alternative would provide no reduction in the toxicity, mobility or volume of contamination. It would provide no protection of human health or the environment with respect to potential exposures to ground water contamination. However, based on the risk assessment conducted for this site, cancer risks under most current and future land use scenarios are less than 10^{-5} . Even under the future residential use scenario, the greatest risk posed by an individual contaminant under the reasonable maximum exposure scenario is within the acceptable risk range for remedial measures of 10^{-4} to 10^{-6} .

<u>Implementability</u> - The no action alternative would require no implementation activities other than the completion of a round of ground water sampling prior to conducting a five-year review of the no action decision.

Cost - The only costs associated with implementation of the no action alternative are the ground water monitoring costs and a nominal cost associated with the preparation of the five-year review. An initial estimate of the cost of Alternative VI-1 is a present worth value of \$21,000 (see Appendix F).

6.7.2 Alternative VI-2 - Ground Water Monitoring with Deed Restrictions and Fencing

6.7.2.1 Description

This alternative was developed as a limited action alternative which provides no active remediation other than natural attenuation. The alternative consists of the institution of site use restrictions, long-term ground water monitoring, and fencing.

For Alternative VI-2, deed restrictions would be implemented to limit potential future site use and development, thereby limiting potential future

exposures to surface soil contamination or to ground water contamination which could result from the future installation of potable wells at Site 10. A six-foot-high chain link fence would be placed around Site 10, as indicated in Figure 6-6, to limit direct exposures to the site. Placement of hazard warning signs on the fence would also be included in this alternative. Ground water monitoring would provide a means of monitoring the extent of ground water contamination and any changes in ground water quality over time. A 30-year time frame has been assumed for the monitoring program.

In contrast to Alternative VI-1, which was required to be considered under the NCP, this alternative has been developed to provide an increased level of protection of human health through fencing, land use restrictions, and continued ground water monitoring, while providing no action to reduce the toxicity, mobility or volumes of contaminated surface soil or ground water on-site.

6.7.2.2 Evaluation

Effectiveness - Alternative VI-2 would provide no reduction in toxicity, mobility or volume of contaminated media. Potential future exposures to risks posed by surface soil and ground water contamination would be limited by deed restrictions and fencing. Minimal risks would be associated with its implementation. Long-term effectiveness would be dependent on the long-term maintenance of the perimeter fence and compliance with deed restrictions. Due to the scheduled base closure, long-term maintenance and enforcement of this alternative could be difficult to implement, unless these duties were accepted by the U.S. Army, to whom it is anticipated this site will be excessed.

Implementability - Alternative VI-2 would be fairly easy to implement although it would require implementation of deed restrictions and a continued

ground water monitoring effort. Availability of materials and equipment to install fencing is readily available.

Cost - The main cost factors associated with Alternative VI-2 would be the implementation of deed restrictions, long-term ground water monitoring, and the installation of fencing. An initial estimate of the cost for Alternative VI-2 is a present worth value of \$420,000, assuming a 30-year maintenance and monitoring period (see Appendix F).

6.7.3 <u>Alternative VI-3 - RCRA Subtitle D Soil Cap/Deed Restrictions with Slurry Wall Option</u>

6.7.3.1 Description

This alternative was developed to meet the NCP's requirement for consideration of an alternative which utilizes containment with little or no treatment.

Two scenarios were developed for the evaluation of this alternative. Option A incorporates the capping or covering of the site with a RCRA Subtitle D soil cap which would minimize potential risks associated with direct contact with or erosion of contaminated surface soils. The soil cap would cover approximately 25 acres, based on the extent of surface soils which exceeded risk-based cleanup levels, and would include surface drainage features to properly control surface water runoff. The proposed physical limits of the cap are shown on Figure 6-7. The cap would consist of a minimum 18-inch infiltration layer topped by a minimum 6-inch erosion layer. The infiltration layer would be constructed to provide a permeability less than or equal to the natural subsoils or a permeability no greater than 1 x 10⁻⁵ cm/sec, whichever is less. The erosion layer would consist of a minimum of 6 inches of earthen material capable of sustaining native plant growth.

Prior to constructing the soil cap, the site would require appropriate preparation. This would include clearing of site vegetation, the removal of near-surface debris, and partial grading and leveling of existing topographic features.

In addition to the RCRA Subtitle D soil cap, deed restrictions would be implemented to limit future site use and development. The deed restrictions would minimize potential disruption of the cap and prevent future residential site use. Ground water monitoring would also be included in this alternative.

In addition to the soil cap, the second option, Option B, would include the construction of a slurry wall, a low permeability vertical barrier, along the upgradient portion of the site. This barrier would be constructed from the ground surface to the depth of the bedrock present under the site (estimated to be at a depth of 45 feet). The slurry wall would be constructed upgradient of the area of ground water contamination to minimize ground water flow through the disposal areas on-site. The slurry wall would be constructed of a slurred mixture of native soils and bentonite, cement and bentonite, or a proprietary mixture which when set, creates a low permeability vertical barrier to limit horizontal ground water flow. For costing purposes, the length of the slurry wall is preliminarily estimated at 1,400 feet. Upon collection of additional data during the Phase II RI, the proposed slurry wall location and associated design details could be better defined.

6.7.3.2 Evaluation

Effectiveness - Alternative VI-3 would provide no reduction in the toxicity or volume of site contaminants but the slurry wall option could reduce ground water flow from upgradient areas into the potentially contaminated areas of the site. It would be ineffective, however, in addressing any inorganic ground water contaminant migration which has already

occurred. Additional protection from potential direct exposure to surficial contamination would be provided by the physical presence of the cap and deed restrictions. Short-term effectiveness would be impacted by the disruption of surficial materials required to clear vegetation, remove surficial debris, and cap the site as well as by slurry wall construction activities. Verification of long-term effectiveness would require continued ground water monitoring.

Implementability - Alternative VI-3 would be relatively easy to implement. It would require clearing of vegetation, removal of surficial debris, surface grading, and construction of a cap. Each of these activities employs commonly used and widely accepted construction techniques. Construction of a slurry wall to the depth of the bedrock unit under the site (estimated to be 45 feet) could be accomplished using relatively common earth working equipment. However, the potential presence of buried munitions would complicate the excavation effort. The presence of subsurface boulders and cobbles could also complicate the slurry wall construction. Administrative implementation of deed restrictions would be relatively easy. The overall implementability of Alternative VI-3 is good.

Cost - The main cost factors associated with Alternative VI-3 are those associated with the construction of the RCRA Subtitle D soil cap and/or slurry wall. An initial estimate of the present worth cost for Option A, the capping option of Alternative VI-3, is \$3,100,000. The estimated present worth of Option B, capping with a slurry wall, is \$3,600,000. Both options include the cost of ground water monitoring for a thirty-year period.

6.7.4 Alternative VI-4 - Soil and Ground Water Treatment

6.7.4.1 Description

Alternative VI-4 consists of active site restoration, and includes the consideration of a number of treatment technologies for both contaminated soil

and ground water. The period of restoration will be dependent upon the combination of technologies included in the final alternative. A preliminary ground water extraction and treatment period of five years has been assumed, to be refined upon collection of additional site data. This analysis is intended to provide the basis for a general comparison between Alternatives VI-1, VI-2, VI-3 and VI-4. Preliminary analyses of the effectiveness, implementability and costs of the individual technology options are presented in Sections 6.7.6 through 6.7.12.

6.7.4.2 Evaluation

Effectiveness - For soils, Alternative VI-4 would provide a reduction in the mobility or toxicity of soil contaminants through either excavation and disposal or excavation and treatment. Alternative VI-4 would provide a reduction in the toxicity of ground water contamination through extraction, treatment and subsequent discharge of treated water. It would also limit contaminant mobility by capturing contaminated ground water, thereby preventing contaminated ground water migration off-site. toxicity reduction would be dependent upon the individual treatment technology An upgradient slurry wall could be combined with a ground extraction and treatment system to enhance the effectiveness of the system. In general, by excavating and treating or disposing of the contaminated soils and by treating the ground water contamination, the long-term effectiveness of this alternative would be considered greater than that of the previously evaluated no action, minimal action and containment alternatives. effectiveness of those soil treatment options which require excavation would be impacted by the disruption of the soils during the excavation activities, but personnel protective measures could be taken during the removal to protect on-site workers and dust minimization controls could be used as necessary to minimize off-site migration of any airborne particulates. Removal activities could be completed within a relatively short time frame. Ground water treatment could require an extended time frame to meet cleanup objectives.

<u>Implementability</u> - Alternative VI-4 is implementable, although its implementability would be highly dependent upon the individual technologies included in the alternative.

<u>Cost</u> - As with implementability, cost would be highly dependent upon the individual technologies included in the alternative. In general, Alternative VI-4 would cost significantly more than Alternatives VI-1, VI-2, and VI-3 due to the active restoration activities involved in its implementation.

6.7.5 Alternative VI-4, Option A - Soil Excavation and Disposal

6.7.5.1 Description

Disposal of contaminated soil at an off-site landfill would eliminate the potential need for long-term management of contaminated soil on-site. This option would involve excavation and off-site transportation of a two-foot depth of contaminated surface soil to a suitable landfill. Factors which are considered in the cost evaluation of this alternative include the replacement and compaction of clean back-fill over the excavation area and the premium cost involved with engineering oversight and the monitoring of worker health and safety during excavation operations. Prior to landfilling, the excavated soil must be characterized to determine if it meets the definition of hazardous waste and if it falls under land disposal restrictions. Federal land disposal restrictions (40 CFR Parts 261 and 268) prohibit the acceptance of certain waste types at landfills. Restricted waste types include solvent-, dioxin-, and California-list-contaminated soils and soils contaminated with listed or characteristic hazardous wastes. No TCLP analyses were conducted on soil samples collected at Site 10 during the Phase I RI. However, based on

the relatively low detected contaminant levels in soils at Site 10, it is assumed that the excavated soil could be disposed of as a non-hazardous waste.

6.7.5.2 Evaluation

Effectiveness - Option A, off-site landfilling of contaminated surface soil, would eliminate any need for long-term management of surface soils or restrictions to public exposures to surface soils; however off-site landfilling would provide no treatment of the contaminants of concern. Long-term effectiveness would be dependent upon the long-term operation and maintenance of the receiving landfill. The main hazard associated with the soil contaminants, potential residential exposure, would be eliminated through off-site landfilling. In the short-term, exposures to remedial workers could be minimized through the use of appropriate health and safety equipment.

Implementability - The implementation of this option would be dependent on the additional characterization of the soils and the availability of a suitable landfill with adequate capacity to accept the type and volume of soil generated. Due to the significant volume of soil to be addressed under this option (80,000 cubic yards), the identification of a landfill with available capacity to accept such a volume may be difficult.

 $\underline{\text{Costs}}$ - The major costs associated with this option are those associated with off-site transportation and disposal. An initial estimate of the present worth costs for this option is \$13,000,000 (see Appendix F).

6.7.6 Alternative VI-4, Option B - Soil Excavation and Treatment (Soil Washing)

6.7.6.1 Description

Soil washing is a process whereby contaminated soil is mixed with water which may contain surfactants, chelating agents, acids or bases, or with a

solvent and mechanically scrubbed to separate soil fractions, thereby removing the contaminants. Many soil washing units operate on the principle that most of the contaminants are adsorbed to the finer materials and, therefore, size segregation reduces the volume of soil requiring treatment. Analyses of particle size distribution as well as the distribution of contamination by particle size are necessary to determine the potential applicability of soil washing. The cleaned, coarser-grained soil fraction produced by the soil washing process may be either redeposited on-site or otherwise beneficially used as backfill or industrial sand. The finer-grained fraction, which contains the concentrated contaminants, requires off-site disposal in accordance with state and federal regulations. A schematic of a typical soil washing system is presented in Figure 6-8.

Soil washing has been used as a single-stage, stand-alone technology where applicable, or coupled with other on-site remediation technologies to achieve desired contaminant levels. Typically, in order to justify mobilization/demobilization costs, a minimum of 5,000 tons of soil should be processed. Based on the surface soil estimated volume of 80,000 cubic yards, mobilization of an on-site soil washing system could be justified.

6.7.6.2 Evaluation

Effectiveness - Soil washing provides a reduction in the volume of contaminated soil materials by separating the "dirty" finer-grained fraction from the cleaner coarse-grained fraction. The fine-grained fraction subsequently requires off-site disposal. The process can be effective for both organic and inorganic constituents and is applicable to large volumes of soil. The level of effectiveness depends on the identification of the appropriate extractant chemical(s). If cleanup objectives can be achieved,

the process would be protective of human health. Short-term risks would be limited to exposures to the contaminated soils during excavation and on-site processing. These could be limited through the use of appropriate personnel protection equipment.

Implementability - The overall soil washing process is fairly easy to implement although it is a relatively innovative technology with a limited number of vendors. Since soil washing is a slurry-based process, a water supply would be required.

<u>Costs</u> - The main costs associated with implementation of Option B include the mobilization and operation of the soil washing system, excavation, and treatment/disposal of the process residuals. The estimated present worth cost of implementing soil washing at Site 10 is \$27,000,000 (see Appendix F).

6.7.7 Alternative VI-4, Option C - Stabilization/Solidification

6.7.7.1 Description

Option C consists of the excavation and stabilization of contaminated surface soils at Site 10. The solidification/stabilization process uses additives or processes to physically or chemically immobilize the hazardous constituents of a contaminated soil. The soils would be stabilized by mixing with a cementing material and water. As the mixture hardens, the hazardous constituents are encapsulated within the solid matrix which is formed. Following stabilization, the stabilized material would require testing and handling in accordance with federal and state regulations. It is assumed that the stabilized material would be placed back on-site. In order to minimize the exposure of the stabilized material to moisture and minimize any subsequent contaminant leaching, a synthetic liner would be placed beneath and above the material. In addition, approximately four feet of compacted clean

soil would be placed above the top of the liner to minimize freeze/thaw of the stabilized material.

6.7.7.2 Evaluation

Effectiveness - Alternative VI-4, Option C would be effective in immobilizing the soil contaminants through stabilization processes. While solidification/stabilization has primarily been applied to soils contaminated with metals and other inorganics, the process has also been proven applicable to semivolatile and nonvolatile organic compounds such as PAHs. The process would be effective in treating the volumes of contaminated material which exist at Site 10. The main exposure pathways identified during the human health risk assessment would be addressed by this alternative. Short-term effectiveness would be limited by the site disruption which would occur during excavation and stabilization activities. These risks could be limited through the use of appropriate personnel protection equipment. The use of synthetic liner materials to isolate the stabilized soils would provide an added measure of long-term protection and effectiveness.

Implementability - The technical implementability of this alternative would be expected to be good, with stabilization services available from numerous vendors. Mobile stabilization units are available in which the stabilization area is truck-mounted and requires no on-site construction of mixing pits. Physical separation of stones or cobbles may be required prior to the stabilization process. The presence of stones and cobbles may also complicate the construction of a lined area for on-site disposal of the stabilized materials. The administrative implementability would be dependent on the ability of the system to treat the soils sufficiently to meet the substantive requirements applicable to land disposal of the treated material.

<u>Costs</u> - The major costs associated with this option are those associated with the implementation of the soil stabilization process. The cost of implementing Option C is preliminarily estimated at \$40,000,000. See Appendix F for the preliminary cost estimate.

6.7.8 Alternative VI-4, Option D - Ground Water Extraction

6.7.8.1 Description

Based on a preliminary evaluation of extraction options, sufficient information does not exist on the horizontal or vertical distribution of ground water contamination or on the hydrogeologic properties of the aquifer to allow adequate evaluation of the most appropriate means of extracting ground water. Therefore, both an interceptor drain and ground water extraction wells will be discussed qualitatively as potential means of extracting contaminated ground water. Ground water extraction could potentially be combined with the construction of an upgradient slurry wall or other barrier mechanism to enhance the extraction system effectiveness. For comparison purposes, it is assumed extraction would occur over a five-year period. This option would be combined with a ground water treatment option and discharge option to form a complete restoration remedial alternative.

Interceptor Drain - An interceptor drain could potentially be effective in the collection and extraction of shallow contaminated ground water. The drain would be installed in a trench in the eastern portion of the site, downgradient from the monitoring wells which have exhibited elevated concentrations of inorganics, as discussed in Section 6.3.1. Based on existing information, the proposed trench location would be oriented in a general north-south direction, downgradient of monitoring wells MW10-1 and MW10-2, as indicated in Figure 6-9. For preliminary evaluation purposes, a

trench approximately 330 feet in length and approximately 25 feet deep has been assumed. This trench design would allow collection of ground water within the shallow portion of the saturated zone. Additional hydrogeologic information is required to determine the effectiveness of this preliminary design and to develop the actual applicability of this technology in capturing contaminated ground water.

The drain itself would consist of a perforated pipe placed at an incline within a trench filled with a highly-permeable backfill. Ground water would flow by gravity into and through the pipe to pre-cast manhole sumps where it would be lifted by means of a submersible pump to the surface for treatment, as necessary. For preliminary evaluation purposes, it is assumed that ground water would be extracted at the rate of approximately 250 gpm.

Extraction Wells - Contaminated ground water could also be extracted via extraction wells. Again, extraction wells would be located at the leading edge of ground water contamination, as indicated in Figure 6-9, with a pumping rate designed to capture the ground water contamination. Based on an estimated saturated thickness of 30 feet, an estimated hydraulic conductivity of 90 feet/day, a hydraulic gradient of 0.05 feet/feet, an extraction system consisting of seventeen extraction wells each pumping at 15 gallons per minute is assumed.

Slurry Wall - Slurry wall construction was previously described in the discussion of Option B of Alternative VI-3 (see Section 6.7.3.).

6.7.8.2 Evaluation

<u>Effectiveness</u> - Additional information on the vertical and horizontal extent of contaminated ground water within the aquifer as well as existing geologic and hydrogeologic characteristics of the aquifer are required to

determine the effectiveness of the proposed extraction options in capturing and thereby limiting the mobility of contaminated ground water and the potential applicability of a slurry wall.

Implementability - Installation of either of the proposed ground water extraction systems would be relatively easy to implement. The potential presence of buried munitions and subsurface cobbles and boulders could complicate the construction of an upgradient hydraulic barrier, such as a slurry wall.

Cost - Present worth cost estimates for the construction of the ground water extraction systems considered have been developed but are to be considered as very preliminary in nature. The initial cost of an interceptor trench is estimated to be on the order of \$40,000 while the initial cost of an extraction well system is estimated to be on the order of \$250,000 (see Appendix F). As previously evaluated in Section 6.7.3.2, construction of an upgradient slurry wall could add approximately \$500,000 to the overall cost.

6.7.9 Alternative IV-4, Option E - Ground Water Treatment (Membrane Microfiltration)

6.7.9.1 Description

Membrane microfiltration is a physical process for removing fine particulate matter from a wastestream. The treatment system is able to physically separate very small particles (less than 1 micron) by passing the wastestream through a membrane filter. Based on current ground water analyses, it is not possible to determine if the inorganic contaminants are due to colloidal particles within the wastestream or dissolved inorganic compounds. This alternative would be effective in removing undissolved inorganics. Treatability studies would be required to determine actual treatment efficiencies.

The treatment system is fairly simple. The waste feed is pumped through a filter fabric under pressure. The fabric allows water and very small particles (less than 1 micron) to pass through the openings in the fabric. Filtered solids accumulate on the fabric, forming a filter cake, while the filtrate is discharged from the system. Figure 6-10 provides a schematic of the membrane microfiltration system offered by DuPont, which utilizes DuPont's special Tyvek spun-bonded olefin as the filter fabric. The filter cake is dewatered and requires subsequent off-site disposal. Because no chemicals are added in the process, sludge volumes are significantly less than those produced by other inorganic treatment processes involving precipitation or coagulation.

6.7.9.2 Evaluation

<u>Effectiveness</u> - Treatability studies would be required to determine if microfiltration could provide sufficient inorganic removal to meet discharge criteria. The system has been proven to be effective in removing inorganics such as cadmium, lead and zinc to non-detectable levels at the Palmerton Zinc Superfund site in Palmerton, Pennsylvania. The filter cake produced during a SITE demonstration also passed TCLP analysis, thereby allowing for its disposal as a non-hazardous waste.

Implementability - The implementability of this alternative is expected to be good, due to its relative simplicity. Operational activities include maintenance, periodic replacement of the membranes, and sludge handling. Vendors which provide the treatment system are somewhat limited.

<u>Cost</u> - The cost for ground water treatment Option E is initially estimated at a present worth value of \$1,700,000 (see Appendix F).

6.7.10 Alternative IV-4, Option F - Ground Water Treatment (Ion Exchange)

6.7.10.1 Description

In the ion exchange process, contaminants are removed from the aqueous phase by exchanging places with ions held by relatively harmless ions in the exchange material. Ion exchange is a well established technology for removal of heavy metals and hazardous anions from dilute solutions.

Ion exchange resins can be described as strong acid, weak acid, strong basic or weak basic resins, in which the resins contain functional groups derived from the associated acid or base. The resins vary in terms of selectivity for various inorganics, depending upon ionic charge and size.

The wastestream passes through the ion exchange column until the exchange sites are exhausted. Then, the bed is backwashed to allow the resin to expand and resettle. The bed is then regenerated by passing a concentrated solution of the ion originally associated with it through the bed. Excess regenerant is removed through a rinse process and the bed is again ready for service. Ion exchange systems can be operated in batch mode or flow-through mode. Typical operating systems are indicated in Figure 6-11.

6.7.10.2 Evaluation

Effectiveness - The effectiveness of ion exchange would depend upon the identification of ion exchange mediums suitable for the particular inorganic contaminants of concern. In general, ion exchange can be expected to perform well for wastes of variable composition, provided the system's effluent is continually monitored to determine when the resin bed exhaustion has occurred. It should be noted that the reliability of ion exchange is markedly affected by the presence of suspended solids.

Implementability - Ion exchange systems are commercially available from a number of vendors. The units are relatively compact and are not energy intensive. Exchange columns can be operated manually or automatically, although manual operation is generally better suited for hazardous waste site application because of the diversity of wastes encountered. Use of several exchange columns at a site can provide considerable flexibility.

 $\underline{\text{Cost}}$ - The cost of ground water treatment Option F is initially estimated at a present worth value of \$3,400,000 (see Appendix F).

6.7.11 Alternative IV-4, Option G - Discharge (Discharge to Ground Water)

6.7.11.1 Description

This alternative technology option would be incorporated into Alternative IV-4 as a means of discharging treated ground water. Option G consists of discharge to the ground water, using infiltration galleries, reinjection wells or a combination of the two. Based on existing information, a detailed discharge plan cannot be developed at this time. Figure 6-12 provides the general location of a ground water recharge system; the actual location would be designed to be upgradient of contaminated ground water areas and would be used to enhance the flushing of contaminants towards the ground water extraction system. Due to classification of ground water at Site 10 as GAA Non-attainment, the discharge of treated ground water would have to comply with federal, state and local requirements.

6.7.11.2 Evaluation

<u>Effectiveness</u> - Discharge to ground water could potentially be an effective method of handling the treated ground water, based on the sands and gravels present at the site. Additional hydrogeologic information is required to conduct a more detailed evaluation of this discharge option. By recharging treated ground water, an added element of hydraulic control would be provided

to the ground water extraction system. Common operational problems associated with ground water recharge systems include physical clogging of the systems.

<u>Implementability</u> - Implementation of a reinjection well or infiltration gallery system would require construction of the reinjection system and compliance with applicable federal, state and local reinjection discharge regulations. Technically, reinjection of treated ground water to the aquifer is expected to be achievable due to the transmissivity of the aquifer.

<u>Cost</u> - The major costs of implementation of a reinjection system are the construction and maintenance costs. The cost of Option G is initially estimated at a present worth value of \$80,000, based on the assumed installation of an infiltration gallery (see Appendix F).

6.7.12 Alternative IV-4, Option H - Discharge (Discharge to Surface Water)

6.7.12.1 Description

This technology option would be incorporated into Alternative IV-4 as a means of discharging treated ground water. Option H consists of discharge to surface water using direct discharge via a dedicated pipe. The nearest surface water body is to the north of the site (see Figure 1-7).

6.7.12.2 Evaluation

<u>Effectiveness</u> - Discharge to surface water would be an effective method of handling the treated ground water. Surface water discharge typically requires minimal maintenance activities.

<u>Implementability</u> - Implementation of discharge to surface water would require the construction of a dedicated discharge pipe. It would also require compliance with the surface water discharge requirements.

<u>Cost</u> - The major costs of implementation of a discharge to surface water system are the costs associated with installation of the dedicated piping and

discharge monitoring costs. The cost of Option H is initially estimated at a present worth value of \$50,000 (see Appendix F).

6.8 Selection of Alternatives for Detailed Analysis

A comparative analysis of the individual alternatives based on the three evaluation criteria is conducted to allow the elimination of selected alternatives from the detailed analysis process.

6.8.1 Effectiveness

With respect to long-term effectiveness, those alternatives which involve reductions in the toxicity, mobility or volume of contamination and contaminant sources will provide the greatest protection. With respect to short-term effectiveness, those alternatives which are protective during the construction and implementation period and which achieve remedial response objectives within a timely manner are most effective. The ability of an alternative to handle the contaminated media and its reliability are also considered in the effectiveness analysis.

For the alternatives developed, those that offer the greatest long-term effectiveness, due to the removal/treatment of contaminated soils or ground water, typically have increased short-term risks associated with their implementation, due to the required disruption of the waste materials or on-site treatment operations.

Alternative VI-4, soil and ground water treatment, provides the greatest long-term effectiveness by treating or disposing of the contaminated soil and ground water. With respect to the soil, the soil excavation and treatment options (Options B and C) provide the greatest long-term effectiveness by treating the soil contaminants, whereas Option A, soil excavation and

disposal, provides no treatment but contains the soil contamination. Option C utilizes stabilization, a more proven technology than Option B, soil washing. However, Option B is expected to require less long-term maintenance than Option C. All of the soil treatment/disposal options provide protection of human health by remediating the contaminated soils. With respect to ground water, both treatment options evaluated (Options E and F) may be effective in the treatment of contaminated ground water. Without additional hydrogeologic information, the effectiveness of ground water extraction and discharge options (Options D, G, and H) are difficult to compare at this time.

Of the remaining alternatives, the Alternative VI-3 options, containment provided by a RCRA Subtitle D soil cap, with or without a slurry wall, provide the next level of long-term effectiveness through a reduction in risks associated with direct contact with contaminated surficial soils. Option B of Alternative VI-3 provides greater potential long-term effectiveness by implementing a slurry wall to minimize ground water flow through potentially contaminated areas. Alternative VI-2 also provides protection against potential human exposures but to a lesser degree, through the use of deed restrictions and fencing. Both Alternatives VI-3 and VI-2 require long-term maintenance, which may be complicated by the scheduled base closure. Alternative VI-1, no action, provides the least long-term effectiveness because it does not address soil or ground water contamination. The no action alternative could be protective with respect to soil exposures in a non-residential use scenario. With respect to ground water, however, it does not address the ground water contaminants which exceed MCLs in a GAA Non-attainment ground water area.

6.8.2 Implementability

Implementability is a measure of the technical and administrative feasibility of constructing, operating and maintaining a remedial action alternative. Alternative VI-1, no action, and Alternative VI-2, ground water monitoring with deed restrictions and fencing, are the most implementable alternatives, although Alternative VI-2 requires long-term maintenance. Alternative VI-3 would follow in terms of implementability, with Option A, the soil cap, being more implementable than Option B, the soil cap combined with the slurry wall. Alternative VI-4 is the least implementable alternative, requiring soil excavation and handling and ground water extraction, treatment and discharge. The implementation of all soil remediation options is also complicated by the volume of soil requiring remediation. The implementation of Option A, soil excavation and off-site disposal, is limited by the required identification of a landfill able to accept the excavated soil. Implementation of Option B, soil excavation and treatment using soil washing is limited by the developing nature of the technology and the limited number of vendors. Implementation of Option C, stabilization and solidification, is limited by the required handling/disposal of the solidified materials. Ground water treatment options (Options E and F) are both easily implemented. implementability of ground water extraction and discharge options will be more easily evaluated following additional site investigations.

6.8.3 Cost

Alternative VI-1, no action, is the lowest cost alternative, closely followed by Alternative VI-2, ground water monitoring with deed restrictions and fencing. The soil cap option (Option A) of Alternative VI-3 is less expensive than Option B, soil capping with a slurry wall. The soil and ground

water treatment options, when combined in Alternative VI-4, comprise the highest remedial cost. The estimated soil treatment option costs are extremely high, ranging from \$13,000,000 to \$40,000,000. The ground water treatment option costs range from \$1,700,000 to \$3,400,000.

6.8.4 Selection of Alternatives for Further Consideration

Based on the comparative analysis presented in the previous section, no alternatives are proposed to be eliminated from the range of alternatives undergoing detailed analysis. However, the soil disposal/treatment options (Options A, B and C) are proposed to be eliminated from further consideration. This determination is based on the uncertainties associated with the calculation of the risk-based cleanup levels or the applicability of the calculated risk-based cleanup levels to Site 10. These uncertainties impact the alternatives' effectiveness evaluation in terms of the ability of the alternatives to meet the cleanup level objectives and to provide greater protection of human health and the environment.

PAHs and beryllium were detected in surface soils at Site 10 at levels exceeding risk-based cleanup levels. Arsenic was also detected at a level exceeding the risk-based cleanup level in a surface soil sample which was collected during the Phase I RI as a background sample. With respect to PAHs, as noted previously in Section 6.3.2, in all SVOC analyses of surface soil samples at Site 10, detection limits exceeded the calculated risk-based cleanup levels for PAHs. Therefore, the one sample at Site 10 which exhibited PAHs at levels exceeding risk-based cleanup levels was identified on the basis of qualified data (i.e., samples where PAHs were detected at J-qualified or estimated levels). For the arsenic and beryllium which were detected at levels exceeding risk-based cleanup levels, the calculated risk-based cleanup

levels are less than the geometric mean concentration for background soils in the eastern U.S. (USGS, 1984). Site-specific background soil concentrations require further definition, as will be done in the Phase II RI, before the applicability of the calculated risk-based cleanup levels can be determined.

Further supporting the elimination of soil remediation options is the significant cost associated with implementation. Active soil restoration options range in cost from \$13 million to \$40 million.

Potential cancer risks associated with exposures to soils at Site 10 range from 10^{-5} for future residential use to the 10^{-6} to 10^{-7} range for existing site use. Therefore, risks are within the acceptable range of 10^{-4} to 10^{-6} for remedial actions at Superfund sites and, with the proposed excessing of the site to the Army, these residual risks may be considered to be acceptable for this site. With no ARARS/TBCs exceeded for identified soil contaminants, the elimination of active restoration alternatives is considered appropriate for this site. The containment alternative will be retained for further consideration in addressing the potential exposure pathways at the site.

If the Phase II RI results confirm that potential unacceptable risks to human health or the environment are associated with PAHs and inorganics at this site and that detected contaminant levels are attributable to the site and are not naturally occurring, the active restoration remedial alternatives will be reconsidered.

All of the remaining alternatives and technology options will be retained for detailed analysis. This will allow for the further consideration of a wide variety of remedial options providing a range in the degree of treatment for soil and ground water contamination at the site.

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TABLES

TABLE 2-1 FEDERAL CHEMICAL-SPECIFIC ARARS AND TBCS FEASIBILITY STUDIES SITES 05, 06, 08, 10, 12, 13, AND 14 NCBC - DAVISVILLE

MEDIA	REQUIREMENT	STATUS	SYNOPSIS	APPLICABILITY TO SITE CONDITIONS
Ground	Water — — Safe Drinking Water Act (40 CFR 141.11 – .16 and 141.60 – .63) Maximum Contaminant Levels (MCL's)	Applicable or Relevant and Appropriate	MCL's directly apply to "public water systems", defined as systems with at least 15 connections which service a minimum of 25 persons.	Ground water at NCBC is not a current source of drinking water, but is classified as GB at Sites 05, 06, 13, and 14, and as GAA Non-attainment at Sites 08, 10, and 12. MCLs are therefore applicable or may be but may be relevant and appropriate. Contaminant concentrations are compared to MCLs to assess potential risks associated with ingestion of ground water.
	Safe Drinking Water Act (40 CFR 141.50 – .52) Maximum Contaminant Level Goals (MCLGs)	Applicable or Relevant and Appropriate	Non-enforceable health goals for public water supply systems, set at levels which result in no known or anticipated adverse health effects.	Ground water at NCBC is not a current source of drinking water, but is classified as GB at Sites 05, 06, 13, and 14 and as GAA Non-attainment at Sites 08, 10, and 12. MCLGs are therefore applicable or may be relevant and appropriate. Non-zero MCLGs are to be used as remedial goals for current or potential sources of drinking water, per the NCP (40 CFR 300). Contaminant concentrations are compared to MCLGs to assess potential risks associated with ingestion of ground water.
	Resource Conservation and Recovery Act, Subpart F (40 CFR 264.94) Ground Water Protection Standards, Alternate Concentration Limits	Applicable or Relevant and Appropriate	Sets ground water protection standards for 14 pesticides and metals or allows for the development of alternate concentration limits for facilities which treat, store or dispose of hazardous waste.	Ground water at NCBC is not a current source of drinking water, but is classified as GB at Sites 05, 06, 13, and 14, and as GAA Non-attainment at Sites 08, 10, and 12. RCRA ground water concentration limits are therefore applicable or may be relevant and appropriate.
	USEPA Risk Reference Doses (RfDs)	To Be Considered	Toxicity values for evaluating noncarcinogenic effects resulting from exposures to contamination.	USEPA RfDs are used to characterize risks due to noncarcinogens in ground water.
	Lifetime Health Advisories	To Be Considered	Guidelines developed based on toxicity for noncarcinogenic compounds	TBC criteria due to the presence of contaminants in ground water.

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TABLE 2-1, continued FEDERAL CHEMICAL-SPECIFIC ARARS AND TBCS FEASIBILITY STUDIES SITES 05, 06, 08, 10, 12, 13, AND 14 NCBC - DAVISVILLE

MEDIA	REQUIREMENT	STATUS	SYNOPSIS	APPLICABILITY TO SITE CONDITIONS
Ground	Water (cont.) USEPA Human Health Assessment Group Cancer Slope Factors (CSFs)	To Be Considered	A slope factor is used to estimate an upper—bound probability of an individual developing cancer as a result of a lifetime of exposure to a particular level of a potential carcinogen.	USEPA CSFs are used to compute the individual incremental cancer risk resulting from exposure to certain compounds.
Surface	Water			
·	Clean Water Act (40 CFR 121) Ambient Water Quality Criteria (AWQC)	To be determined	Non-enforceable guidelines established for the protection of human health and/or aquatic organisms.	AWQC will be applicable to remedial alternatives which involve discharges to surface water.
	Clean Water Act (40 CFR 401.15) Effluent Discharge Limitations	To be determined	Regulates the discharge of contaminants from an industrial point source.	Regulations will be applicable to remedial alternatives which involve discharges to surface water.
Soils/Su	faces		··	
	Toxic Substances Control Act (40 CFR 761.125)	Relevant and Appropriate	Establishes PCB cleanup levels for soils and solid surfaces.	Applicable to spills of materials containing PCBs at concentrations of 50ppm or greater that occurred after May 4, 1987. While not applicable to NCBC Davisville sites, these requirements may be relevant and appropriate.
•	Interim Guidance on Establishing Soil Lead Cleanup Levels at Superfund Sites (OSWER Directive 9355.4-02)	To Be Considered	Sets forth an interim soil cleanup level for lead at 500 to 1000 ppm.	Will be considered at sites with lead as a soil contaminant.

TABLE 2-1, continued FEDERAL CHEMICAL-SPECIFIC ARARS AND TBCs FEASIBILITY STUDIES SITES 05, 06, 08, 10, 12, 13, AND 14 NCBC - DAVISVILLE

MEDIA	REQUIREMENT	STATUS	SYNOPSIS	APPLICABILITY TO SITE CONDITIONS
Air——	Clean Air Act (40 CFR 50) National Ambient Air Quality Standards (NAAQS)	To be determined	Establishes maximum levels for pollutants and particulates within air quality control districts.	Potential ARARS for alternatives involving remedial actions which impact ambient air (i.e. incinerators, soil venting, etc.).
	Clean Air Act (40 CFR 60) New Source Performance Standards (NSPS)	To be determined	Establishes emissions limitations for new sources.	Potential ARARS for alternatives involving treatment methods which emit pollutants.
	Clean Air Act (40 CFR 61) National Emissions Standard for Hazardous Air Pollutants	To be determined	Establishes emissions standards for hazardous air pollutants.	Potential ARARS for alternatives involving treatment methods which emit hazardous air pollutants.

TABLE 2-2 STATE CHEMICAL-SPECIFIC ARARS AND TBCs FEASIBILITY STUDIES SITES 05, 06, 08, 10, 12, 13, AND 14 NCBC - DAVISVILLE

MEDIA	REQUIREMENT	STATUS	SYNOPSIS	APPLICABILITY TO SITE CONDITIONS
Ground	Water – – RI Ground Water Protection Act (RIGL, 46–13 et seq.) Public Drinking Water Regulations	Applicable	Establishes provisions for the protection and management of potable drinking waters, including the development of ground water classifications and associated standards which specify maximum contaminant levels for each classification.	Ground water at NCBC is not a current source of drinking water, but is classified as GB at Sites 05, 06, 13, and 14, and as GAA Non-attainment at Sites 08, 10, and 12. These regulations are applicable and contaminant concentrations will be compared to the established ground water quality standards.
	Water RI Water Pollution Control Law (RIGL 46-12 et seq.) RI Water Quality Standards	To be determined	Establishes water use classification and water quality criteria for all waters of the state. Also establishes acute and chronic	Regulation will be applicable for remedial alternatives which involve discharges to surface water.
	rfaces Soil Cleanup Standards (Guidance)	To Be Considered	water quality criteria for the protection of aquatic life. A PCB cleanup standard of 1 ppm is used by RIDEM, while RIDEM and the Rhode	To be considered at sites with PCB or lead soil contamination.
			Island Department of Health-Risk Assessment consider a safe lead level in soil (total) to be under 300 ppm.	
	RI Hazardous Waste Management Act of 1987 (RIGL 23-19.1 et seq.) Proposed RI Rules and Regulations for the Investigation and Remediation of Hazardous Material Release		Requires investigation and/or remediation of PCBs exceeding 10 ppm in any environmental media and/or 2 micrograms/ 100 sq.cm on any surface.	To be considered at sites with PCB contamination.
Air——	RI Clean Air Act (RIGL Title 23, Chapter 23) Air Pollution Control Regulation Standards	To be determined	Establishes maximum ambient levels for criteria pollutants.	Potential ARARs for remedial alternatives involving treatment methods which emit criteria pollutants.

TABLE 2-3 FEDERAL LOCATION-SPECIFIC ARARS AND TBCs FEASIBILITY STUDIES SITES 05, 06, 08, 10, 12, 13, AND 14 NCBC - DAVISVILLE

MEDIA	REQUIREMENT	STATUS	SYNOPSIS	APPLICABILITY TO SITE CONDITIONS
Vetland	ds – – Executive Order 11990	To be determined	Regulates activities conducted in a wetland area to minimize the destruction, loss, or degradation of the wetlands.	Regulation will be applicable if implementation of a remedial action impacts wetland areas.
	Wetlands Construction and Management Procedures (40 CFR 6, Appendix A)	To be determined	Sets forth EPA policy for carrying out the provisions of Executive Order 11990 (see above)	Regulation will be applicable if implementation of a remedial action impacts wetland areas.
	Clean Water Act Section 404 (40 CFR 230; 33 CFR 320-330) Prohibition of Wetland Filling	To be determined	Prohibits the discharge of dredged or fill material to a wetland without a permit issued by the Corp of Engineers.	Regulation will be applicable if implementation of a remedial action impacts wetland areas.
oodpl	ains Executive Order 11988 Protection of Floodplains	To be determined	Regulates activities conducted in a floodplain to minimize adverse affects to the floodplain and ensure that flood hazards have been considered.	Potential ARARs as sites may be located within the 100-year floodplain zone.
	Flood Disaster Protection Act of 1973 Protection of Floodplain	To be determined	Regulates development in flood prone areas under FEMA.	Potential ARAR as sites may be located within the 100-year floodplain zone. Applicable to remedial alternatives conducted within floodplain zones.
	National Flood Insurance Act of 1968 (24 CFR 1909.124)	To be determined	Provides flood insurance for disaster relief and establishes flood control methods.	Potential ARAR as sites may be located within the 100-year floodplain zone. Applicable to remedial alternatives conducted within floodplain zones.

TABLE 2-3, continued FEDERAL LOCATION-SPECIFIC ARARS AND TBCs FEASIBILITY STUDIES SITES 05, 06, 08, 10, 12, 13, AND 14 NCBC - DAVISVILLE

MEDIA	REQUIREMENT	STATUS	SYNOPSIS	APPLICABILITY TO SITE CONDITIONS
Riv rs-	_			
•	Wild and Scenic Rivers Act (16 U.S.C. 1271) Protection of Riverways	To be determined	Regulates activities in vicinity of designated rivers.	Potential ARAR as Hunt River is located in close proximity to the NCBC-Davisville facility.
	Fish and Wildlife Coordination Act (16 U.S.C. 661) Protection of Wildlife Habitats	To be determined	Prevents the modification of a stream or river that affects fish or wildlife.	Potential ARAR as sites are located adjacent to streams.
/ildlife-	- -			
	Endangered Species Act of 1973 (16 U.S.C. 1531) Protection of Endangered Species	To be determined	Restricts activities in areas inhabited by registered endangered species.	Potential ARAR as surrounding wetlands may sustain endangered or threatened wildlife species.
istoric I	Places	•		
	National Historic Preservation Act of 1966 (16 USC 470, et seq.) Protection of Historic Lands and Structures	To be determined	Requires actions to take into account effects on properties included in or eligible for the National Register of Historic Places and minimizes harm to National Historic Landmarks.	Potential ARAR for activities which could impact historic places.
	Archeological and Historic Preservation Act of 1974 (132 CFR 229 & 229.4, 43 CFR 7 & 7.4) Protection of Archeological	To be determined	Restricts the use of land of known archeological or historical significance.	Potential ARAR for activities which could impact archeological or historic places.
	and Historic Lands			
armlan				
·	Farmland Protection Policy Act (7 USC 4201 et seq.) Protection of Significant/ Important Agricultural Lands	To be determined	Requires evaluation of direct and indirect effects of actions on remaining farms and farm support services.	Potential ARAR for activities which could impact off – site farmland areas.

TABLE 2-4 STATE LOCATION-SPECIFIC ARARS AND TBCS FEASIBILITY STUDIES SITES 05, 06, 08, 10, 12, 13, AND 14 NCBC - DAVISVILLE

MEDIA	REQUIREMENT	STATUS	SYNOPSIS	APPLICABILITY TO SITE CONDITIONS
Wetland				
	Rhode Island Wetlands Laws (RIGL 2-1-18 et seq.)	To be determined	Defines and establishes provisions for the protection of swamps, marshes and other freshwater wetlands in the state.	Regulation will be applicable if implementation of a remedial action impacts a wetland area.
Ground	Water			
	RI Ground Water Protection Act (RIGL, Title 46, Chapter 13.1 et. seq.)	Applicable	Provides for protection of state ground waters, requiring the maintenance or upgrading of existing or potential drinking water sources and prohibits the degradation of state ground water.	Applicable (ground water at Sites 08, 10, and 12 is designated GA-NAA; at other sites ground water is designated GB).
Surface	Water – – RI Water Pollution Control Law (RIGL 46 – 12 et seq.) Rhode Island Water Quality Standards	To be determined	Provides for the restoration and preservation of state surface waters.	Regulations will be applicable if existing contamination or implementation of a remedial action impacts surface water.

TABLE 2-5 FEDERAL ACTION-SPECIFIC ARARS AND TBCs FEASIBILITY STUDIES SITES 05, 06, 08, 10, 12, 13, AND 14 NCBC - DAVISVILLE

REQUIREMENT	STATUS	SYNOPSIS	APPLICABILITY TO SITE CONDITIONS
Resource Conservation and Recovery Act (RCRA) (40 CFR 262) Generator Requirements for Manifesting Waste for Off – Site Disposal	To be determined	Standards for manifesting, marking and recording off—site hazardous waste shipments for treatment/disposal.	This regulation will be applicable to alternatives which utilize an off—site disposal/treatment method for hazardous wastes.
RCRA (40 CFR 263) Transporter Requirements for Off-Site Disposal	To be determined	Standards for transporters of hazardous waste materials.	This regulation will be applicable to alternatives which utilize an off-site disposal/treatment method for hazardous wastes.
RCRA (40 CFR 264 and 265) Requirements for Hazardous Waste Treatment Facility Design and Operating Standards for Treatment and Disposal Systems	To be determined	Outlines specifications and standards for design, operation, closure and monitoring of performance for hazardous waste storage, treatment and disposal facilities.	Potential ARARs for alternatives which utilize a surface impoundment, waste pile, landfill, land treatment, incineration or miscellaneous treatment units for on—site storage/disposal/treatment of hazardous wastes.
RCRA (40 CFR 264.10-264.18) Subpart B - General Facility Standards	To be determined	General requirements regarding waste analysis, security, training, inspections, and location applicable to a facility which stores, treats or disposes of hazardous wastes (a TSDF facility).	This regulation may be applicable to remedial actions conducted at the facility, if the facility meets the definition of a TSDF.
RCRA (40 CFR 264.30-264.37) Subpart C - Preparedness and Prevention	To be determined	Requirements applicable to the design and operation, equipment, and communications associated with a TSDF facility, and to arrangements with local response departments.	This regulation may be applicable to remedial actions conducted at the facility, if the facility meets the definition of a TSDF.
RCRA (40 CFR 264.50-264.56) Subpart D - Contingency Plan and Emergency Procedures	To be determined	Emergency planning procedures applicable to a TSDF facility.	This regulation may be applicable to remedial actions conducted at the facility, if the facility meets the definition of a TSDF.

TABLE 2-5, continued FEDERAL ACTION-SPECIFIC ARARS AND TBCs FEASIBILITY STUDIES SITES 05, 06, 08, 10, 12, 13, AND 14 NCBC - DAVISVILLE

REQUIREMENT	STATUS	SYNOPSIS	APPLICABILITY TO SITE CONDITIONS
RCRA (40 CFR 264) Subpart F Ground Water Protection	To be determined	Ground water monitoring/corrective action requirements; dictates adherence to MCLs and establishes points of compliance.	Potential ARARs for alternatives which involve placement of hazardous wastes within solid waste management units, including surface impoundments, waste piles, and land treatment units.
RCRA (40 CFR 264) Subpart G Closure/Post Closure Requirements	To be determined	Establishes requirements for the closure and long—term management of a hazardous disposal facility.	Applicable to the closure of any hazardous waste management facility.
RCRA (40 CFR 264) Subpart I Use and Management of Containers	To be determined	Outlines use and management standards applicable to owners and operators of all hazardous waste facilities that store containers of hazardous waste.	Potential ARARs for remedial actions which require storage of hazardous waste in containers.
RCRA (40 CFR 264) Subpart L Waste Piles	To be determined	Regulates owners and operators of facilities that store or treat hazardous waste in piles.	Potential ARARs for remedial alternatives which utilize a waste pile for on-site storage/treatment of hazardous waste.
RCRA (40 CFR 264) Subpart O Incinerator Restrictions	To be determined	Outlines specifications and standards for incinerating hazardous waste.	Potential ARARs for alternatives which utilize incineration for on—site treatment of hazardous wastes.
RCRA (40 CFR 264.600 – 264.999) Subpart X – Miscellaneous Units	To be determined.	Environmental performance standards, monitoring requirements'and post—closure care requirements applicable to miscellaneous units (not otherwise defined in the RCRA regulations) used to treat, store or dispose of hazardous waste.	This regulation may be applicable to remedial actions involving hazardous waste treatment, storage or disposal in units not otherwise covered under RCRA regulations.

TABLE 2-5, continued FEDERAL ACTION-SPECIFIC ARARS AND TBCs FEASIBILITY STUDIES SITES 05, 06, 08, 10, 12, 13, AND 14 NCBC - DAVISVILLE

REQUIREMENT	STATUS	SYNOPSIS	APPLICABILITY TO SITE CONDITIONS
RCRA (40 CFR 268) Land Disposal Restrictions	To be determined	Identifies hazardous wastes that are restricted from land disposal and sets treatment standards for restricted wastes.	This regulation will be applicable to alternatives which utilize land disposal of hazardous wastes.
Toxic Substances Control Act (15 USC. Sect. 2601) Subpart D - Storage and Disposal Requirements for PCBs	To be determined	Establishes requirements for the storage, landfilling, and incineration of PCBs.	This regulation may be applicable or relevant and appropriate to alternatives which involve handling of PCBs or PCB—contaminated materials.
Safe Drinking Water Act (40 CFR 144 and 146) Underground Injection Control Requirements	To be determined	Establishes the general requirements, technical criteria and standards for underground injection wells.	This regulation will be applicable to alternatives in which treated water is discharged back to the ground water.
Clean Water Act (40 CFR 122-125) National Pollutant Discharge Elimination System (NPDES) Permit Requirements	To be determined	Permits contain applicable effluent standards (i.e., technology—based and/or water quality—based), monitoring requirements, and standards and special conditions for discharge.	This regulation will be applicable to alternatives in which treated water is discharged to surface waters or back to the ground water.
Clean Water Act (40 CFR 403) Discharge to Publicly – Owned Treatment Works (POTW)	To be determined	A national pretreatment program designed to protect municipal wastewater treatment plants and the environment from damage that may occur when hazardous, toxic or other non-domestic wastes are discharged into a sewer system.	This regulation is applicable to alternatives in which waters are discharged to a POTW.
Clean Water Act (40 CFR 404) Requirements for Discharge of Dredged or Fill Material	To be determined	Prohibits activities that impact a wetland unless no other practical alternatives are available.	ARARs for alternatives conducted in or around adjacent wetlands.

TABLE 2-5, continued FEDERAL ACTION-SPECIFIC ARARS AND TBCs FEASIBILITY STUDIES SITES 05, 06, 08, 10, 12, 13, AND 14 NCBC - DAVISVILLE

REQUIREMENT	STATUS	SYNOPSIS	APPLICABILITY TO SITE CONDITIONS
Fish & Wildlife Coordination Act (16 U.S.C. 661) Protection of Wildlife Habitats	To be determined	Regulates actions which cause the impoundment, diversion or modification of a body of water, or affect fish and wildlife.	ARARs for alternatives conducted around wetlands and adjacent streams.
Clean Air Act (40 CFR 50) National Ambient Air Quality Standards (NAAQS) – Particulates	To be determined	Establishes maximum concentrations for particulates and fugitive dust emissions.	ARARs for alternatives involving treatment methods which impact ambient air (i.e. incineration, soil venting, etc.).
Clean Air Act (40 CFR 50) New Source Performance Standards (NSPS)	To be determined	Requires Best Available Control Technology (BACT) for new sources, and sets emissions limitations.	ARARs for alternatives involving treatment methods which impact ambient air (i.e., incineration, soil venting, etc.).
Clean Air Act (40 CFR 61) Emissions Standards for Hazardous Pollutants (NESHAPS)	To be determined	Establishes emissions limitations for hazardous air pollutants.	Potential ARARs for alternatives using treatments (i.e., incineration, etc.) which result in emissions to the air.
Hazardous Materials Transportation Act (49 CFR 170, 171) Rules for Transportation of Hazardous Materials	To be determined	Procedures for packaging, labelling, manifesting, and off—site transport of hazardous materials.	This regulation will be applicable to alternatives which include off—site transport of hazardous materials.
Federal Water Pollution Control Act (40 CFR 220 – 233) Ocean Discharge Criteria	To be determined	Establishes general requirements for discharge into United States oceans.	This regulation will be applicable if waters are discharged to surface waters, which ultimately discharge to the Narragansett Bay.

TABLE 2-5, continued FEDERAL ACTION-SPECIFIC ARARS AND TBCs FEASIBILITY STUDIES SITES 05, 06, 08, 10, 12, 13, AND 14 NCBC - DAVISVILLE

REQUIREMENT	STATUS	SYNOPSIS	APPLICABILITY TO SITE CONDITIONS
Occupational Safety and Health Act (29 CFR 1904) Recordkeeping, Reporting and Related Regulations	To be determined	Outlines recordkeeping and reporting requirements.	These requirements will apply to all contractors/ subcontractors involved in hazardous activities.
Occupational Safety and Health Act (29 CFR 1910) General Industry Standards	To be determined	Establishes requirement for 40—hour training and medical surveillance of hazardous waste workers. Establishes Permissible Exposure Limits (PELs) for workers at hazardous waste operations and during emergency response.	These requirements will apply to all contractors/ subcontractors involved in hazardous activities.
Occupational Safety and Health Act (29 CFR 1926) Safety and Health Standards	To be determined	Regulations specify the type of safety equipment and procedures for site remediation/excavation.	These requirements will apply to all contractors/ subcontractors involved in hazardous activities.

TABLE 2-6 STATE ACTION-SPECIFIC APARs AND TBCs FEASIBILITY STUDIES SITES 05, 06, 08, 10, 12, 13, AND 14 NCBC - DAVISVILLE

REQUIREMENT	STATUS	SYNOPSIS	APPLICABILITY TO SITE CONDITIONS
RI Water Pollution Control			
RI Water Quality Regulations (RIGL 46-12 et seq.)	To be determined	Establishes general requirements and effluent limits for discharge to area waters.	This regulation will be applicable to alternatives in which treated water is discharged to area surface water or ground water.
RI Pollutant Discharge Elimination Systems (RIGL 46-12 et seq.)	To be determined	Permits contain applicable effluent standards (i.e., technology—based and/or water quality—based), monitoring requirements, and standards and special conditions for discharge.	This regulation will be applicable to alternatives in which treated water is discharged to area surface water or ground water.
RI Pretreatment Regulations (RIGL 46-12 et seq.)	To be determined	Establishes rules concerning pretreatment of water prior to discharge to a Rhode Island POTW.	This regulation will be applicable to alternatives which include discharge of waters to a POTW.
RI Underground Injection Control Regulations (RIGL 46-12 et seq.)	To be determined	Establishes the general requirements, technical criteria and standards for underground injection wells.	This regulation will be applicable to alternatives in which treated water is discharged back to the ground water via injection.
Public Drinking Water Laws (RIGL, Title 46, Chapter 14) Protection of Public Drinking Water	To be determined	Establishes rules concerning discharge to any source of water supply for drinking purposes.	Potential ARARs for alternatives which affect public drinking water supplies.
RI Ground Water Protection Act (RIGL, Title 46, Chapter 13.1) Protection of Ground Water	To be determined	Establishes ground water classifications and maximum contaminant levels for each classification.	Potential ARARs for alternatives involving the treatment of contaminated ground water. Will establish cleanup levels.
RI Hazardous Waste Management Act of 1978 (RIGL 2319.1 et seq.) Hazardous Waste Management Rules and Regulations and Proposed Amendments	To be determined	Rules and regulations for hazardous waste generation, transportation, treatment, storage, and disposal.	These rules will be applicable for alternatives which involve the on- or off-site management of hazardous wastes.

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TABLE 2-6, continued STATE ACTION - SPECIFIC ARARS AND TBCs FEASIBILITY STUDIES SITES 05, 06, 08, 10, 12, 13, AND 14 NCBC - DAVISVILLE

REQUIREMENT	STATUS	SYNOPSIS	APPLICABILITY TO SITE CONDITIONS
Proposed Rules and Regulations for the Investigation and Remediation of Hazardous Material Releases	To be determined	Proposed rules and regulations for the investigation and remediation of releases of hazardous materials.	These rules will be applicable to the design and operation of remedial systems.
RI Hazardous Substance Community Right to Know Act (RIGL, Title 23, Chapter 24.4) Public Right-to-Know Requirements	To be determined	Establishes rules for the public's right-to-know concerning hazardous waste storage and transportation.	These rules will be applicable for alternatives which involve the on- or off-site management of hazardous wastes.
RI Refuse Disposal Law Solid Waste Management Rules and Regulations and Proposed Amendments	To be determined	Rules and regulations for solid waste management facilities.	ARARs for alternatives involving the on-site storage and disposal of solid wastes.
RI Underground Storage Tanks Act (RIGL, Title 46, Chapter 12.1) Regulations for Underground Storage Facilities used for Petroleum Products and Hazardous Materials	To be determined	Permits and regulates installation, operation and closure of underground storage tanks.	ARARs for alternatives involving closure of existing underground storage tanks.
RI Clean Air Act (RIGL, Title 23, Chapter 23) General Air Quality and Air Emissions Requirements	To be determined	Sets emissions limitations for particulates and visible air contaminants.	ARARs for alternatives involving remedial actions which impact ambient air.
RI Coastal Resource Management Council (CRMC)	To be determined	Review and permit actions which impact coastal areas.	Alternatives which impact coastal areas will require CRMC approval.

TABLE 3-1
Site 05 - Transformer Oil Disposal Area
Comparison of Maximum Soil Contaminant Levels to Action Levels

		centraction Detected (ppm)			
Parameter	Surface Soils (0-2')	Subsurface Soils (>2')	Federal Action Level (ppm)	State Ac Guidance Level (ppm)	tion Levels Proposed Regulatory Level (ppm)
PCBs	0.33	ND.	10 ⁽¹⁾	1 ⁽³⁾	10/50 ⁽³⁾
LEAD	303	10.6	500-1,000(2)	300(4)	

ND - Not Detected

- (1) TSCA (40 CFR 761); Requirements for decontaminating spills in nonrestricted areas.
- (2) USEPA, OSWER Directive 9355.4-02, Interim Guidance on Establishing Soil Lead Cleanup Levels at Superfund Sites.
- (3) RIDEM Historic Cleanup Standard (1 ppm).

 RIDEM Proposed Amendments to the Rules and Regulations for Solid Waste Management Facilities defines solid waste as including any soil debris or other material with a concentration of 10 ppm or greater PCBs.

 RIDEM Proposed Amendments to the Rules and Regulations for Hazardous Waste Management defines Type 6 extremely hazardous waste as including waste which contains 50 ppm or greater PCBs.
- (4) RIDEM and RI Dept. of Health-Risk Assessment Guidance Level.

TABLE 3-2
Site 06 - Solvent Disposal Area
Comparison of Maximum Soil Contaminant levels to Action Levels

		centraction Detected (ppm)		·
Parameter	Surface Soils (0 – 2')	Subsurface Soils (>2')	Federal Action Level (ppm)	State Action Level (ppm)
LEAD	43.9	5.6	500-1,000 ⁽¹⁾	300 ⁽²⁾

⁽¹⁾ USEPA, OSWER Directive 9355.4-02, Interim Guidance on Establishing Soil Lead Cleanup Levels at Superfund Sites.

⁽²⁾ RIDEM and RI Dept. of Health-Risk Assessment Guidance Level.

TABLE 3-3
Site 13 - Disposal Area Northwest of Buildings W-3, W-4, and T-1
Comparison of Maximum Soil Contaminant Levels to Action Levels

		centraction Detected (ppm)				
Parameter	Surface Soils (0-2')	Subsurface Soils (>2')	Federal Action Level (ppm)	State Ac Guidance Level (ppm)	tion <u>Levels</u> Proposed Regulatory Level (ppm)	
					,	
PCB - 1254	1.9	ND	10(1)	1 ⁽³⁾	10/50(3)	
PCB - 1248	1.1	ND	10(1)	1 ⁽³⁾	10/50 ⁽³⁾	
PCB - 1260	4,563	, ND	10(1)	1 ⁽³⁾	10/50 ⁽³⁾	
LEAD	64.1	63.2	500-1,000 ⁽²⁾	300 ⁽⁴⁾		

ND - Not Detected

- (1) TSCA (40 CFR 761); Requirements for decontaminating spills in nonrestricted areas.
- (2) USEPA, OSWER Directive 9355.4-02, Interim Guidance on Establishing Soil Lead Cleanup Levels at Superfund Sites.
- (3) RIDEM Historic Cleanup Standard (1 ppm). RIDEM Proposed Amendments to the Rules and Regulations for Solid Waste Management Facilities defines solid waste as including any soil debris or other material with a concentration of 10 ppm or greater PCBs. RIDEM Proposed Amendments to the Rules and Regulations for Hazardous Waste Management defines Type 6 — extremely hazardous waste as including waste which contains 50 ppm or greater PCBs.
- (4) RIDEM and RI Dept. of Health-Risk Assessment Guidance Level.

TABLE 3-4

Site 06 — Solvent Disposal Area Comparison of Detected Ground Water Contaminants to Applicable or Relevant and Appropriate Requirements (ARARs) or To—be Considered Requirements (TBCs)

		FEDERA	L ARARs/TB	Cs	RHODE ISLAND -ARARS/TBCs-
Parameter	Maximum Concentration Detected in Ground Water (ppb)	MCL ¹ (ppb)	MCLG² (ppb)	SMCL ³ (ppb)	Ground Water ⁴ Quality Standards (ppb)
Inorganics					
Arsenic	2.1	50		•	50
Beryllium	7.3	4	4		
Chromium	81.6	100	100		50(Hexavskut)/100(Total)
Copper	85.8	1300*	•	1000	
Lead	63.2	15*			50/15 ^(P)
Nickel	67.9	100	100		•
Zinc	279	-		5000	
Barium	171	2000	2000		1000/2000 ^(P)
Iron	113000			300	
Manganese	2680			50	
Vanadium	156				
Aluminum	47900			50	
Cobalt	61.5				
Magnesium	17700				
Calcium	15300				
Sodium	89600				
Potassium	12400				
Cyanide	31.5	200	200		

- 1. MCL Maximum Contaminant Level. National Primary Drinking Water Regulations, Final Rule Amendments to SDWA, U.S. EPA, Effective July 1992; for beryllium and nickel, effective January 17, 1994.
- 2. MCLG— Maximum Contaminant Level Goal, based on health considerations only, Final Rule Amendments to SDWA, U.S. EPA, Effective July 1992; for beryllium and nickel, ffective January 17, 1994.
- 3. SMCL Secondary Maximum Contaminant Level, National Secondary Drinking Water Regulations, Final Rule Amendments to SWDA, U.S. EPA, Effective July 1992.
- 4. Water Quality Standards, Class GAA and Class GA ground waters, Rhode Island Regulation DEM-GW-01-92, May 1992. (P) = Proposed, F bruary 1993.
- *-Action levels representative of drinking wat r quality at the tap, U.S. EPA, May 7, 1991.

TABLE 3-5

Site 13 – Disposal Area Northwest of Buildings W-3, W-4, and T-1 Comparison of Detected Ground Water Contaminants to Applicable or Relevant and Appropriate Requirements (ARARs) or To-be Considered Requirements (TBCs)

		FEDERA	L ARARs/TB(Cs	RHODE ISLAND -ARARs/TBCs-
Parameter	Maximum Concentration Detected in Ground Water (ppb)	MCL ¹ (ppb)	MCLG ² (ppb)	SMCL ³ (ppb)	Ground Water ⁴ Quality Standards (ppb)
Volatile Organics 1,2-Dichloroethane Xylenes (Total)	2 1	5 10000	0 10000		5 10000 ^(P)
Semivolatiles Bis(2-ethylhexyl)phthalate Naphthalene 2-Methylnaphthalene	45 2 4.5	6	0		
Inorganics Antimony Arsenic Beryllium Cadmium	31.7 55.1 10.3 9.5	6 50 4 5	6 - 4 5		50 10/5 ^(P)
Chromium Copper Lead Mercury	166 236 158.5 0.2	100 1300* 15* 2	100	1000	50 ^(Hexavalent) /100 ^(Total) (P) 50/15 ^(P) 2
Nickel Zinc Barium Iron Manganese	179 709 345 188000 2170	2000	100 2000	5000 300 50	1000/2000 ^(P)
Vanadium Aluminum Cobalt Magnesium	257 144000 124.5 30100			50	
Calcium Sodium Potassium	20400 1070000 20300			•	

- 1. MCL Maximum Contaminant Level. National Primary Drinking Water Regulations, Final Rule Amendments to SDWA, U.S. EPA, Effective July 1992; for beryllium and nickel, effective January 17, 1994.
- 2. MCLG- Maximum Contaminant Level Goal, based on health considerations only, Final Rule Amendments to SDWA, U.S. EPA, Effective July 1992; for bis(2-ethylhexyl)phthalate (also known as di(2-ethylhexyl) phthalate), beryllium and nickel, effective January 17, 1994.
- 3. SMCL Secondary Maximum Contaminant Level, National Secondary Drinking Water Regulations, Final Rule Amendments to SWDA, U.S. EPA, Effective July 1992.
- 4. Water Quality Standards, Class GAA and Class GA ground waters, Rhode Island Regulation DEM-GW-01-92, May 1992. (P) = Proposed, February 1993.
- *-Action levels representative of drinking water quality at the tap, U.S. EPA, May 7, 1991.

TABLE 3-6 SUMMARY OF RISK-BASED CLEANUP LEVELS - SURFACE SOILS GROUP | SITES - SITES 05, 06, AND 13 NCBC - DAVISVILLE, RHODE ISLAND

	Surface Solls Maximum Detected Concentration	Estimated Reasonable Cance	10 ⁻⁶ Risk – Based ⁽²⁾ Cleanup Level	
Parameter	(ppm)	Adult/Youth (7-70 years)	Small Child (0-6 years)	(ppm)
	Site 05 - Trai	nsformer Oil Disposal Area	1	•
Benzo (a) anthracene	0.47	2.59 x 10 ⁻⁵	3.50 x 10 ⁻⁵	0.34
Benzo (a) pyrene	0.44	2.59 x 10 ⁻⁵	3.50 x 10 ⁻⁵	0.34
Benzo (b/k) fluoranthene	1.8	2.59 x 10 ⁻⁵	3.50 x 10 ⁻⁵	0.34
Chrysene	1.0	2.59 x 10 ⁻⁵	3.50 x 10 ⁻⁵	0.34
Indeno(1,2,3-cd)pyrene*	0.33	2.59 x 10 ⁻⁵	3.50 x 10 ⁻⁵	0.34
Arsenic	· 6.7	3.43 x 10 ⁻⁶	5.04 x 10 ⁻⁶	1.4
Beryllium	1.4	1.76 x 10 ⁻⁶	2.59 x 10 ⁻⁶	0.57
	Site 06 -	Solvent Disposal Area		
Benzo (a) anthracene*	0,14	1.45 x 10 ⁻⁶	1.97 x 10 ⁻⁶	0.34
Benzo (a) pyrene*	0.050	1.45 x 10 ⁻⁶	1.97 x 10 ⁻⁶	0.34
Benzo (b) fluoranthene*	0.054	1.45 x 10 ⁻⁶	1.97 x 10 ⁻⁶	0.34
Benzo (k) fluoranthene*	0.050	1.45 x 10 ⁻⁶	1.97 x 10 ⁻⁶	0.34
Chrysene*	0.068	1.45 x 10 ⁻⁶	1.97 x 10 ⁻⁶	0.34
	Site 13 - D	isposal Area Northwest		
Arsenic	1.6	8.21 x 10 ⁻⁷	1.21 x 10 ⁻⁶	1.4

^{* -} Maximum detected concentration does not exceed 1 x 10⁻⁶ cancer risk-based cleanup level.

General Note: At Sites 05 and 06, semivolatile detection limits exceeded PAH risk-based residential use cleanup levels for all samples.

^{(1) -} Risk estimates represent total cancer risk due to ingestion and dermal contact under future residential use, as presented in the Draft Final Remedial Investigation Report (TRC, May 1991)

^{(2) -} See Appendix A for discussion of risk-based cleanup level calculations

TABLE 3-7 SUMMARY OF RISK-BASED CLEANUP LEVELS - GROUND WATER GROUP I SITES - SITES 05, 06, AND 13 NCBC - DAVISVILLE, RHODE ISLAND

<u>Parameter</u>	Ground Water Maximum Detected Concentration (ppm)	Estimated ⁽¹⁾ Reasonable Maximum Exposure Cancer Risk	10 ⁻⁶ Risk – Based ⁽²⁾ Cleanup Level (ppm)	Estimated ⁽¹⁾ Non – Cancer Based Hazard Index	Hazard Index Based ⁽²⁾ Cleanup Level (ppm)
No Risk – Based Cacula	tions for Ground Water at	Site 05 - Transforme	er Oil Disposal Area		
		Site 06 - Solven	t Disposal Area		
Manganese	2.68	-	-	1.68	0.18
		Site 13 - Disposal	l Area Northwest		
Manganese	2.17	. -	_	1.36	0.18

^{(1) -} Risk estimates represent total cancer risk or total non-cancer hazard index ratio due to ingestion and dermal contact under future residential use, as presented in the Draft Final Remedial Investigation Report (TRC, May 1991)

^{(2) -} See Appendix A for discussion of risk-based cleanup level calculations

TABLE 3-8 TECHNOLOGIES WHICH PASSED SCREENING SURFACE SOIL/SEDIMENT GROUP I SITES - SITE 05, 06, 13

No Action

No Action

Institutional Control

- Deed Restrictions
- Fencing

Containment

RCRA Subtitle C Multi-Layer Cap
Asphalt Cap
Concrete Cap

RCRA Subtitle D Soil Cap

- Treatment/Disposal

 Off-Site Landfill
 - Stabilization/Solidification
 - On-Site Incineration
 - Off-Site Incineration
 Off-Site Slagging
 Plasma Reactor
 Thermal Desorption
 Soil Washing
 - Acid Extraction
 Dechlorination
 - Solvent Extraction Fungal Degradation Soil Flushing
- Process Technology Used to Formulate Remedial Alternatives

TABLE 3-9 ALTERNATIVES UNDERGOING PRELIMINARY SCREENING SURFACE SOIL/SEDIMENT GROUP I SITES - SITE 05, 06, 13

Alternative I-1

No Action

Alternative I-2

Limited Action

- Fencing/Deed Restrictions

Alternative I-3

Containment

- RCRA Subtitle D Soil Cap/Deed Restrictions

Alternative I-4

Active Restoration

- Off-Site Landfill/Off-Site Incineration or
- On-Site Incineration or
- Stabilization/Solidification or
- Acid Extraction and Solvent Extraction

TABLE 4 – 1
Site 08 – DPDO Film Processing Disposal Area
Comparison of Maximum Soil Contaminant Levels to Action Levels

	Maximum Concentraction Detected (ppm)						
Parameter	Surface Soils (0-2')	Subsurface Soils (>2')	Federal Action Level (ppm)	State Ac Guidance Level (ppm)	tion Levels Proposed Regulatory Level (ppm)		
PCBs	1.4	ND .	10 ⁽¹⁾	1 ⁽³⁾	10/50 ⁽³⁾		
LEAD	171	12.7	500-1,000(2)	300(4)			

ND - Not Detected

- (1) TSCA (40 CFR 761); Requirements for decontaminating spills in nonrestricted areas.
- (2) USEPA, OSWER Directive 9355.4-02, Interim Guidance on Establishing Soil Lead Cleanup Levels at Superfund Sites.
- (3) RIDEM Historic Cleanup Standard (1 ppm). RIDEM Proposed Amendments to the Rules and Regulations for Solid Waste Management Facilities defines solid waste as including any soil debris or other material with a concentration of 10 ppm or greater PCBs. RIDEM Proposed Amendments to the Rules and Regulations for Hazardous Waste Management defines Type 6 — extremely hazardous waste as including waste which contains 50 ppm or greater PCBs.
- (4) RIDEM and RI Dept. of Health-Risk Assessment Guidance Level.

TABLE 4-2 SUMMARY OF RISK-BASED CLEANUP LEVELS GROUP II SITE - SITE 8 (DPDO FILM PROCESSING AREA) NCBC - DAVISVILLE, RHODE ISLAND

	Surface Soils Maximum Detected	Estimated Reasor Exposure C	10 ⁻⁶ Risk-Based ⁽²⁾	
<u>Parameter</u>	Concentration (ppm)	Adult/Youth (7-70 years)	Small Child (0-6 years)	Cleanup Level (ppm)
Benzo (a) anthracene	0.41	1.79 x 10 ⁻⁶	1.35 x 10 ⁻⁶	0.34
Benzo (a) pyrene*	0.33	1.79 x 10 ⁻⁶	1.35 x 10 ⁻⁶	0.34
Benzo (b/k) fluoranthene	0.65	1.79 x 10 ⁻⁶	1.35 x 10 ⁻⁶	0.34
Chrysene	0.50	1.79 x 10 ⁻⁶	1.35 x 10 ⁻⁶	0.34
Dibenzo(a,h)anthracene*	0.14	1.79 x 10 ⁻⁶	1.35 x 10 ⁻⁶	0.34
Indeno(1,2,3-cd)pyrene*	0.07	1.79 x 10 ⁻⁶	1.35 x 10 ⁻⁶	0.34
Arsenic	2.6	9.74 x 10 ⁻⁷	1.43 x 10 ⁻⁶	1.4
Beryllium	1.4	1.76 x 10 ⁻⁶	2.59 x 10 ⁻⁶	0.57

^{* -} Maximum detected concentration does not exceed 1 x 10⁻⁶ risk-based cleanup level.

General Note: At Site 08, semivolatile detection limits exceeded PAH risk-based residential use cleanup levels for all samples.

^{(1) -} Risk estimates represent total cancer risk due to ingestion and dermal contact under future residential use, as presented in the Draft Final Remedial Investigation Report (TRC, May 1991)

^{(2) -} See Appendix A for discussion of risk-based cleanup level calculations.

TABLE 4-3 TECHNOLOGIES WHICH PASSED SCREENING SURFACE SOIL GROUP II SITE - SITE 08 (DPDO FILM PROCESSING AREA)

No Action

No Action

Institutional Control

- Deed Restrictions
- Fencing

Containment

RCRA Subtitle C Multi-Layer Cap Asphalt Cap Concrete Cap

• RCRA Subtitle D Soil Cap

Treatment/Disposal

- Off-Site Landfill Stabilization/Solidification
- Off-Site Incineration
 Off-Site Slagging
 Plasma Reactor
 Thermal Desorption
 Acid Extraction
 Dechlorination
- Fungal Degradation
 Soil Flushing
- - Process Technology Used to Formulate Remedial Alternatives

TABLE 4-4 ALTERNATIVES UNDERGOING PRELIMINARY SCREENING SURFACE SOIL GROUP II SITE - SITE 08 (DPDO FILM PROCESSING AREA)

Alternative II-1

No Action

Alternative II-2

Limited Action

- Fencing/Deed Restrictions

Alternative II-3

Containment

- RCRA Subtitle D Soil Cap/Deed Restrictions

Alternative II-4

Active Restoration

- Off-Site Landfill or
- Off-Site Incineration or
- Fungal Degradation

TABLE 5-1
Site 12 - Building 316
Comparison of Detected PCB Contaminant Levels to Action Levels

	N	laximum Conce	ntration Detected						•
	Removal Area		Outside of Remov	al Area	. •		S	state Action Level	
		Concrete			Federal Actio	n Level	Guidance Level	Proposed Re	gulatory Level
Parameter	Soils (ppm) (TRC) (0-2")	Chips (TRC) (ppm) (0-1/8")	Wipe Samples (TRC) (ug/100 cm²)	Concrete Chips (EPA) (ppm)	Indoor solid surfaces (ug/100 cm²)	Soil (ppm)	Soil, Debris, or Other Material (ppm)	Surface (ug/100 cm ²)	Soil, Debris, o Other Material (ppm)
PCBs - soil/chip	0.12	5.9		1,200		10(1)	1(3)		10/50 ⁽²⁾
- wipe			48	-	10 ⁽¹⁾			2/10 ⁽²⁾	

- (1) TSCA (40 CFR 761); Requirements for decontaminating spills in nonrestricted areas.
- (2) RIDEM Historic Cleanup Standard (1 ppm).

 RIDEM Proposed Amendments to the Rules and Regulations for Solid Waste Management Facilities defines solid waste as including any soil debris or other material with a concentration of 10 ppm or greater PCBs or 2 micrograms/100 sq. cm or greater via a wipe test.

 RIDEM Proposed Amendments to the Rules and Regulations for Hazardous Waste Management defines Type 6 extremely hazardous waste as including waste which contains 50 ppm or greater PCBs or 10 micrograms/100 sq. cm or greater via a wipe test.

Note: TRC sampling conducted April 11, 1991. EPA sampling conducted September 25 and 26, 1991.

TABLE 5-2
Site 14 - Building 38
Comparison of Detected PCB Contaminant Levels to Action Levels

	Maximum Concentration Detected									
	Removal Area		Outsic	le of Removal	Area			S	tate Action Leve	ı
Parameter	Soils (ppm) (TRC) (0-2")	Asphalt Chips (TRC) (ppm) (0-1/8")	Wipe Samples (TRC) (ug/100 cm²)	Asphalt Chips (EPA) (ppm)	Wipe Samples (EPA) (ug/100 cm²)	Federal Action Indoor solid surfaces (ug/100 cm²)	Soil (ppm)	Guidance Level Soil, Debris, or Other Material (ppm)	Proposed Re Surface (ug/100 cm ²)	gulatory Level Soil, Debris, o Other Materia (ppm)
PCBs - soil/chip	1.6	56		150			10 ⁽¹⁾	1 ⁽²⁾		10/50 ⁽²⁾
– wipe			69		82	10 ⁽¹⁾			2/10 ⁽²⁾	

- (1) TSCA (40 CFR 761); Requirements for decontaminating spills in nonrestricted areas.
- (2) RIDEM Historic Cleanup Standard (1 ppm).

 RIDEM Proposed Amendments to the Rules and Regulations for Solid Waste Management Facilities defines solid waste as including any soil debris or other material with a concentration of 10 ppm or greater PCBs or 2 micrograms/100 sq. cm or greater via a wipe test.

 RIDEM Proposed Amendments to the Rules and Regulations for Hazardous Waste Management defines Type 6 extremely hazardous waste as including waste which contains 50 ppm or greater PCBs or 10 micrograms/100 sq. cm or greater via a wipe test.

Note: TRC sampling conducted April 11, 1991.

EPA sampling conducted September 24 and 25, 1991.

TABLE 5-3 TECHNOLOGIES WHICH PASSED SCREENING BUILDING SURFACES AND SURFACE SOILS GROUP III SITES - SITE 12 (BUILDING 316) AND SITE 14 (BUILDING 38)

No Action

No Action

Institutional Control

- Deed Restrictions
- Site Access Restrictions

Removal

Building Demolition

• Floor Removal

Decontamination

Scarification
Drilling and Spalling

- Sealing
- Solvent Washing

• - Process Technology Used to Formulate Remedial Alternatives

TABLE 5-4 ALTERNATIVES UNDERGOING PRELIMINARY SCREENING BUILDING SURFACES AND SURFACE SOILS GROUP III SITES - SITE 12 (BUILDING 316) AND SITE 14 (BUILDING 38)

Alternative III-1

No Action

Alternative III-2

Limited Action

Site Access/Deed Restrictions

Alternative III-3

Containment

- Surface Sealing

Alternative III-4

Excavation/Treatment/Disposal

Removal with Off-Site Disposal/Incineration

Alternative III-5

Treatment

- Solvent Washing

TABLE 6 – 1
Site 10 – Camp Fogarty Disposal Area
Comparison of Maximum Soil Contaminant Levels to Action Levels

		centraction Detected (ppm)	•		
Parameter	Surface Soils (0-2')	Subsurface Soils (>2')	Federal Action Level (ppm)	State Action Level (ppm)	
LEAD	107	12.5	500-1,000 ⁽¹⁾	300 ⁽²⁾	

- (1) USEPA, OSWER Directive 9355.4-02, Interim Guidance on Establishing Soil Lead Cleanup Levels at Superfund Sites.
- (2) RIDEM and RI Dept. of Health-Risk Assessment Guidance Level.

TABLE 6-2

Site 10 – Camp Fogarty Disposal Area Comparison of Detected Ground Water Contaminants to Applicable or Relevant and Appropriate Requirements (ARARs) or To-be Considered Requirements (TBCs)

		·			
		FEDE	RAL ARARs/T	BCs	
Parameter	Maximum Concentration Detected in Ground Water (ppb)	MCL ¹ (ppb)	MCLG ² (ppb)	SMCL ³ (ppb)	Ground Water ⁴ Quality Standards (ppb)
Inorganics				-	
Beryllium Chromium	5.3 80.8	4 100	4 100		50 ^{(Hexxvalent})/100 ^{(Total})(P)
Copper Mercury	22.2 0.3	1300* 2	2	1000	2
Lead	140	15*			50/15 ^(P)
Nickel Zinc	48 203	. 100	100	5000	
Barium	115 7950	2000	2000	300	1000/2000 ^(P)
Iron Manganese	1120		200	500 50	
Vanadium Aluminum	6.4 6080			50	
Cobalt	7		0.000.000.000.000.000.000.000.000.000		
Magnesium Calcium	1540 6390				
Sodium Potassium	3290 1330				
		200	000		
Cyanide	31.5	200	200	•	

- 1. MCL Maximum Contaminant Level. National Primary Drinking Water Regulations, Final Rule Amendments to SDWA, U.S. EPA, Effective July 1992; for beryllium and nickel, effective January 17, 1994.
- 2. MCLG— Maximum Contaminant Level Goal, based on health considerations only, Final Rule Amendments to SDWA, U.S. EPA, Effective July 1992; for beryllium and nickel, effective January 17, 1994.
- 3. SMCL Secondary Maximum Contaminant Level, National Secondary Drinking Water Regulations, Final Rule Amendments to SWDA, U.S. EPA, Effective July 1992.
- 4. Water Quality Standards, Class GAA and Class GA ground waters, Rhode Island Regulation DEM-GW-01-92, May 1992. (P) = Proposed, February 1993.
- *-Action levels representative of drinking water quality at the tap, U.S. EPA, May 7, 1991.

TABLE 6-3
SUMMARY OF RISK-BASED CLEANUP LEVELS
GROUP VI SITE - SITE 10 (CAMP FOGARTY)
NCBC - DAVISVILLE, RHODE ISLAND

	Surface Soils Maximum Detected	Estimated Reason Exposure C	10 ⁻⁶ Risk-Based ⁽²⁾		
<u>Parameter</u>	Concentration (ppm)	Adult/Youth (7-70 years)	Small Child (0-6 years)	Cleanup Level (ppm)	
Benzo (a) anthracene	0.48	6.87 x 10 ⁻⁶	9.3 x 10 ⁻⁶	0.34	
Benzo (a) pyrene	0.40	6.87×10^{-6}	9.3×10^{-6}	0.34	
Benzo (b/k) fluoranthene	0.37	6.87×10^{-6}	9.3 x 10 ⁻⁶	0.34	
Chrysene	0.58	6.87×10^{-6}	9.3 x 10 ⁻⁶	0.34	
Dibenzo(a,h)anthracene*	0.09	6.87×10^{-6}	9.3 x 10 ⁻⁶	0.34	
Indeno(1,2,3-cd)pyrene*	0.19	6.87×10^{-6}	9.3 x 10 ⁻⁶	0.34	
Arsenic	2.3	1.18 x 10 ⁻⁶	1.73 x 10 ⁻⁶	1.4	
Beryllium	2.5	3.15×10^{-6}	4.62 x 10 ⁻⁶	0.57	

^{* -} Maximum detected concentration does not exceed 1 x 10⁻⁶ risk-based cleanup level.

^{(1) -} Risk Estimates represent total cancer risk due to ingestion and dermal contact under future residential use, as presented in the Draft Final Remedial Investigation Report (TRC, May 1991)

^{(2) -} See Appendix A for discussion of risk-based cleanup level calculations.

General Note: At Site 10, semivolatile detection limits exceeded PAH risk-based residential use cleanup levels for all samples.

TABLE 6-4 TECHNOLOGIES WHICH PASSED SCREENING SURFACE SOIL/GROUND WATER GROUP VI SITE - SITE 10 (CAMP FOGARTY DISPOSAL AREA)

Surface Soil

No Action

No Action

Institutional Control

- Deed Restrictions
- Fencing

Containment

RCRA Subtitle C Multi-Layer Cap Asphalt Cap Concrete Cap

RCRA Subtitle D Soil Cap

Treatment/Disposal

- Off—Site Landfill
- Stabilization/Solidification
 Off—Site Incineration
 Off—Site Slagging
 Plasma Reactor
- Soil Washing Acid Extraction Soil Flushing

Ground Water

No Action

No Action

Institutional Control

- Continued Ground Water Monitoring
- Deed Restrictions

Containment

- Capping
- Slurry Wall

Treatment/Disposal/Discharge

- Extraction Wells
 Well Points
- Interceptor Trench Off—Site POTW
- Ion Exchange Precipitation
- Membrane Microfiltration Filtration
 - Electrochemical
- Discharge to Ground Water
- Discharge to Surface Water Sanitary Sewer/POTW Discharge
- Process Technology Used to Formulate Remedial Alternatives

TABLE 6-5 ALTERNATIVES UNDERGOING PRELIMINARY SCREENING SURFACE SOIL/GROUND WATER GROUP VI SITE - SITE 10 (CAMP FOGARTY DISPOSAL AREA)

Alternative VI-1

No Action

Alternative VI-2

Limited Action

- Fencing/Deed Restrictions/Continued Ground Water Monitoring

Alternative VI-3

Containment

- RCRA Subtitle D Soil Cap and/or Slurry Wall

Alternative VI-4

Active Restoration

Soil Remediation:

- Off-Site Landfill or
- Soil Washing or
- Stabilization/Solidification

and Ground Water Restoration:

- Extraction Wells or
- Interceptor Trench

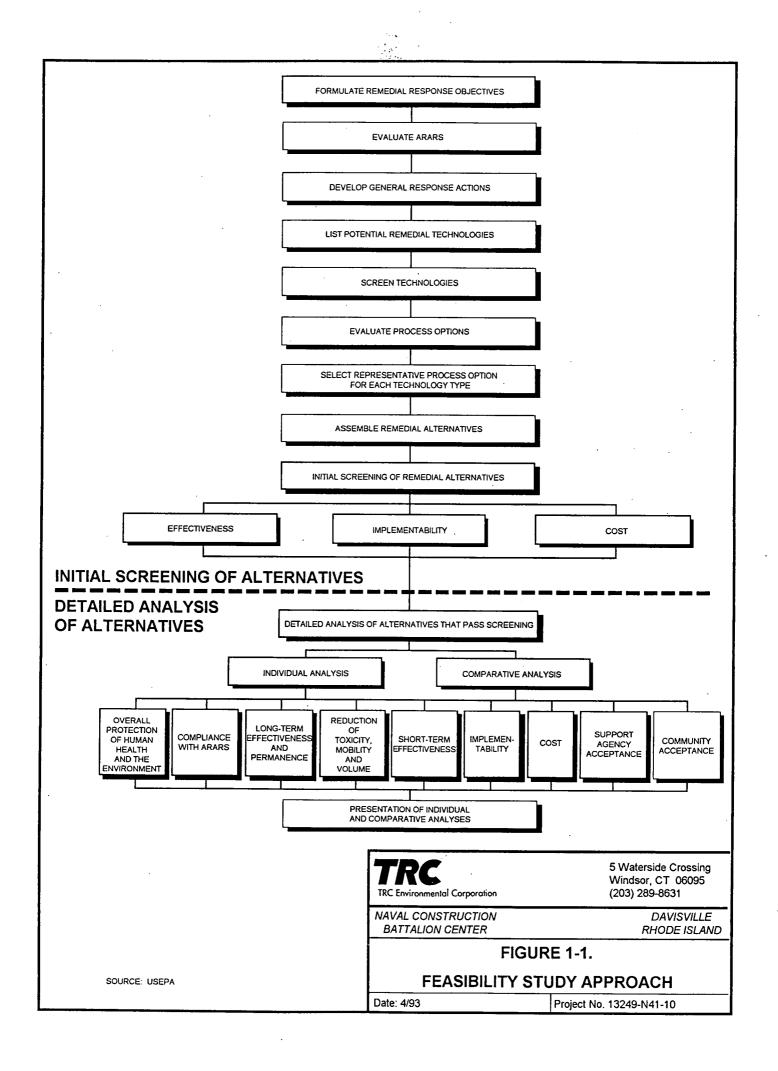
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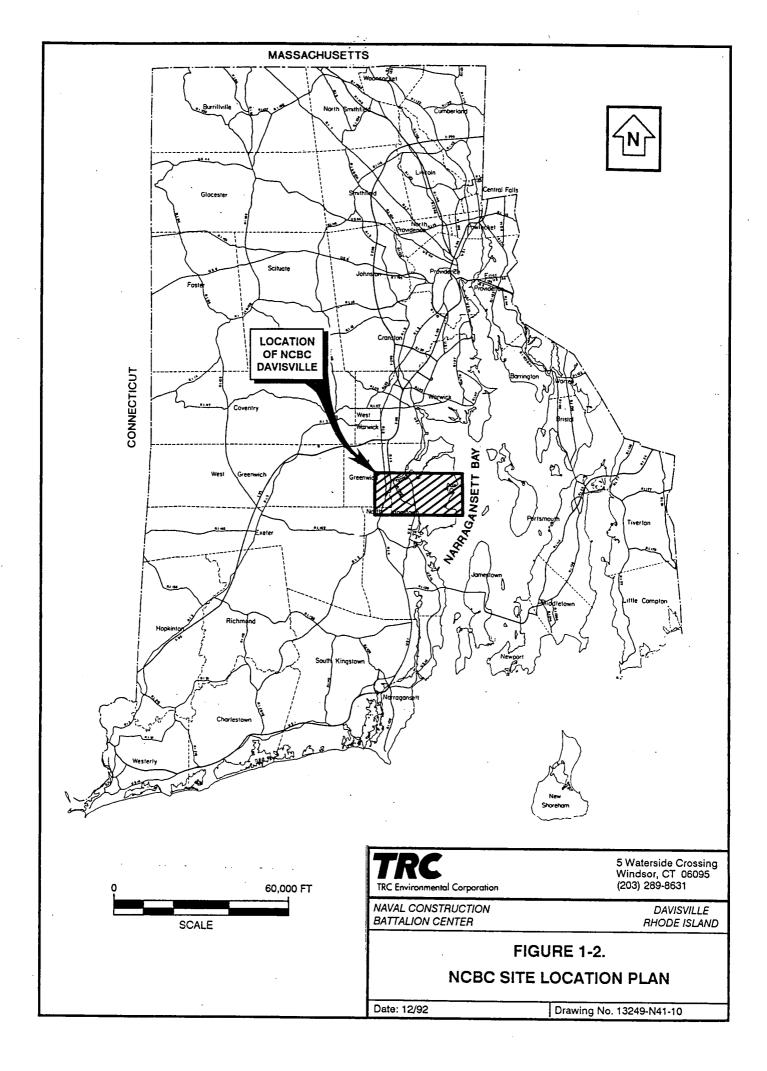
- Membrane Microfiltration or
- Ion Exchange

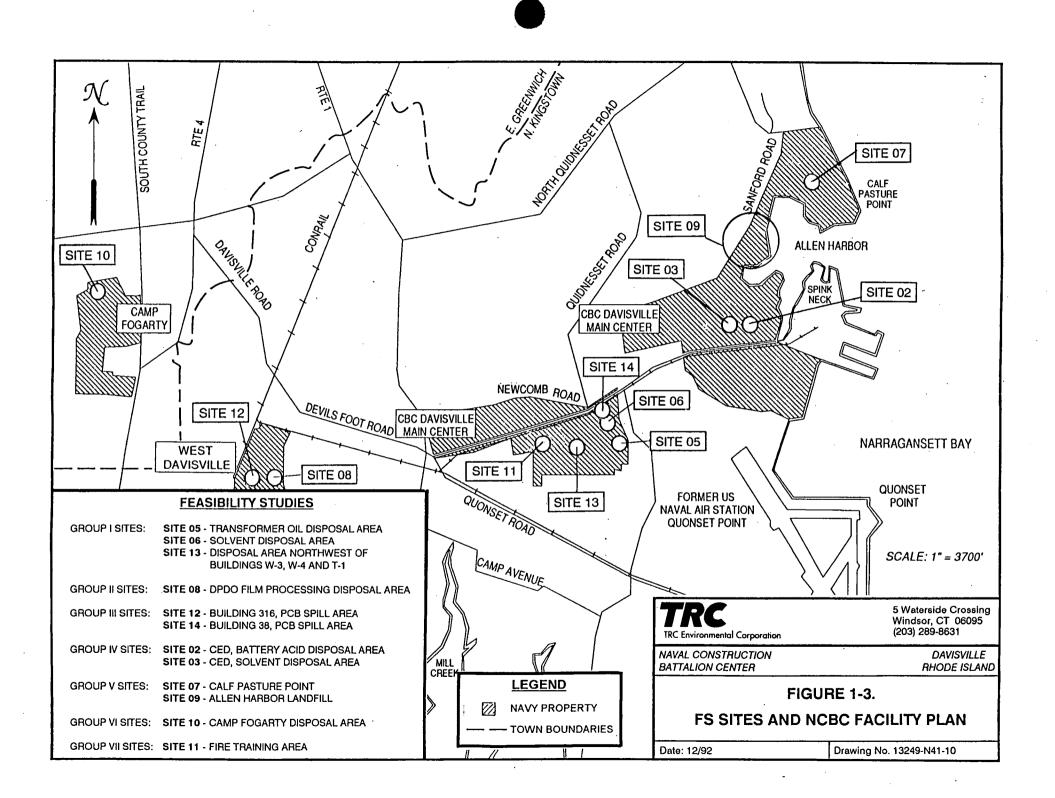
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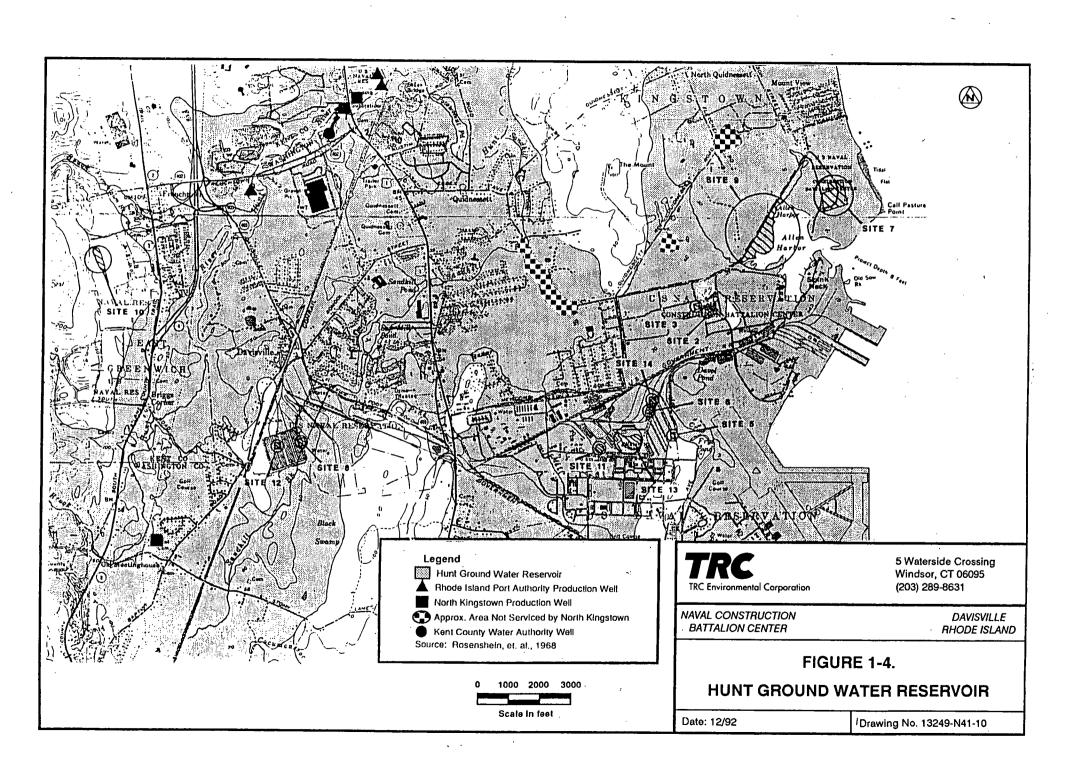
- Discharge to Ground Water or
- Discharge to Surface Water

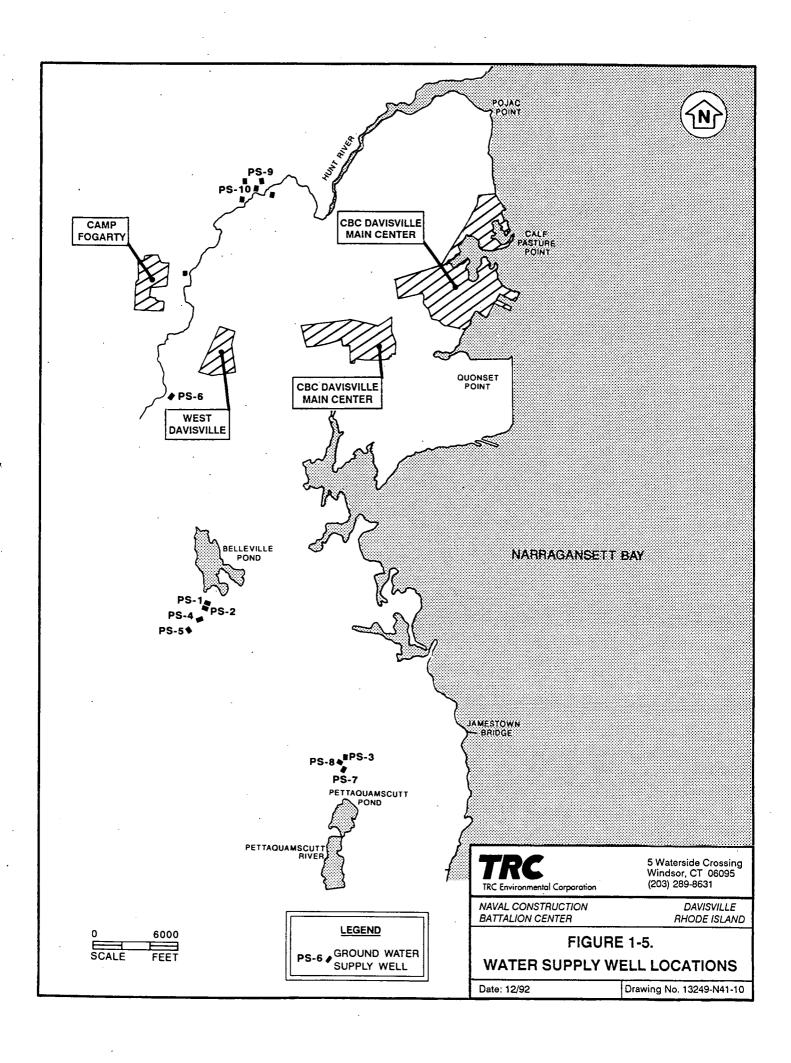
FIGURES

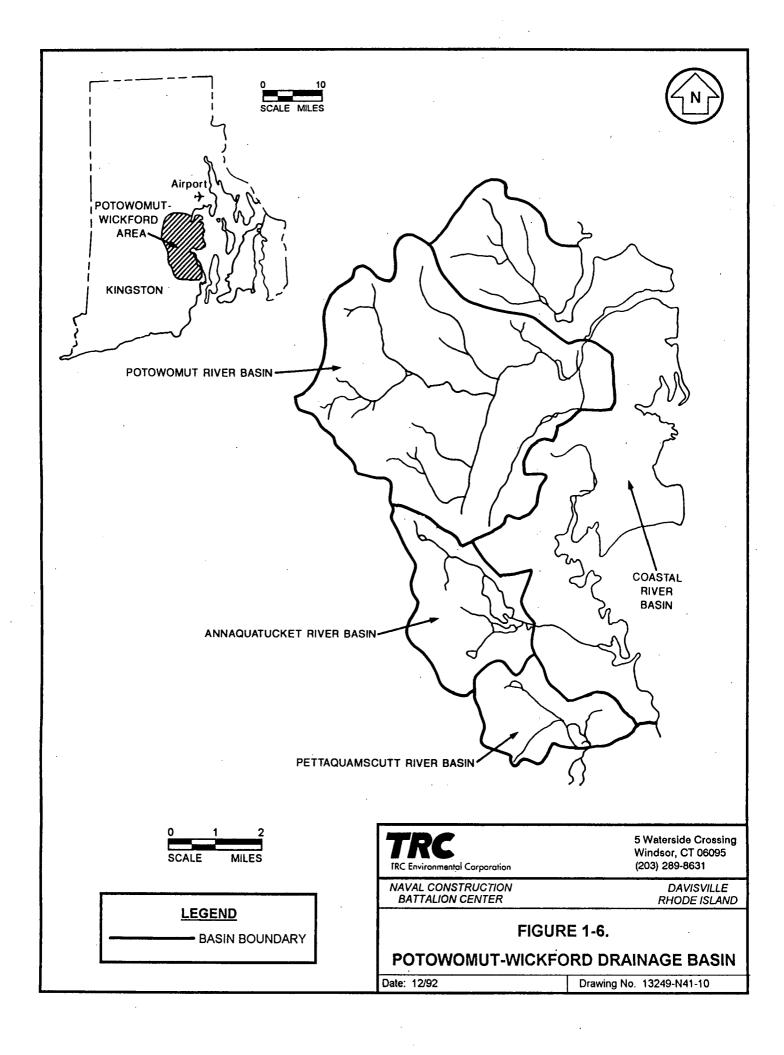


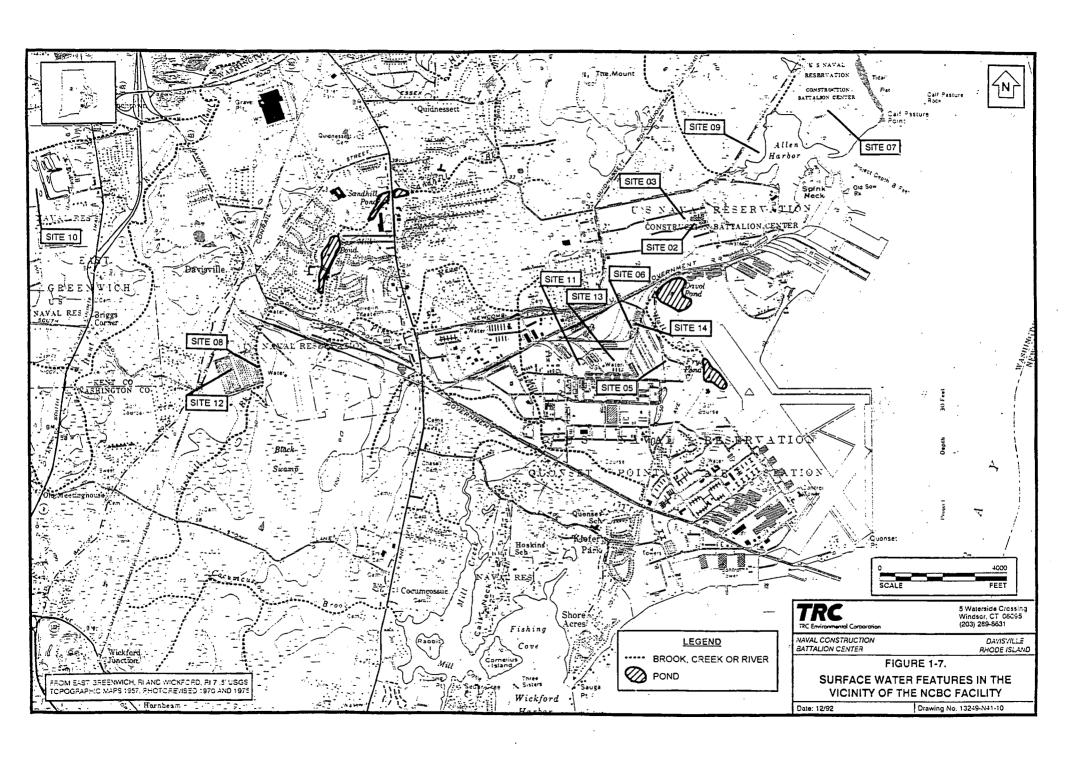


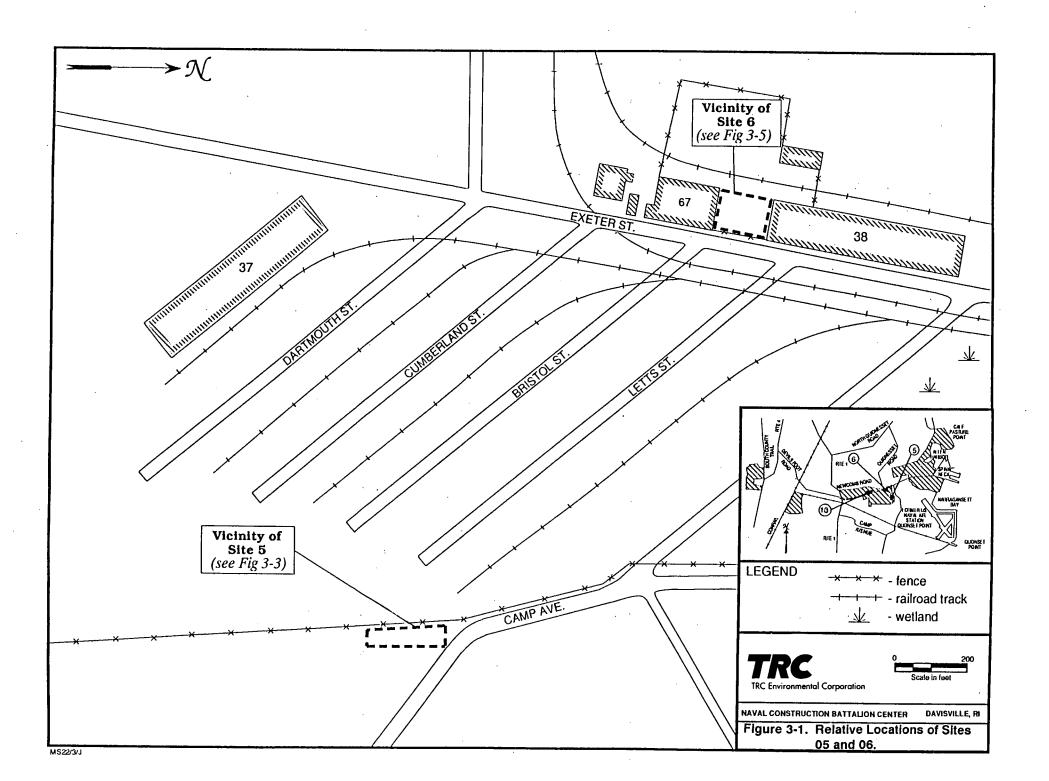


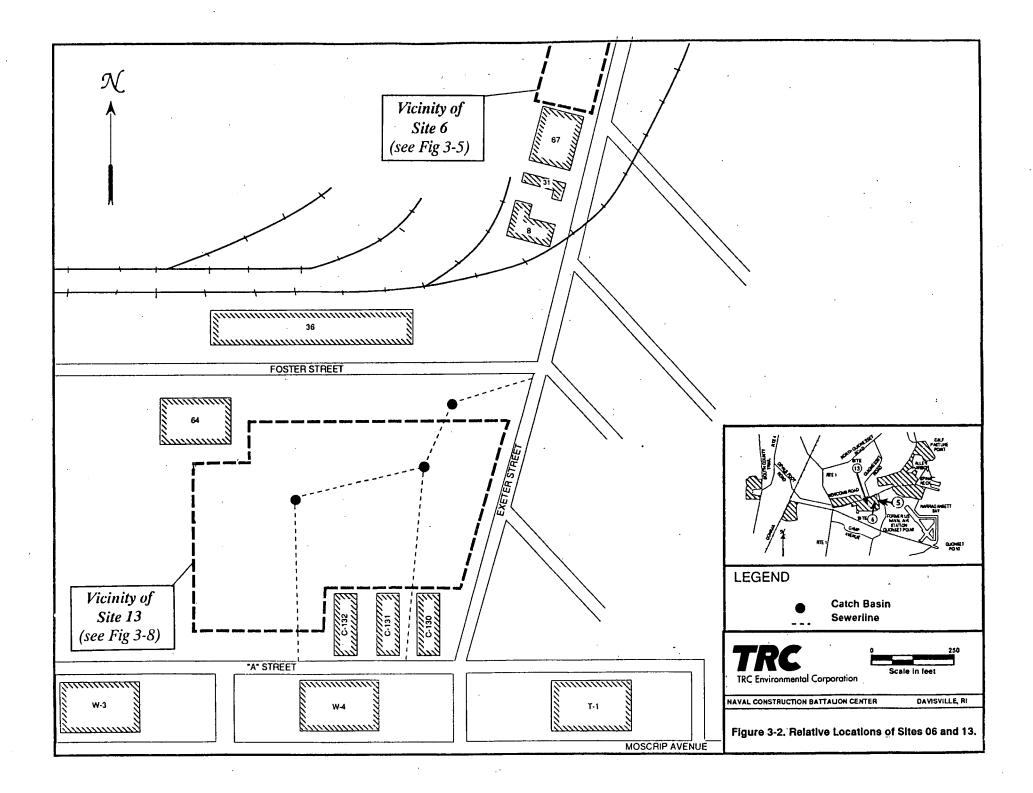


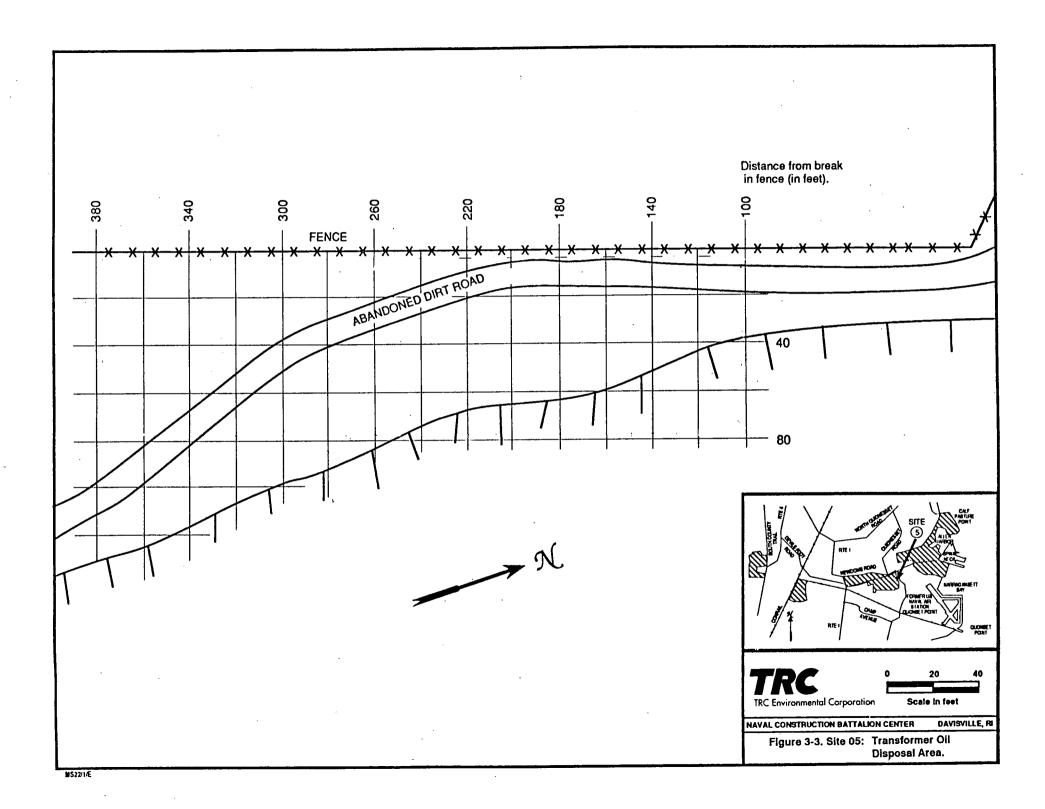


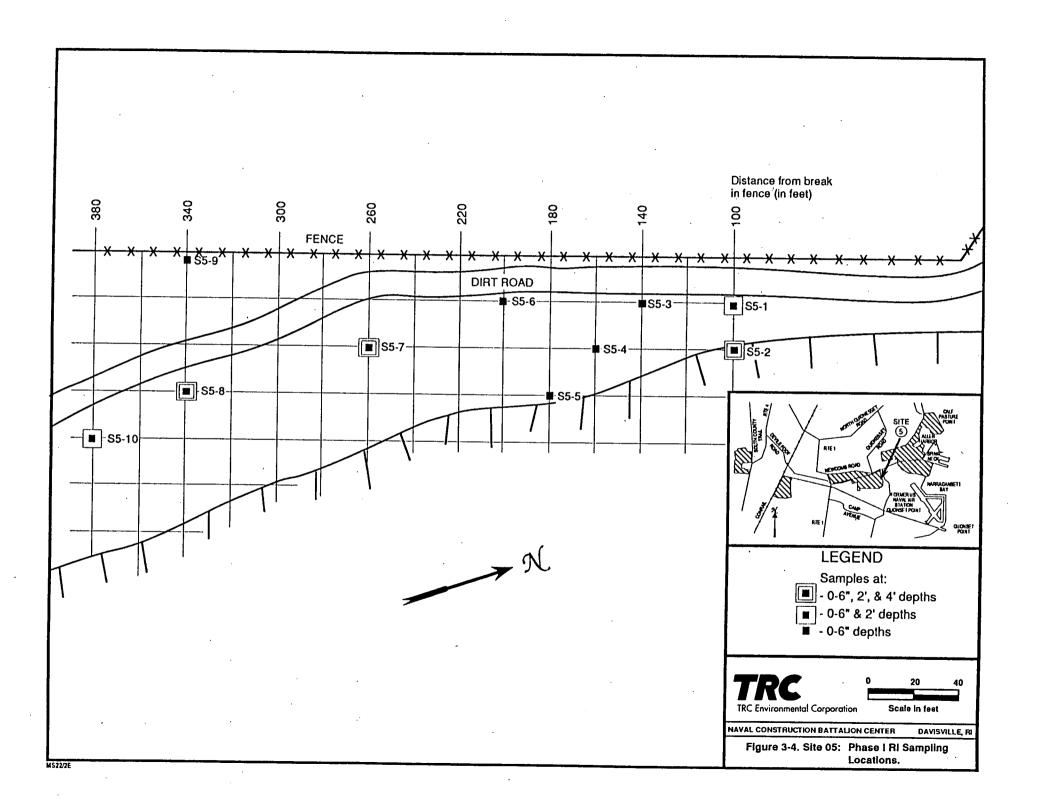


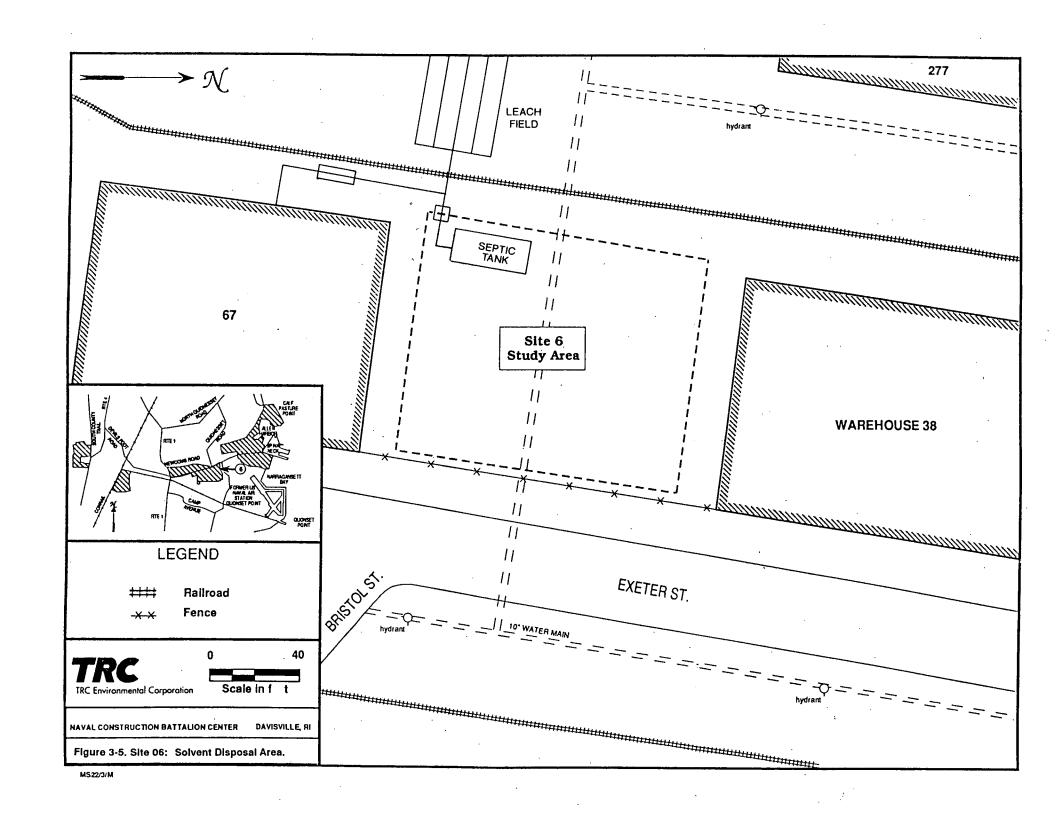


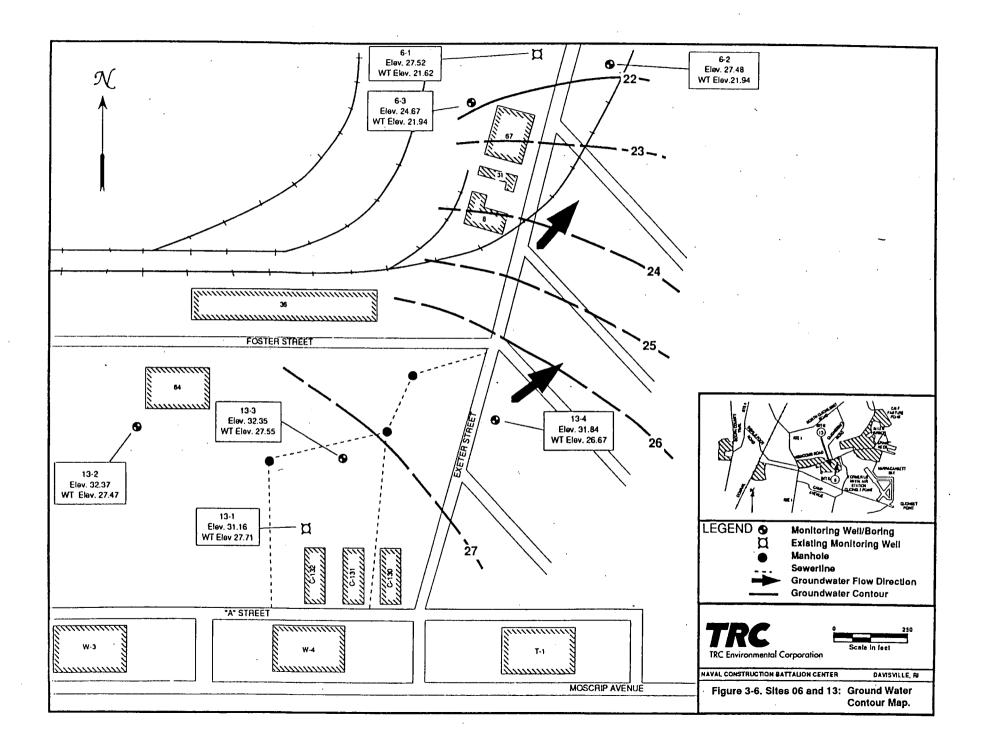


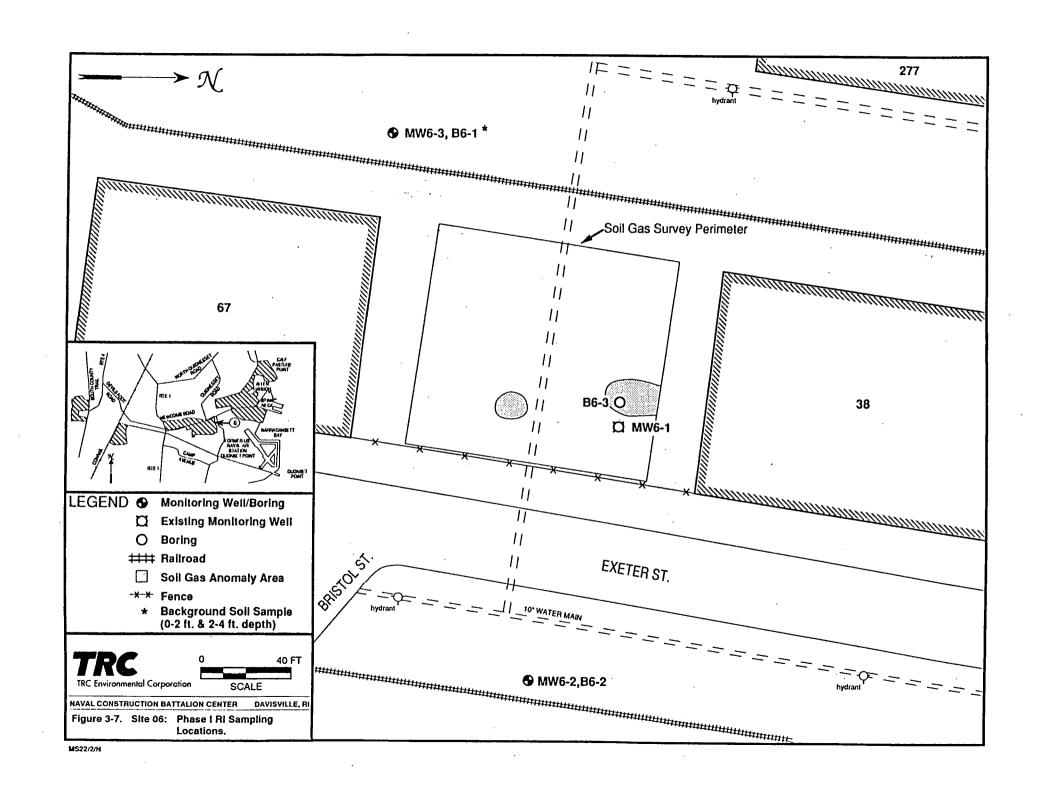


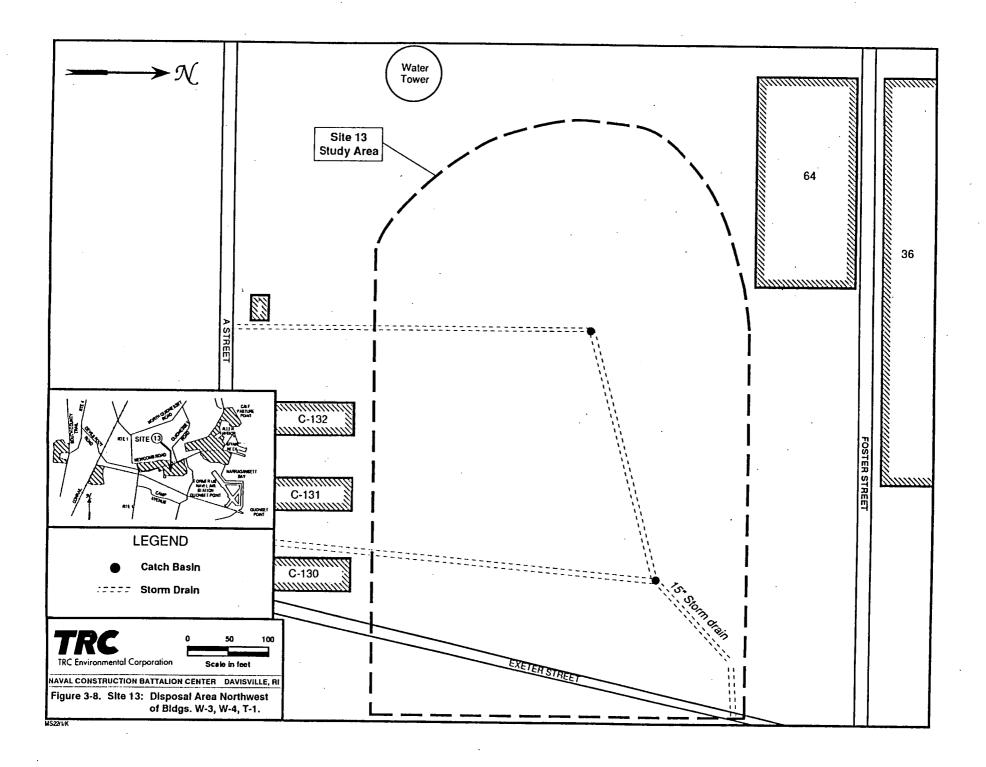


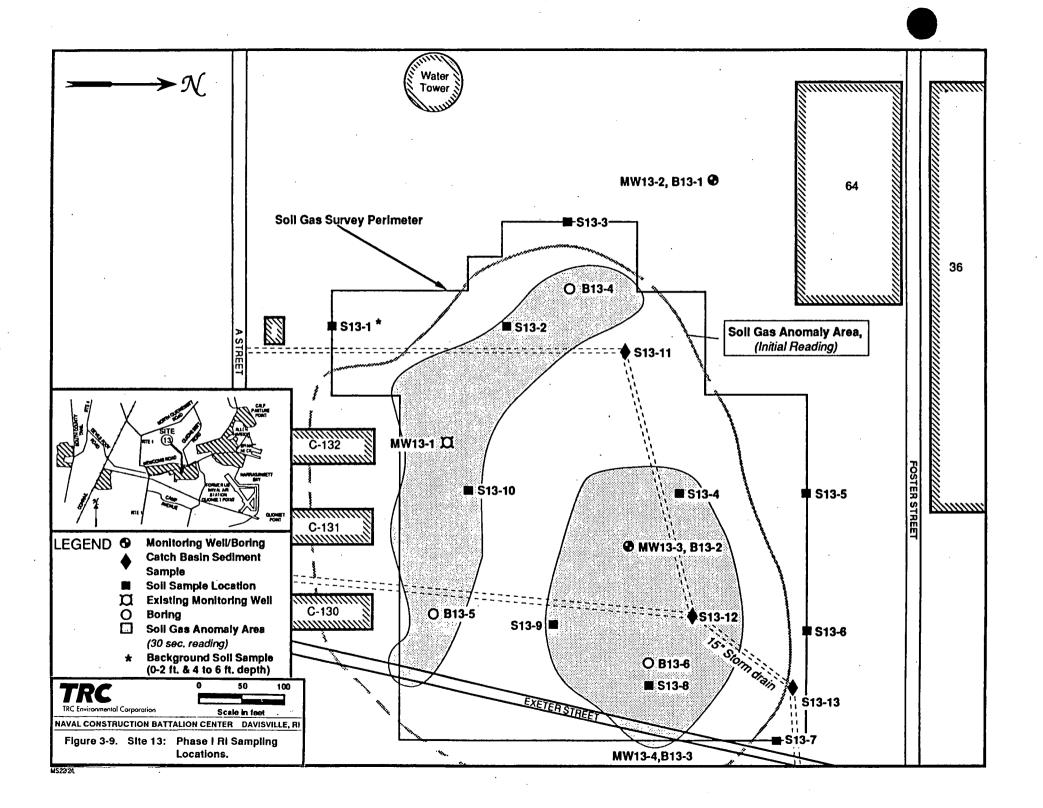


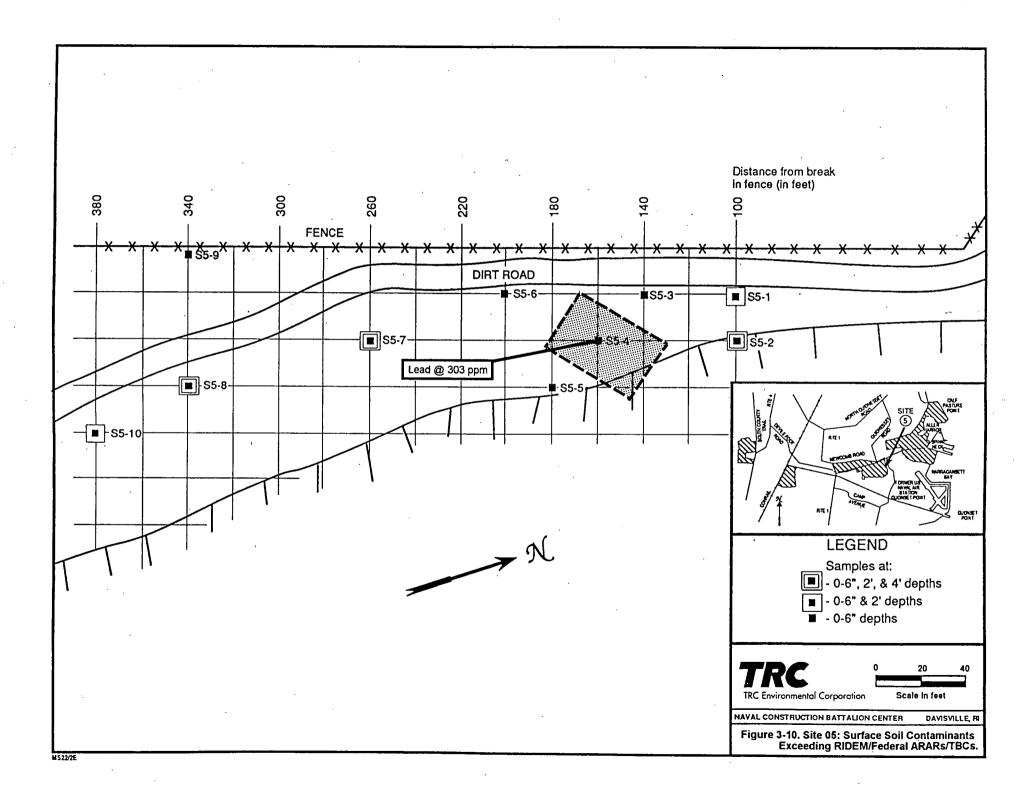


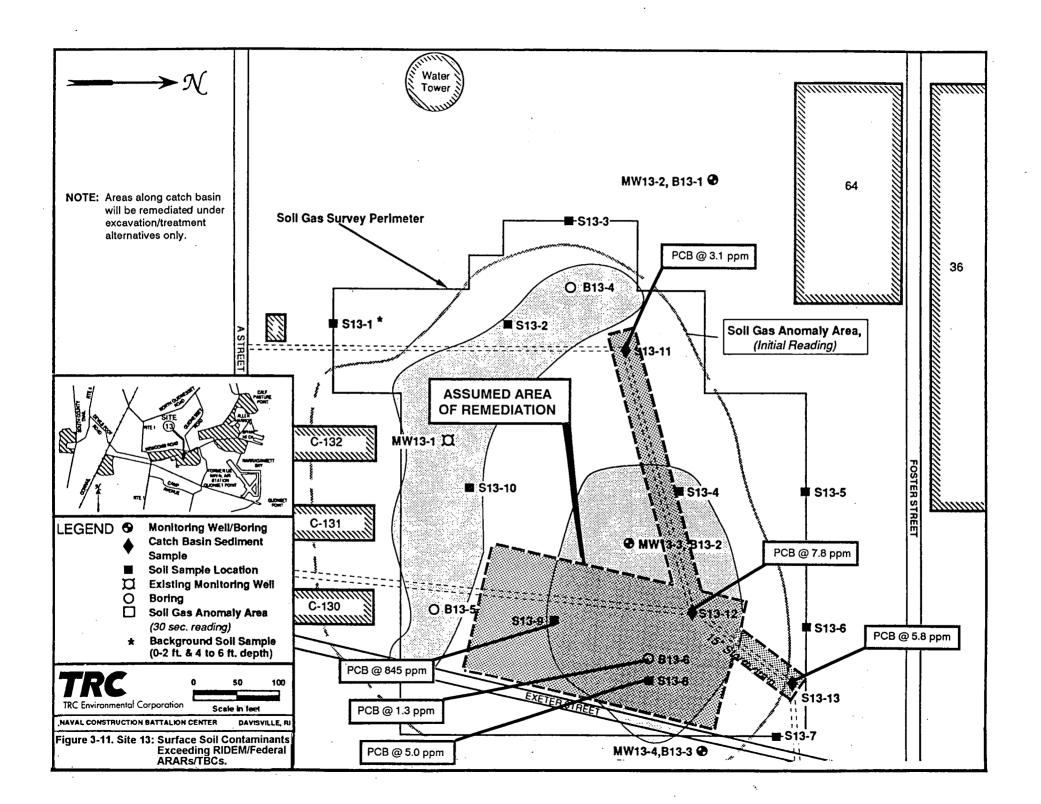


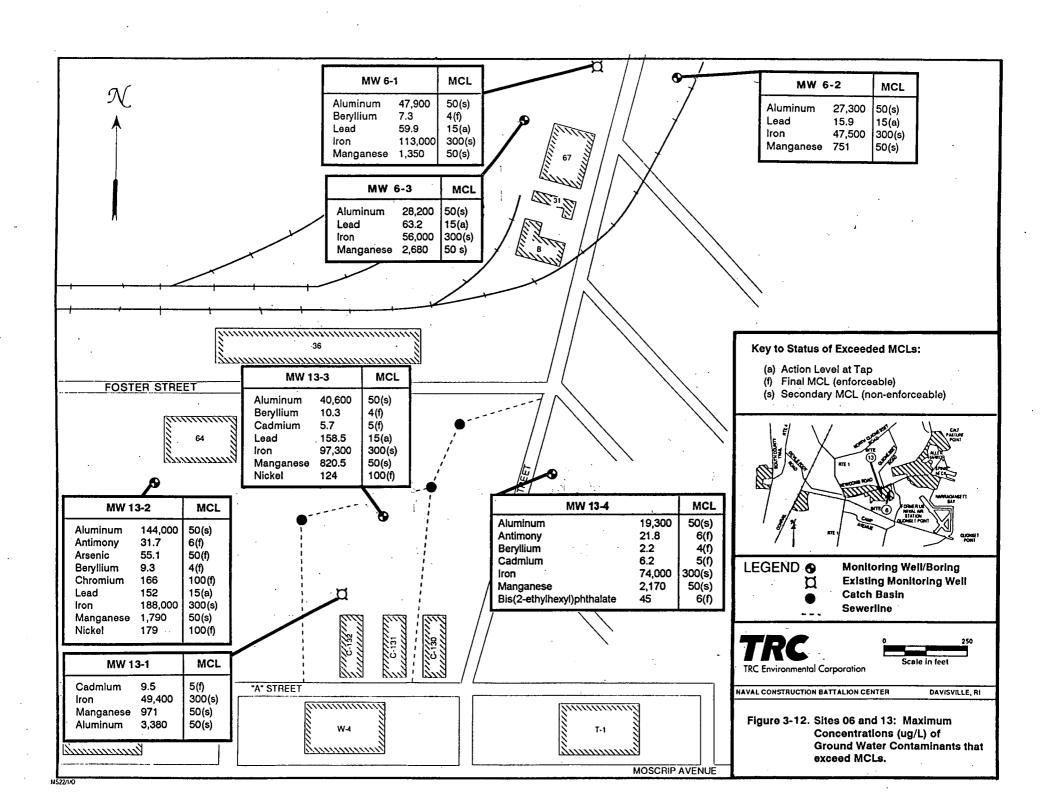


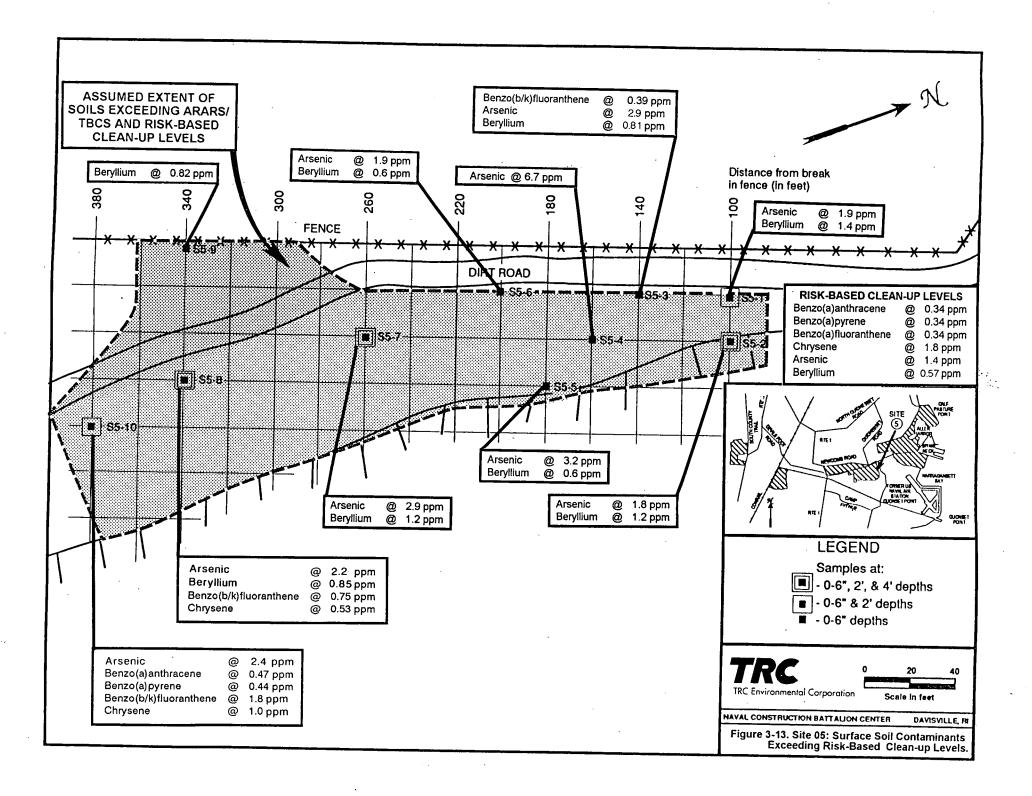


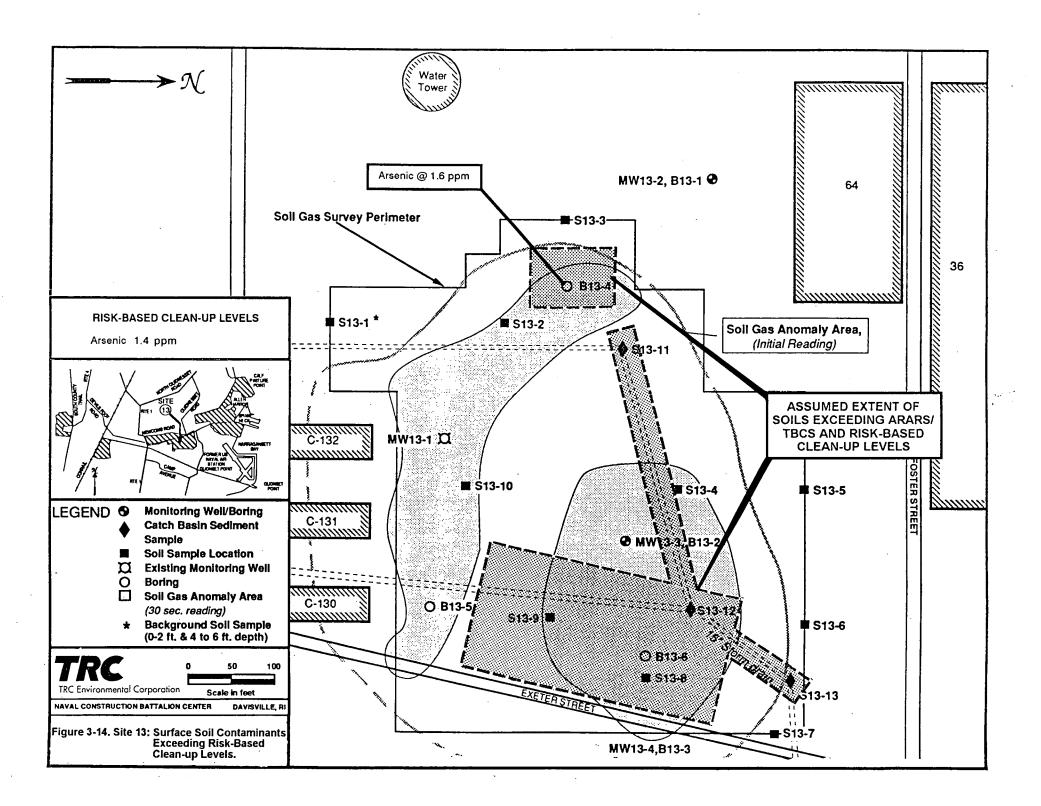


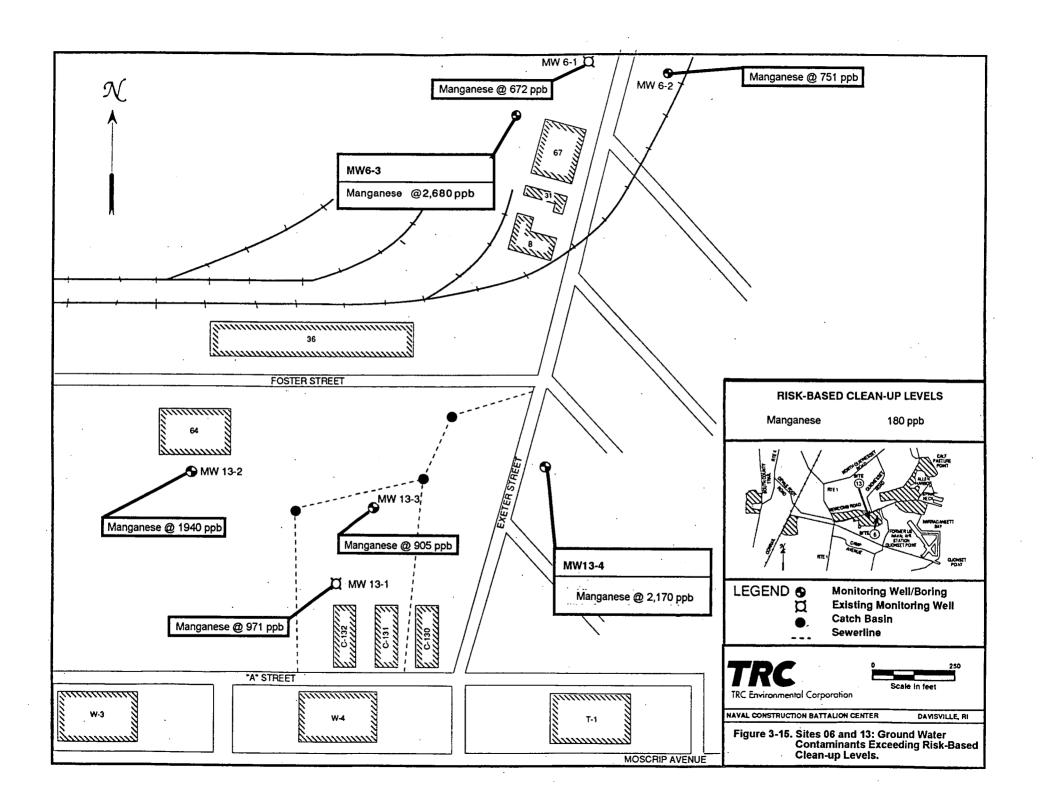


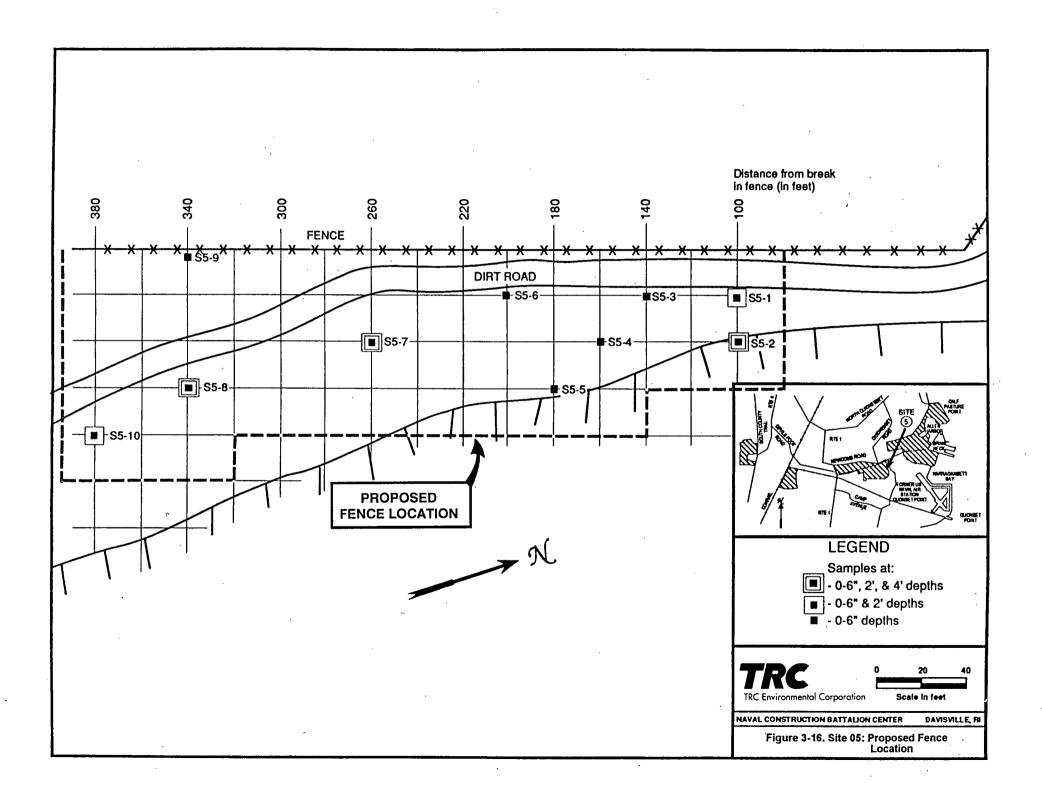


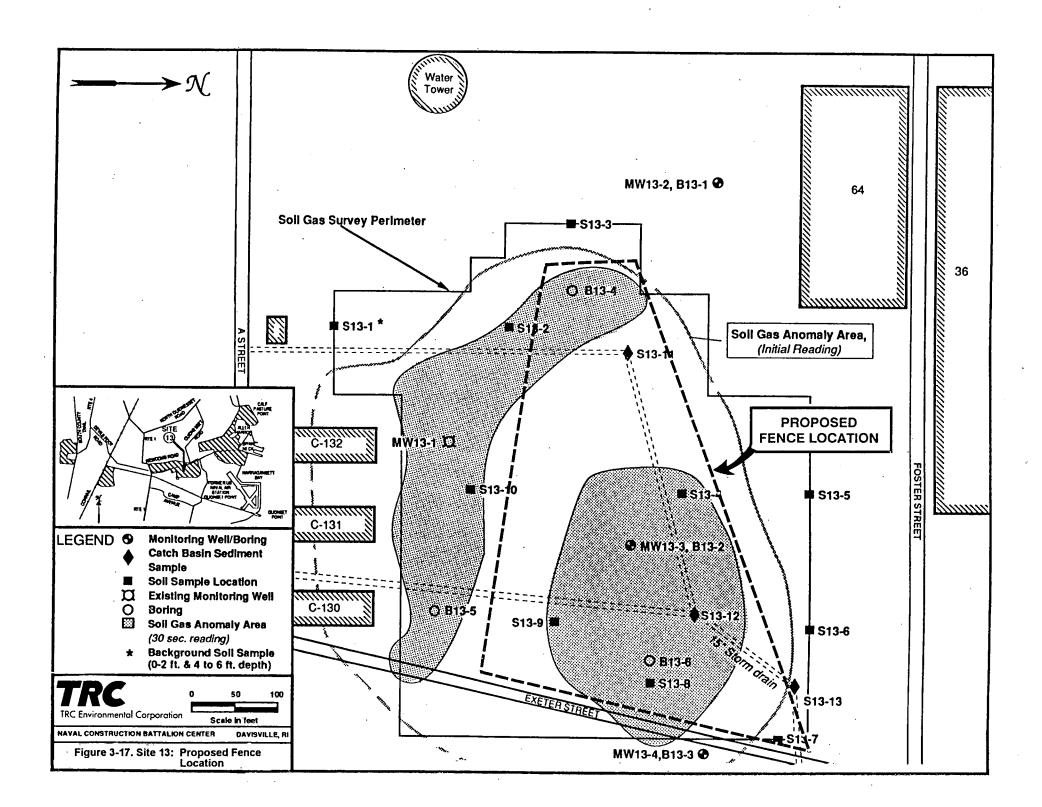


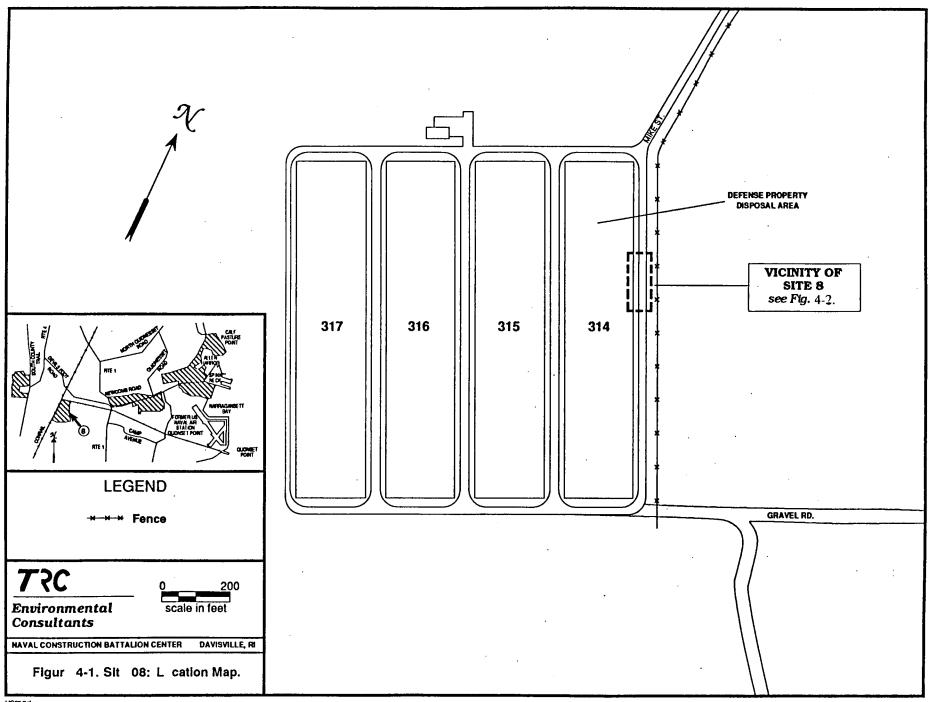


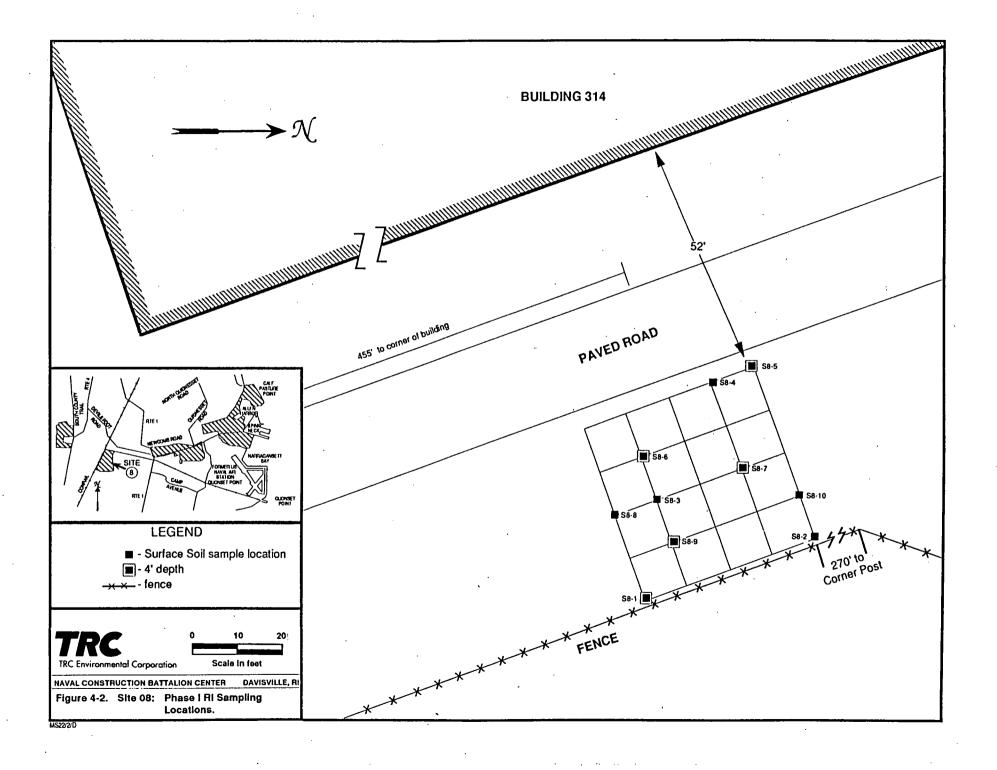


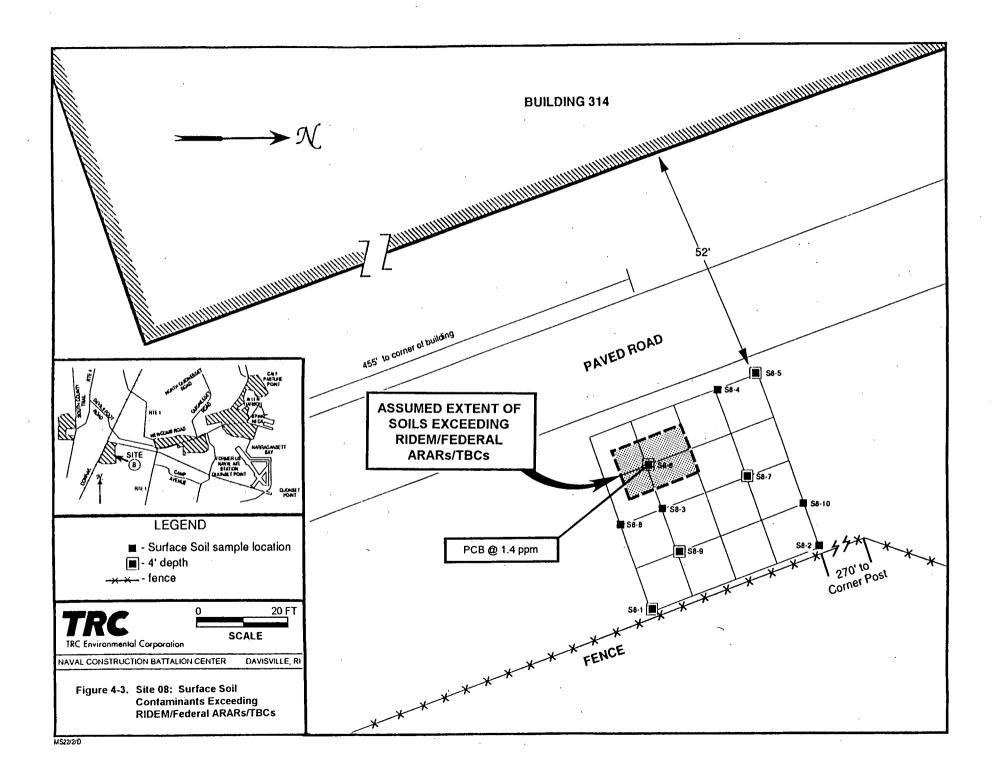


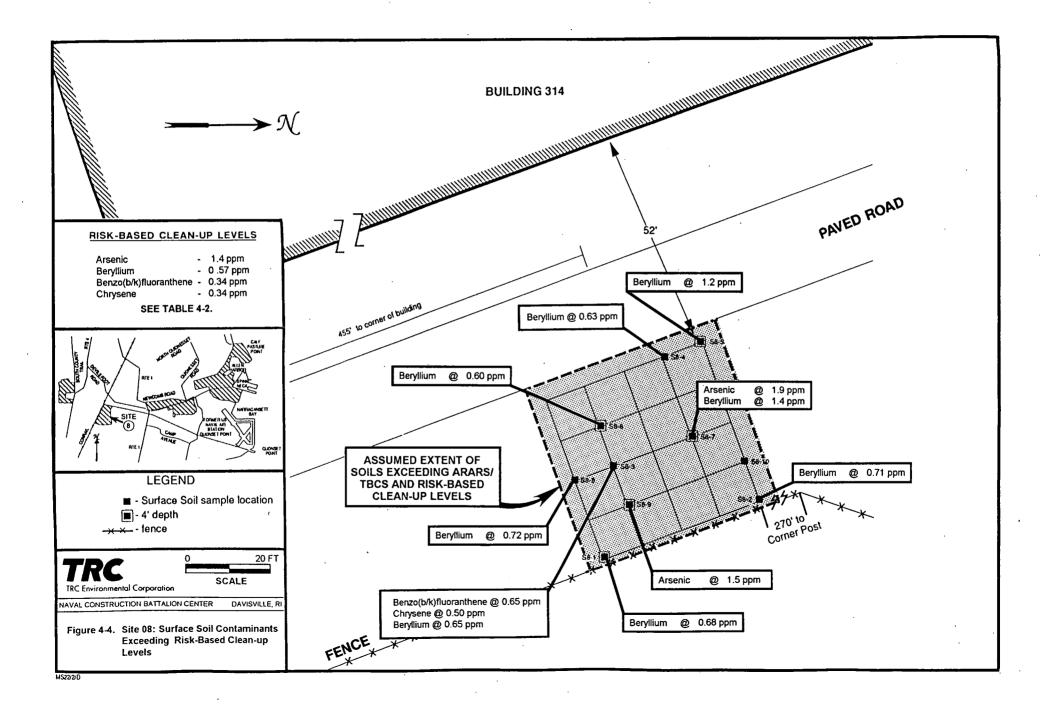


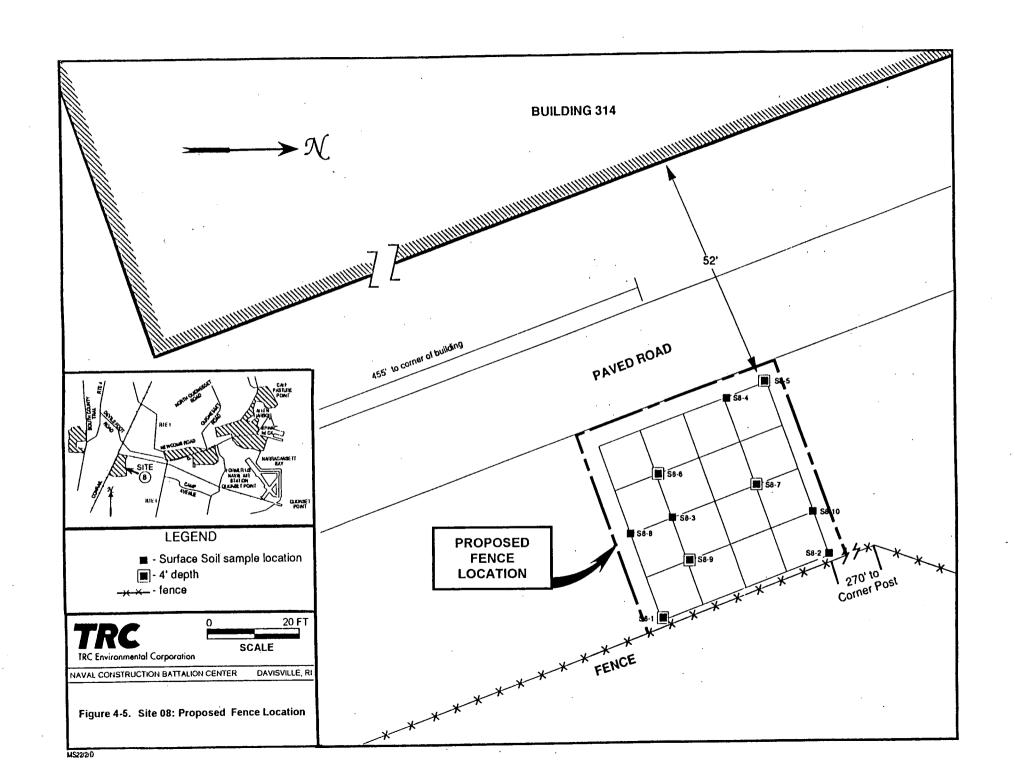


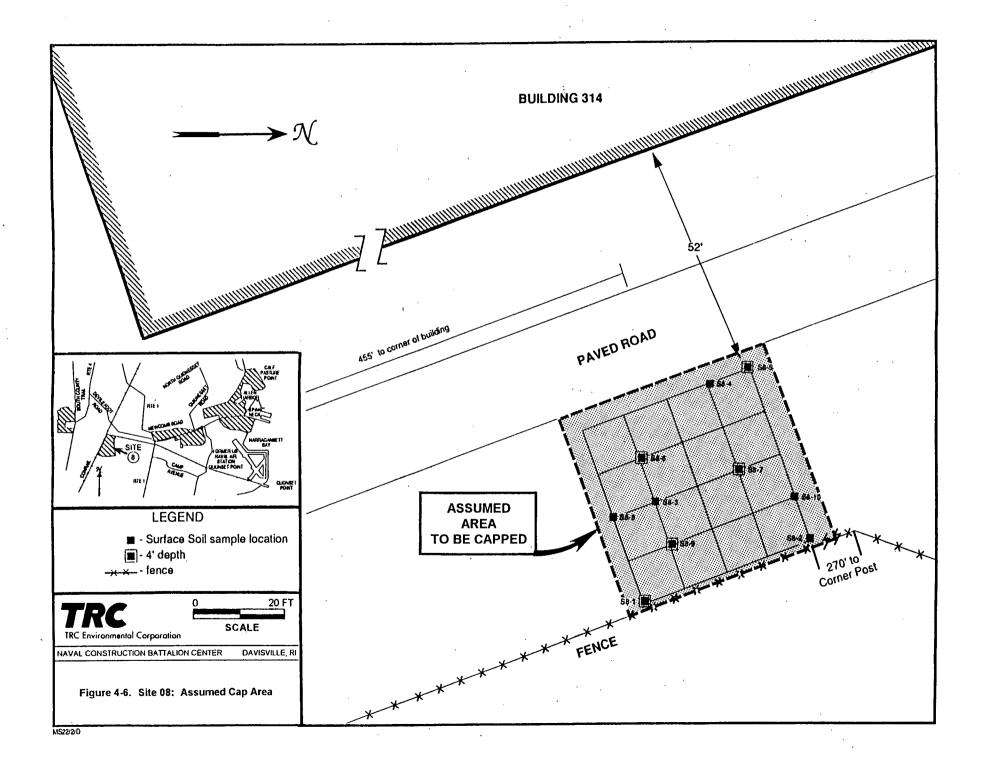


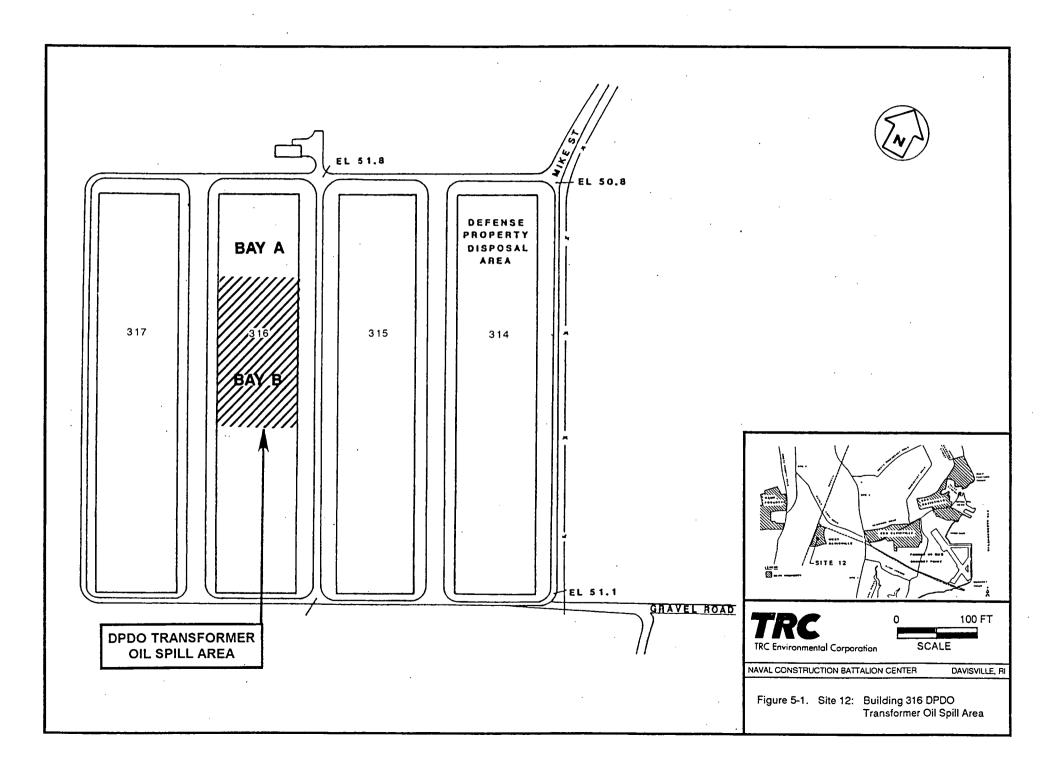


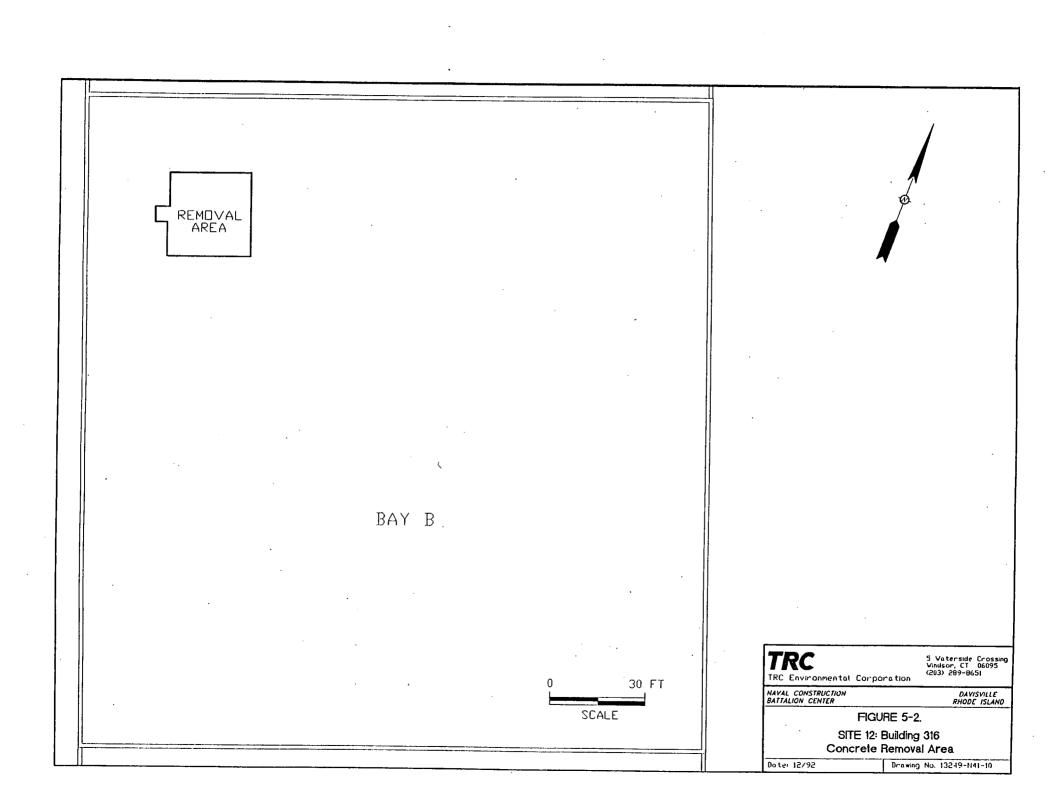


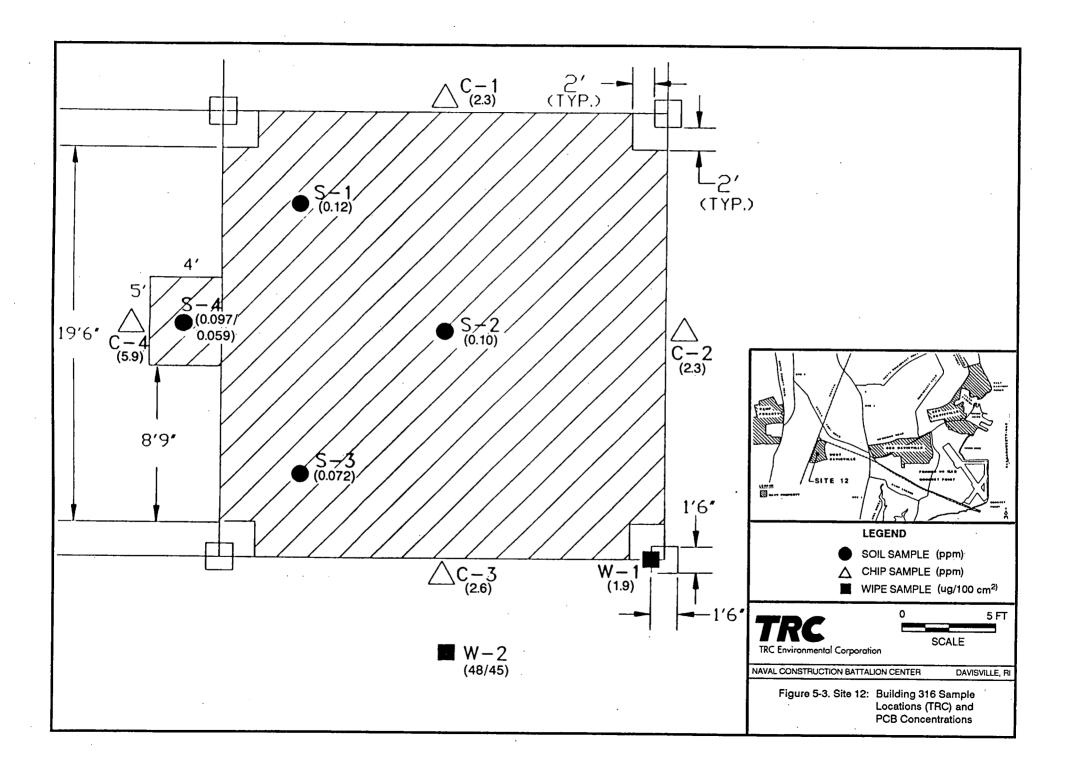


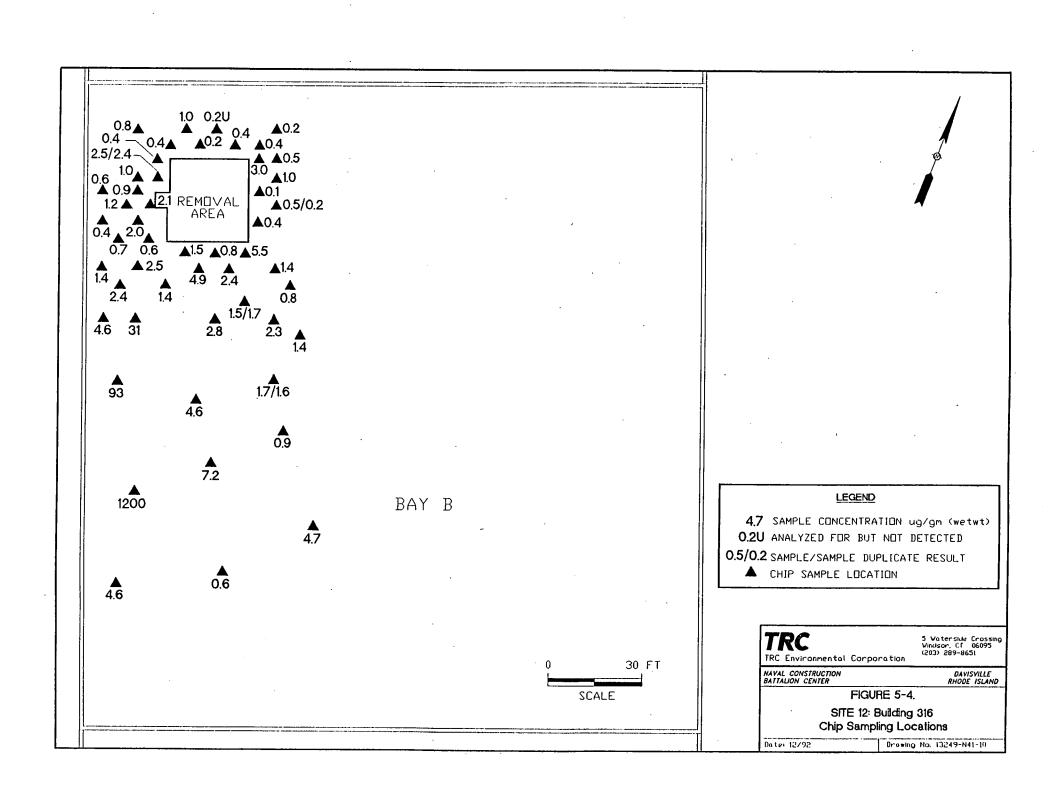


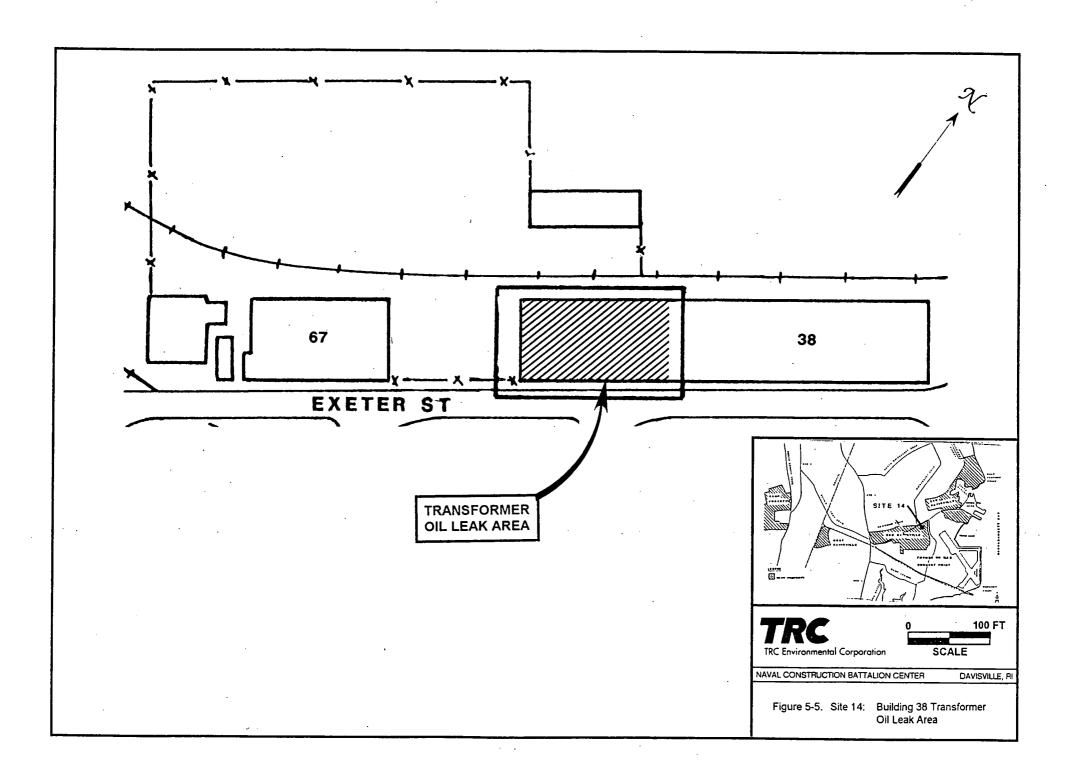


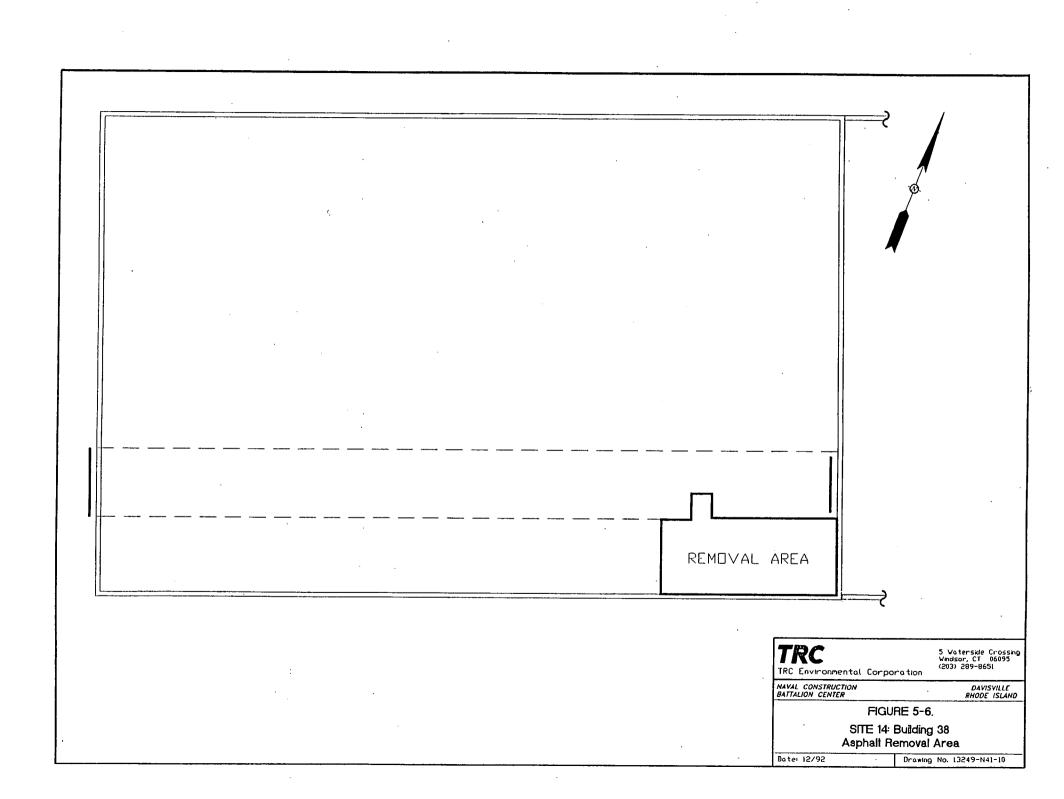


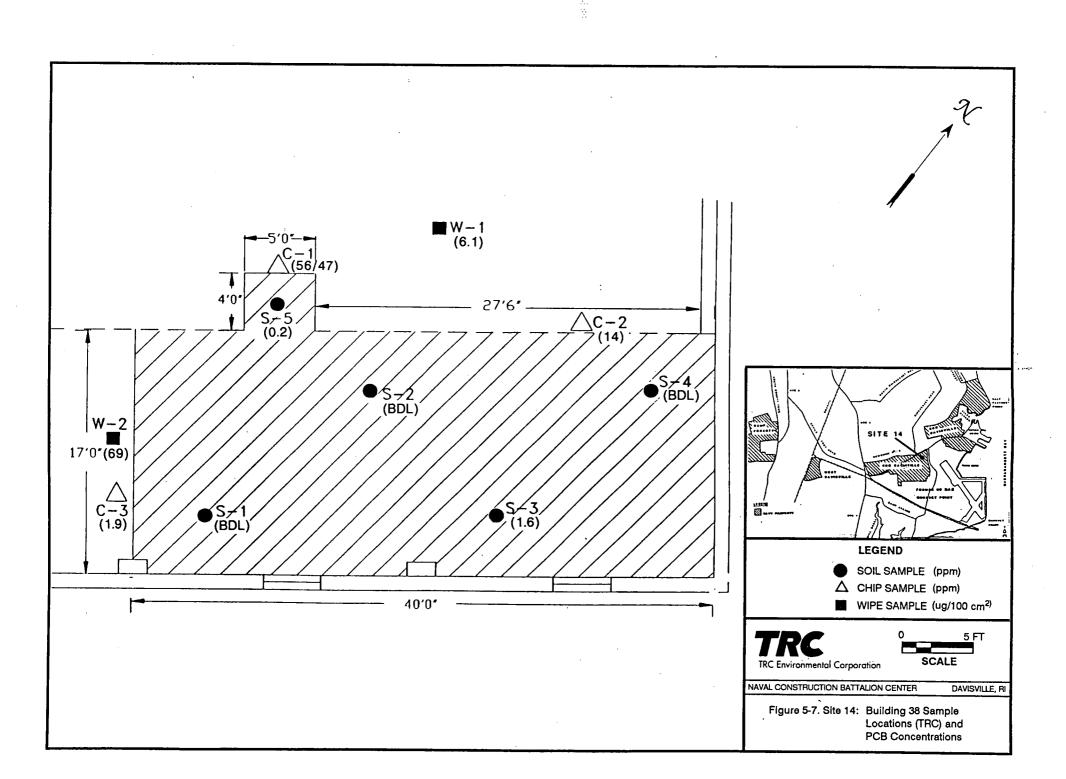


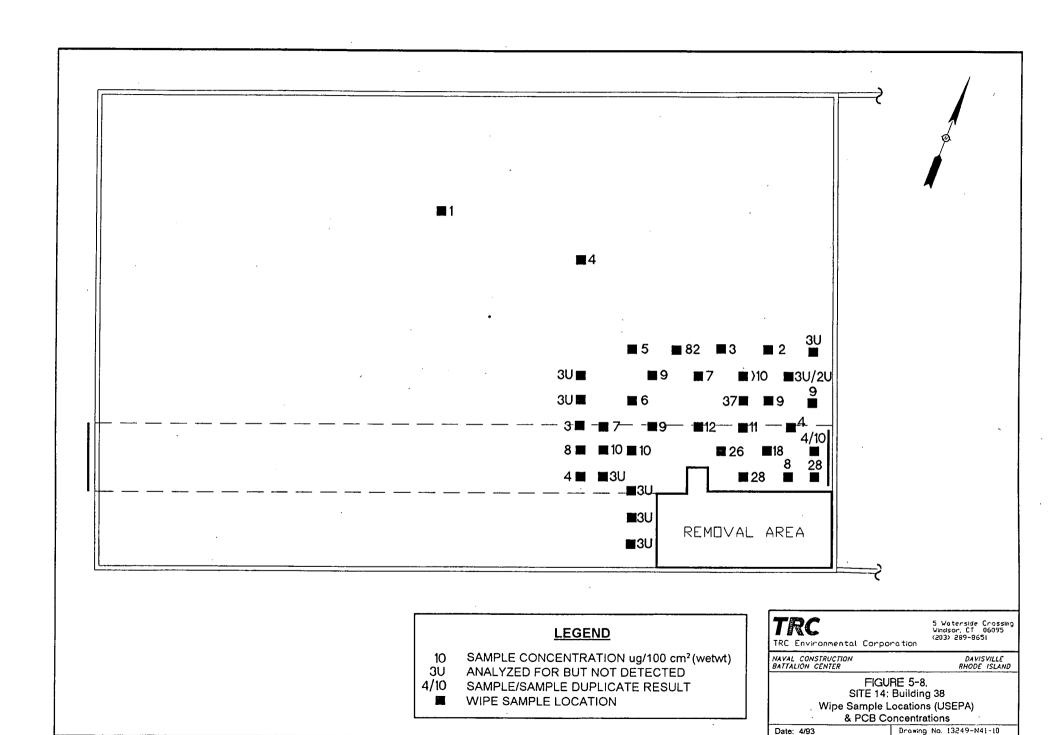


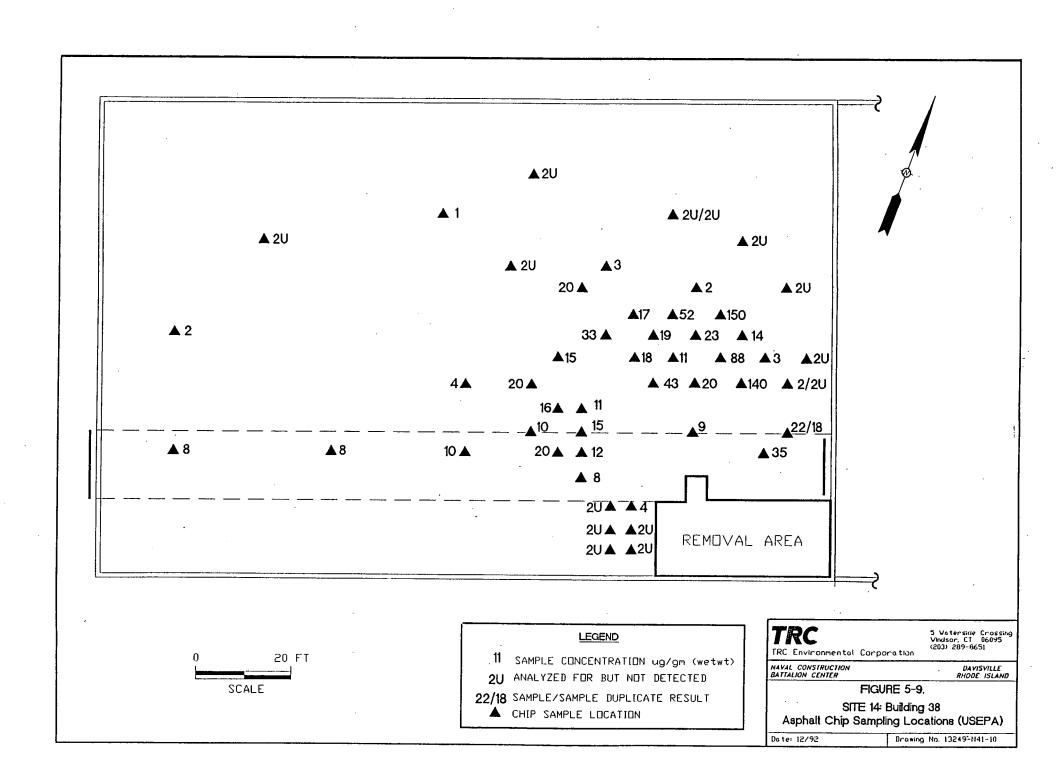


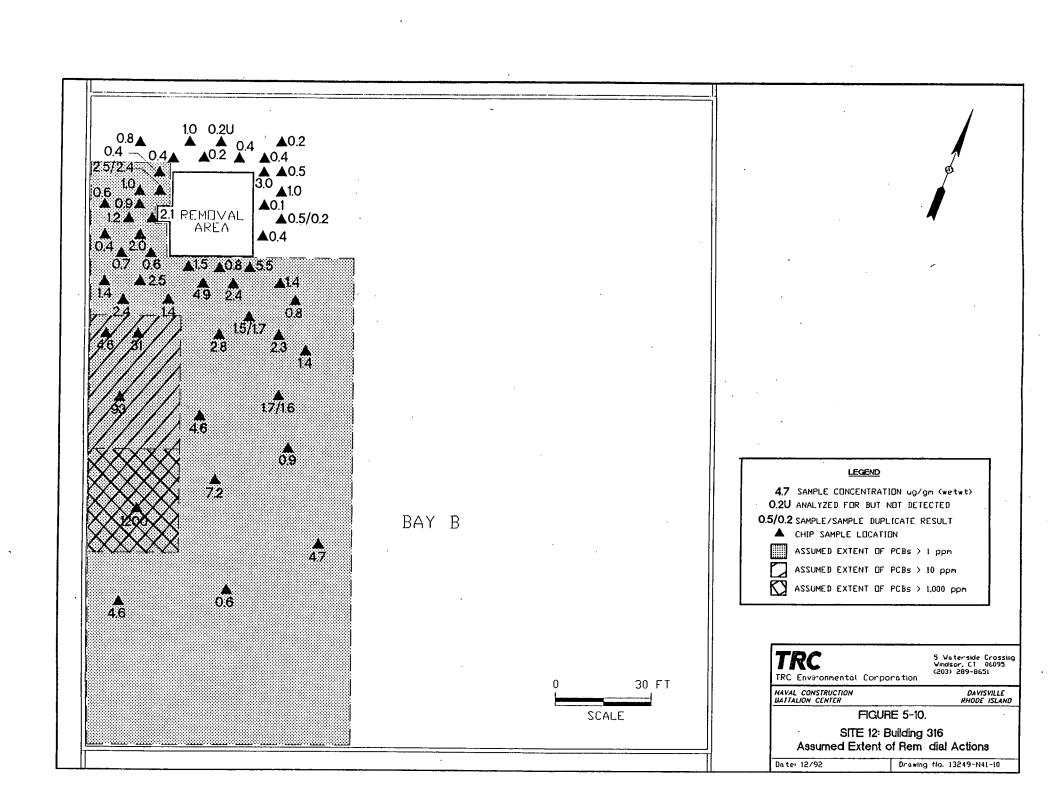


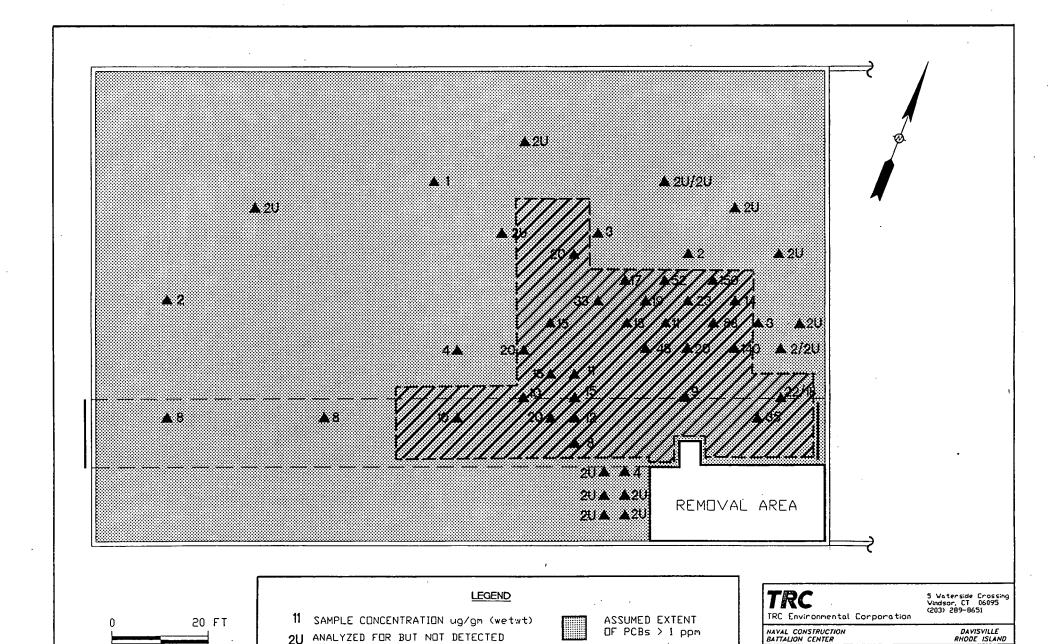












22/18 SAMPLE/SAMPLE DUPLICATE RESULT

▲ CHIP SAMPLE LOCATION

ASSUMED EXTENT OF PCBs > 10 ppm

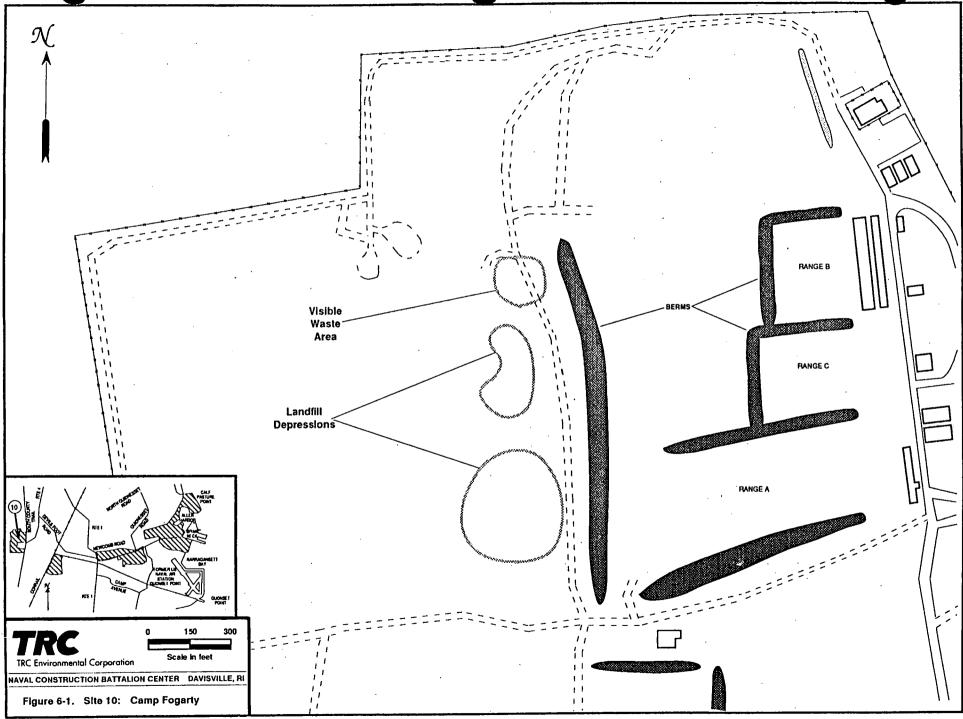
FIGURE 5-11.

SITE 14: Building 38
Assumed Extent of Remedial Actions

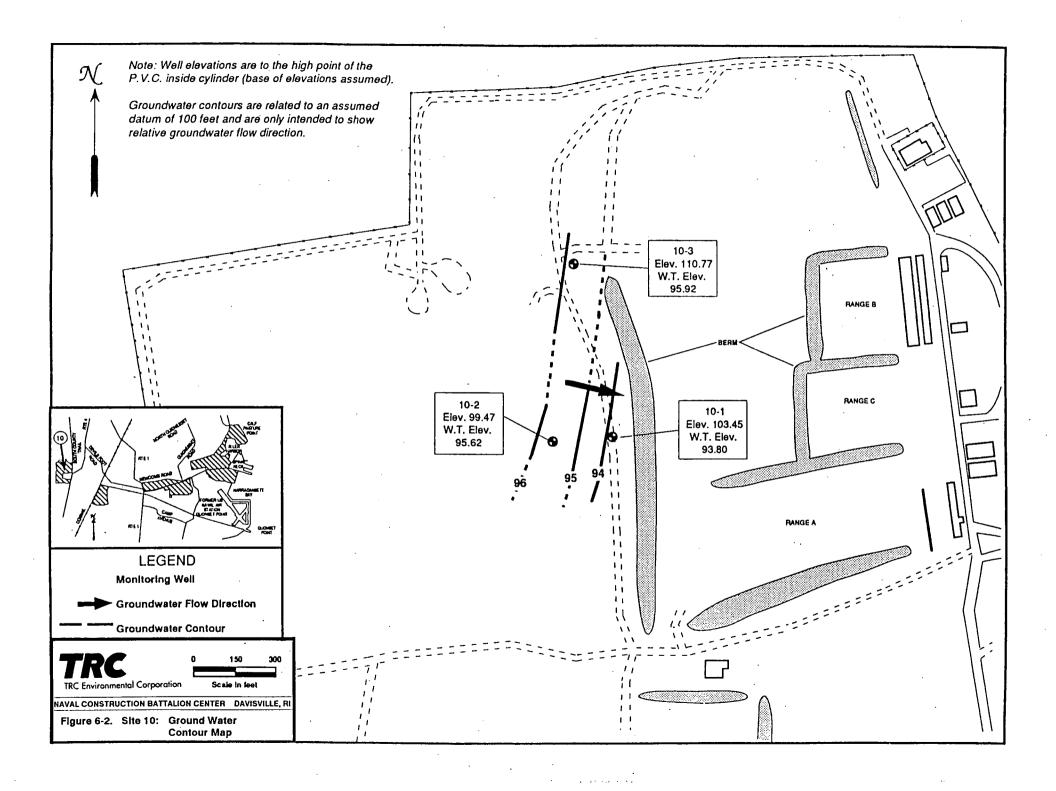
Drawing No. 13249-N41-10

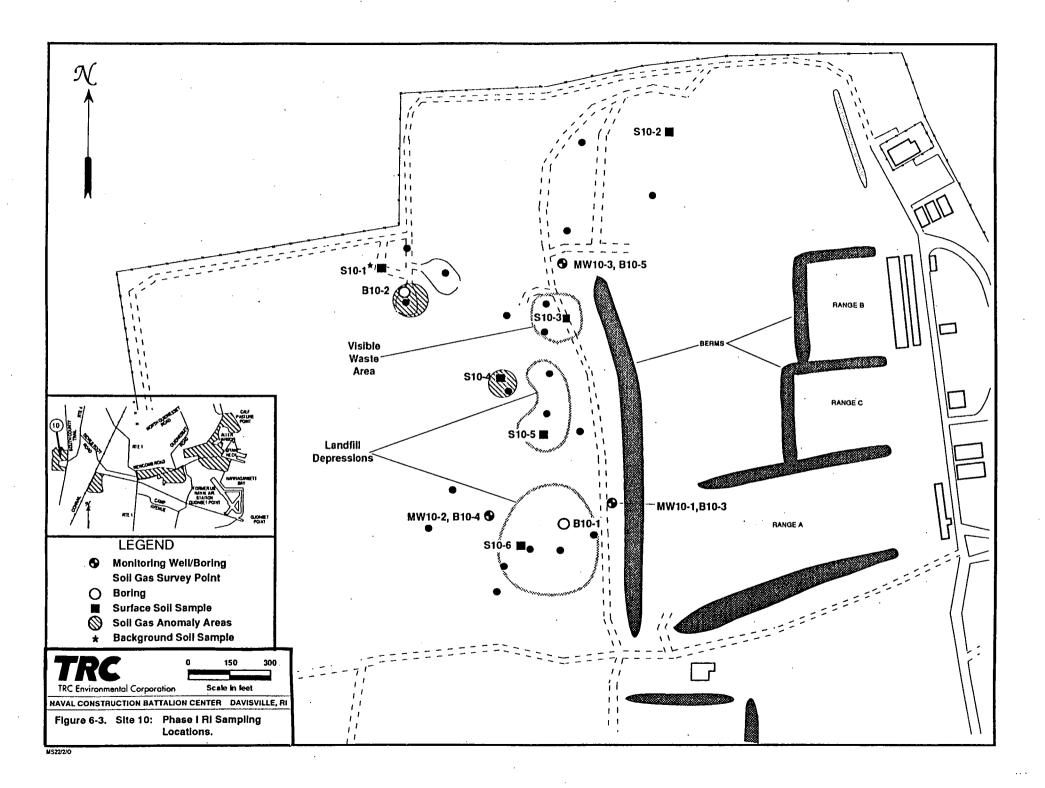
Date: 4/93

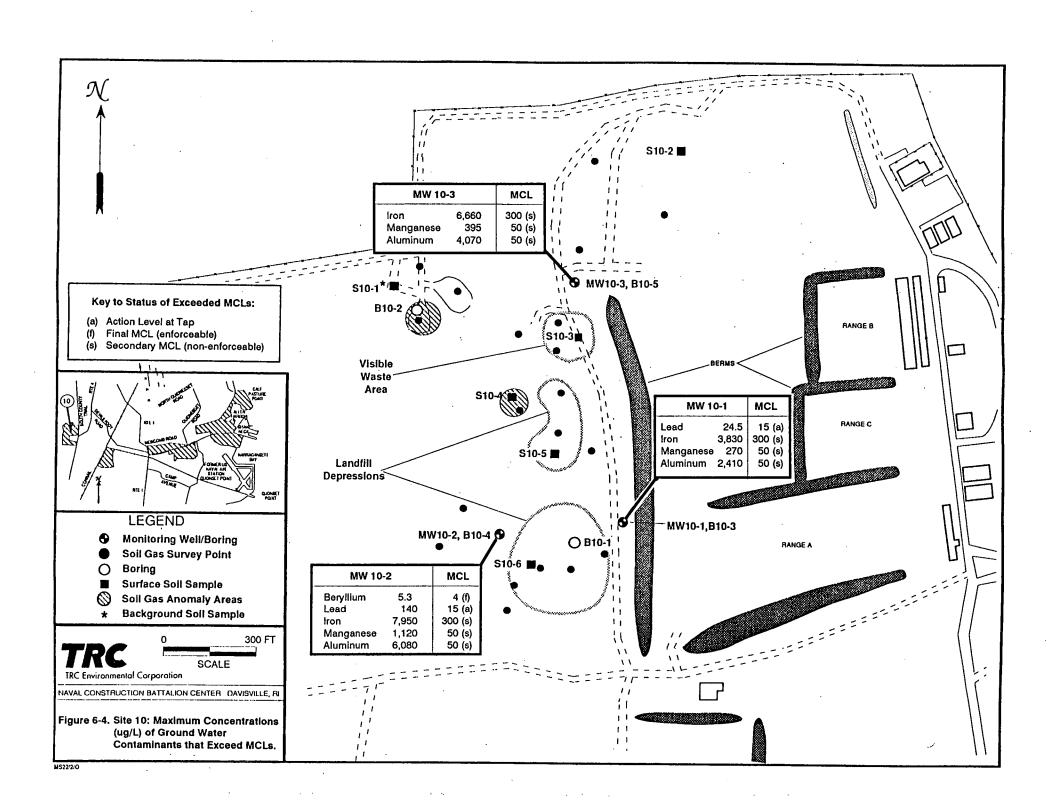
SCALE

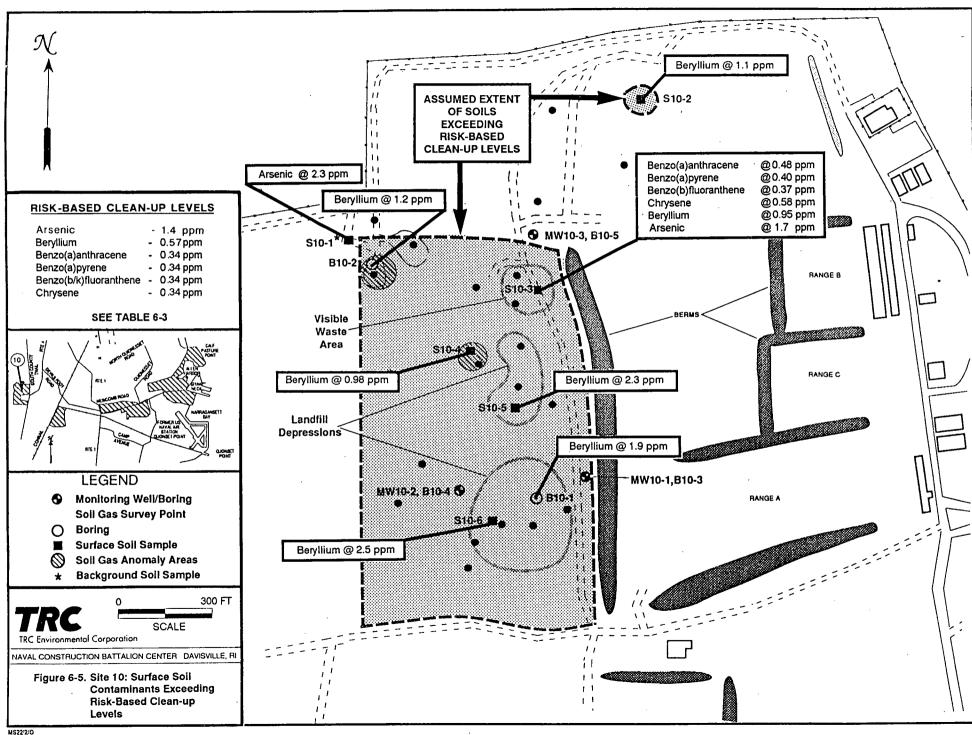


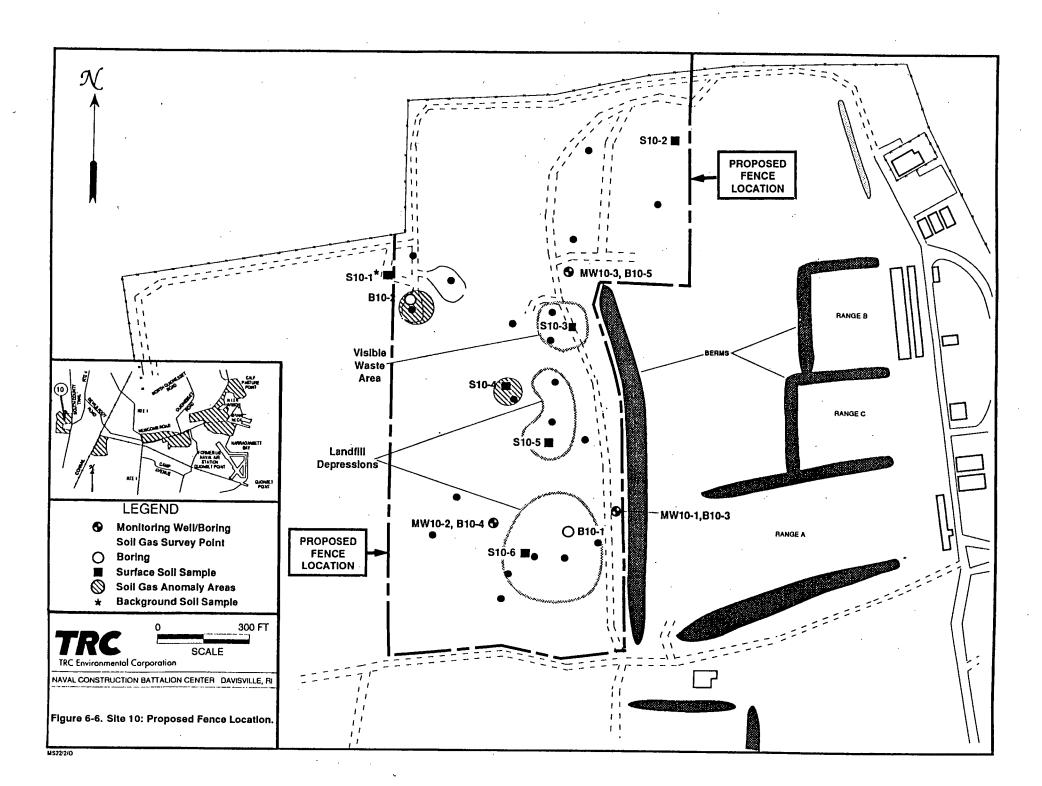
MS22/2/U

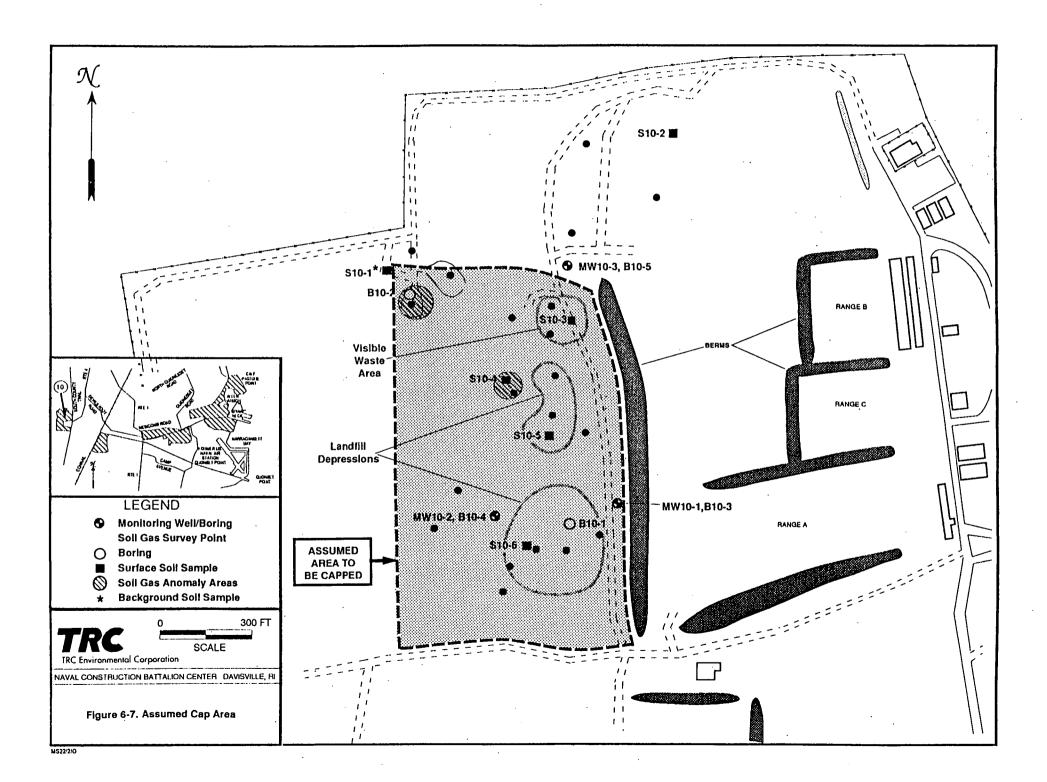


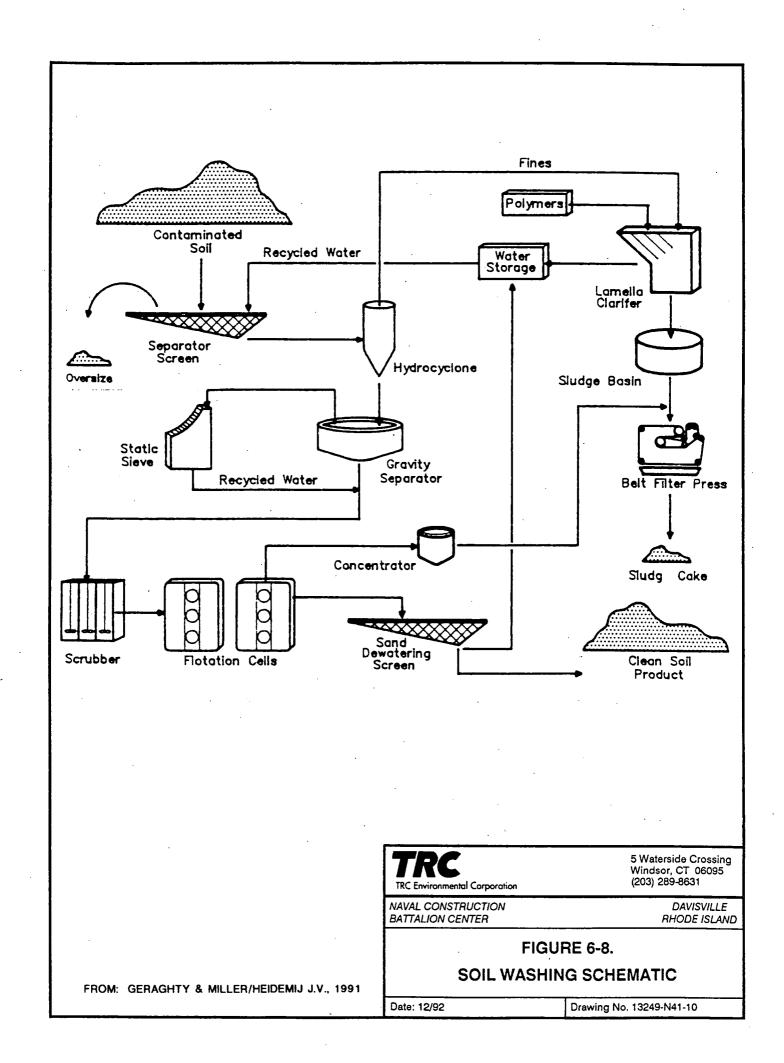


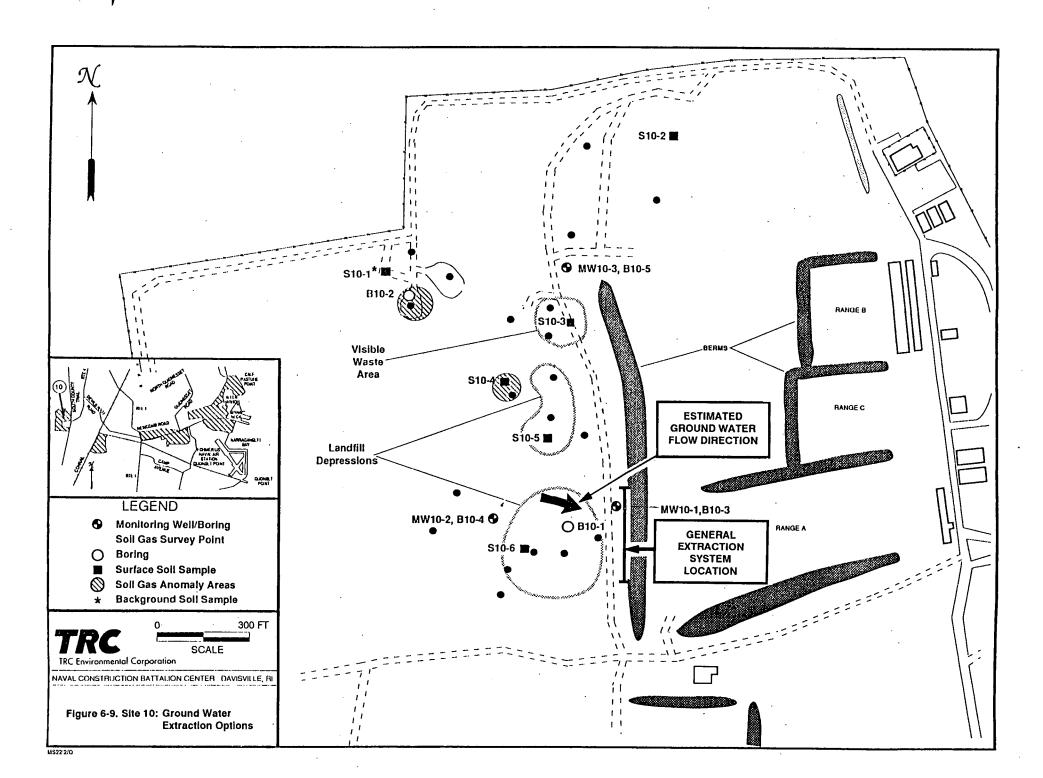


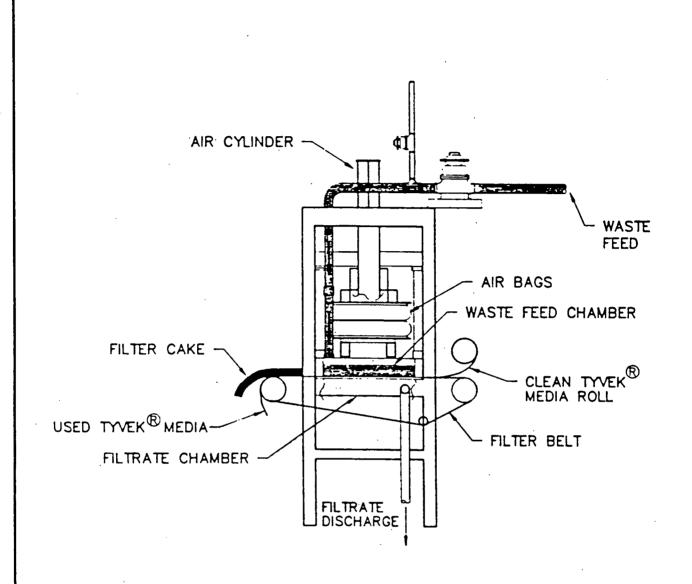












TRC

5 Waterside Crossing Windsor, CT 06095 (203) 289-8631

NAVAL CONSTRUCTION BATTALION CENTER

DAVISVILLE RHODE ISLAND

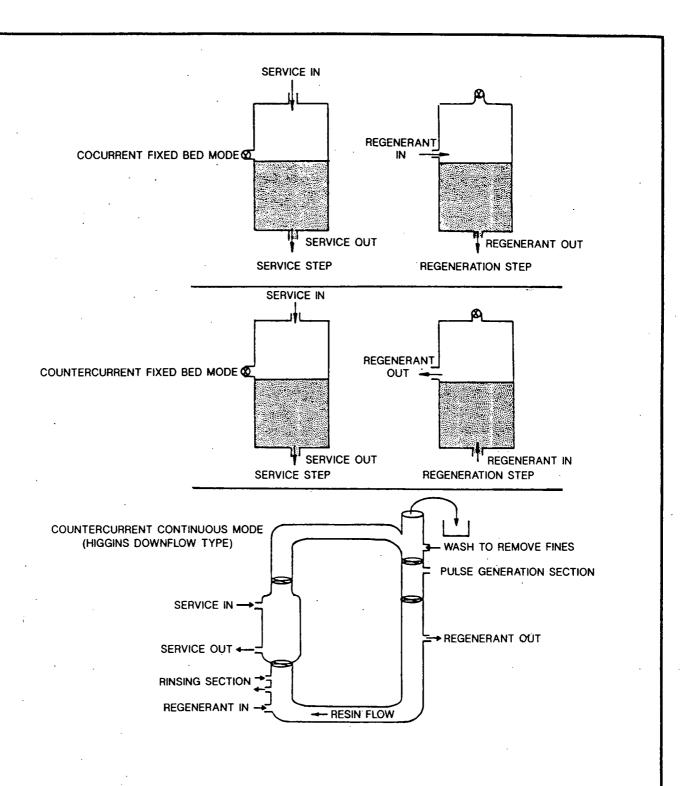
FIGURE 6-10.

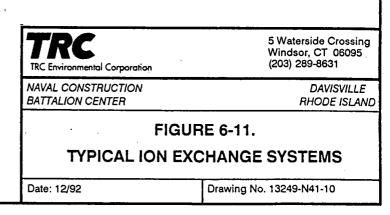
DUPONT/OBERLIN

MICROFILTRATION SYSTEM

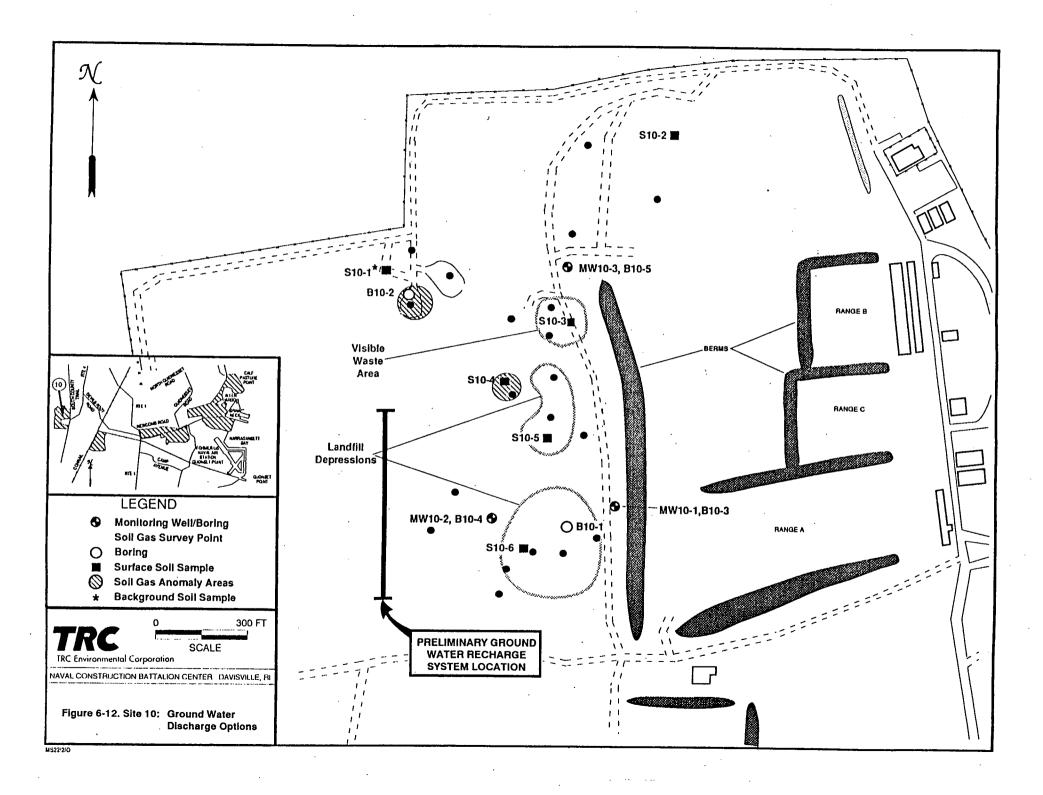
Date: 12/92

Drawing No. 13249-N41-10





SOURCE: DeRENZO, D.J., 1978



APPENDIX A

CALCULATION OF RISK-BASED CLEANUP LEVELS

CALCULATION OF RISK-BASED CLEANUP LEVELS

described in the National Contingency Plan [40 CFR As 300.43(e)(2)(i)(A)(2), "The 10^{-6} risk level shall be used as the point of departure for determining remediation goals for alternatives when ARARs are not available...". U.S. EPA Region I's exposure assessment methodology specifies the use of the "reasonable maximum exposure scenario" in estimating the risks associated with a given site. In the Phase I RI Report, the risk assessment presented risk estimates based on the maximum detected contaminant concentration (which was referred to as "worst-case"), and based on the geometric mean of contaminant levels (which was referred to as "most Since the former scenario coincides with U.S. EPA Region I's definition of the "reasonable maximum exposure scenario", the calculated risks were evaluated to determine if the 10^{-6} point of departure risk level is exceeded for any individual contaminants. A similar evaluation was also conducted to identify constituents with noncarcinogenic hazard index ratios above unity in the Phase I RI Report.

Those contaminants which contributed an individual worst-case cancer risk of greater than 1 x 10⁻⁶ to the overall cancer risk estimate, or an individual hazard index ratio of greater than one to the total hazard index ratio for noncarcinogenic risks, were then evaluated to determine if there were any for which an ARAR/TBC was not identified. For those contaminants without an associated ARAR/TBC, a risk-based cleanup level was calculated, based on a future residential use scenario. The risk-based cleanup levels were calculated based on the Risk Assessment Guidance for Superfund: Volume 1, Human Health Evaluation Manual (Part B), December 1991. The calculations incorporate residential exposure as a child (ages 1 to 6 years) and exposure

as a youth/adult (ages 7 to 30 years). If available, exposure parameters are taken directly from the risk assessment portion of the Phase I Remedial Investigation Report (TRC, 1991). Otherwise, standard default parameters are used (e.g., a youth/adult inhalation rate of 15 m³/day). The inhalation rate for children aged 1 to 6 years is derived from the Exposure Factors Handbook (U.S. EPA, 1990) and assumes 10 hours at rest, 12 hours of light activity, and 2 hours of moderate activity. Based on comments received on the Phase I risk assessment, the total exposure duration is changed from 70 to 30 years (6 years as a child, 24 years as an adult). Similarly, the body weight for a child aged 1 to 6 years has been changed from 16 to 15 kilograms. RfD data were also updated, as appropriate.

Table 1
Residential Surface Soil
Cancer—Based Calculations

		Cancer				Surface Soil	
·	Target	Averaging	Exposure	Ingestion	Slope	Cleanup	Delevent
Chemical	Risk (TR) ()	Time (AT) (days)	Frequency (EF) (days/yr)	Factor (IF) (mg-yr/kg-day)	Factor (SF) (mg/kd*d) ⁻¹	Level (b) (mg/kg)	Relevant Sites
Benzo(a)anthracene (a)	1.0E-06	25550	91	114	7.3	3.4E-01	5,6,8,10
Benzo(a)pyrene (a)	1.0E-06	25550	91	114	7.3	3.4E-01	5,6,8,10
Benzo(b/k)fluoranthene (a)	1.0E-06	25550	91	114	7.3	3.4E-01	5,6,8,10
Chrysene (a)	1.0E-06	25550	91	114	7.3	3.4E-01	5,6,8,10
Dibenzo(a,h)anthracene (a)	1.0E-06	25550	91	114	7.3	3.4E-01	8,10
Indeno(1,2,3-cd)pyrene (a)	1.0E-06	25550	91	114	7.3	3.4E-01	5,8,10
Arsenic	1,0E-06	25550	91	114	1.75	1.4E+00 (c)	5,8,10,13
Beryllium	1.0E-06	25550	91	114	4.3	5.7E-01 (d)	5,8,10

- (a) Carcinogenic PAHs
- (b) Based on USEPA (1991) guidance; exposure parameters taken from Phase I Human Health Risk Assessment
- (c) Cleanup level is less than the geometric mean of 4.8 mg/kg for background soils in eastern U.S. (USGS, 1984)
- (d) Cleanup level is less than the geometric mean of 0.55 mg/kg for background soils in eastern U.S. (USGS, 1984)

Soil cleanup level = [TR * AT] / [SF * CF * EF * IF]

Where:

CF = Conversion factor (kg/mg)

1.0E-06 (--)

EF = age - adjusted exposure frequency:

91 days/yr where:

143 days/yr (age 1-6)

78 days/yr (age 7-30)

$$\mathsf{IF} = [\mathsf{IR}_{\mathsf{soil/age1-6}} \star (\mathsf{ED}_{\mathsf{age1-6}} / \mathsf{BW}_{\mathsf{age1-6}})] + [\mathsf{IR}_{\mathsf{soil/age7-30}} \star (\mathsf{ED}_{\mathsf{age7-30}} / \mathsf{BW}_{\mathsf{age7-30}})]$$

IR = soil ingestion rates:

200 mg/day (age 1-6)

100 mg/day (age 7-30)

ED = exposure durations:

6 yr (age 1-6)

24 yr (age 7-30)

BW = body weights:

15 kg (age 1-6)

70 kg (age 7-30)

Table 1 (cont.) Residential Surface Soil Noncancer—Based Calculations

	Target Noncancer						
	Hazard Index (THI)	Averaging Time (AT)	Exposure Frequency (EF)	Ingestion Factor (IF)	Reference Dose (Rfd)	Cleanup Level (a)	Relevant
Chemical	()	(days)	(days/yr)	(mg-yr/kg-day)	(mg/kd*d)	(mg/kg)	Sites
Arsenic	1.0E+00	10950	91	114	0.001	1.1E+03	13

(a) Based on USEPA (1991) guidance; exposure parameters taken from Phase I Human Health Risk Assessment

Soil cleanup level = [THI * AT] / [1/Rfd * CF * EF * IF]

Where:

CF = Conversion factor (kg/mg)

1.0E-06 (--)

EF = age-adjusted exposure frequency:

91 days/yr where:

143 days/yr (age 1-6)

78 days/yr (age 7-30)

 $\mathsf{IF} = [\mathsf{IR}_{\mathsf{soil/age1-6}} * (\mathsf{ED}_{\mathsf{age1-6}} / \mathsf{BW}_{\mathsf{age1-6}})] + [\mathsf{IR}_{\mathsf{soil/age7-30}} * (\mathsf{ED}_{\mathsf{age7-30}} / \mathsf{BW}_{\mathsf{age7-30}})]$

IR = soil ingestion rates:

200 mg/day (age 1-6)

100 mg/day (age 7-30)

ED = exposure durations:

6 yr (age 1-6)

24 yr (age 7-30)

BW = body weights:

15 kg (age 1-6)

70 kg (age 7-30)

Table 2
Residential Ground Water
Noncancer—Based Calculations

Chemical		Noncancer Averaging Time (AT) (days)	Exposure Frequency (EF) (days/yr)	Oral Reference Dose (RfDo) (mg/kd*d)	Ground Water Cleanup Level (a) (mg/l)	Relevant Sites
Manganese	1.0E+00	10950	365	5.0E-03 (b)	1.8E-01	6,13

(a) Based on USEPA (1991) guidance; exposure parameters taken from Phase I Human Health Risk Assessment

(b) RfD for ingestion of water; RfD of 1.4E-1 mg/kg-day available for food ingestion

Ground water cleanup level* = [TR * AT * BW] / [EF * ED * (1/RfDo * IRw)]

Where:

ED = exposure duration:

30 yr

BW = body weight:

70 kg

EF = exposure frequency:

365 days/yr

IRw = water ingestion rate:

2 I/day

^{*} The volatilization of manganese is expected to be negligible, therefore inhalation not included in calculation.

APPENDIX B

TECHNOLOGY AND PROCESS OPTION SCREENING

INTRODUCTION TO TECHNOLOGY AND PROCESS OPTION SCREENING AND REMEDIAL ALTERNATIVE DEVELOPMENT

Based on the general response actions developed for the sites addressed within this Initial Screening of Alternatives Report, remedial technologies which could potentially meet the remedial action objectives and cleanup criteria are identified and screened. This process is a two-step process in which technologies are initially screened on the basis of technical implementability. For the technologies which pass the initial screening, the process options associated with each technology are screened based on effectiveness, implementability and cost. Representative process options are then chosen based on this screening for inclusion in the comprehensive remedial alternatives developed for the sites.

Technology Screening

The intent of the technology screening is to reduce the universe of potentially applicable technology types and process options based on technical implementability. Two factors which may be considered in the evaluation of the technical implementability of a technology are the type of contaminants present at a site and site-specific conditions which may limit the implementability of a technology. Examples of the application of these factors include the screening of a technology because it treats volatile organics, when inorganics are the contaminants of concern, or the screening of a technology which cannot be applied to a site due to site-specific subsurface conditions. The technologies or technology process options which do not pass the screening process on the basis of technical implementability are not retained for further consideration.

A combined technology screening was performed for all the sites addressed within the Initial Screening of Alternatives. The technology screening for

soils/sediments at Sites 05, 08, 10 and 13 is presented in Table B-1 while the technology screening for ground water at Site 10 is presented in Table B-3. The technology screening for addressing PCB-contaminated building materials at Sites 12 and 14 is presented in Table B-5.

The technology screening tables each include brief descriptions of the individual technologies or process options. More detailed descriptions of the technologies are provided in the text which follows the technology and process option screening tables.

The technology screening tables also include comments on the general applicability of the technologies and limiting characteristics which prevent their application at certain sites. For some technologies, no site-specific or contaminant-specific characteristics which limit the technical implementability of a technology are identified. For these, the word "none" appears in the limiting characteristics column.

For those technology screening tables which address multiple sites (Tables B-1 and B-5), a screening status column is included to summarize for which sites a technology will be retained for further analysis and for which sites a technology will be screened. A technology or process option title block is shaded gray only for those technologies which have been screened from further analysis for all of the sites.

Although the technology screening is presented in a combined manner, the technical implementability of a given technology was evaluated individually for each site. Where sites have been grouped (e.g., Sites 05 and 13 are both included in the Group I sites), the technical implementability of addressing both sites has been considered. For example, although on-site incineration would not be technically implementable at Site 05 due to its limited areal extent (the site is not big enough to set up an on-site incinerator within its

boundaries), an on-site incinerator could potentially be implemented at Site 13, which is larger in size. Therefore, on-site incineration has been retained for further consideration at both Sites 05 and 13.

Process Option Screening

technically those technologies which are identification of Upon implementable, the process options are further evaluated to allow the selection of a representative process option for each technology type. process options are evaluated on the basis of effectiveness, implementability, Factors considered in the effectiveness evaluation include the effectiveness of the process in handling the estimated areas or volumes of media, its ability in meeting remediation goals, potential impacts to human health and the environment during construction and implementation, and how proven and reliable the process is. Both technical and administrative feasibility are considered in the implementability evaluation while relative capital and O&M costs are broadly compared in the cost evaluation.

As with the technology screening, a combined process option screening was conducted for all the sites addressed within the Initial Screening of Alternatives. The process option evaluations for soil/sediment at Sites 05, 08, 10 and 13 are presented in Table B-2 while the process option screening for ground water at Site 10 is presented in Table B-4. The process option evaluation for PCB-contaminated building materials at Sites 12 and 14 is presented in Table B-6. Process options which are selected as representative process options are noted with an asterisk.

For those process option screening tables which address multiple sites (Tables B-2 and B-6), a comment column has been added which indicates for which site or sites a process option has been selected as a representative

process option. Based on site contaminants or site-specific features, different process options are selected for the various sites. As with the technology screening, while the process option screening is presented in a combined manner, each process option was evaluated with respect to its applicability to each individual site.

TABLE B-1 SOIL/SEDIMENT REMEDIAL TECHNOLOGY SCREENING SITES 05, 08, 10, AND 13 NCBC-DAVISVILLE

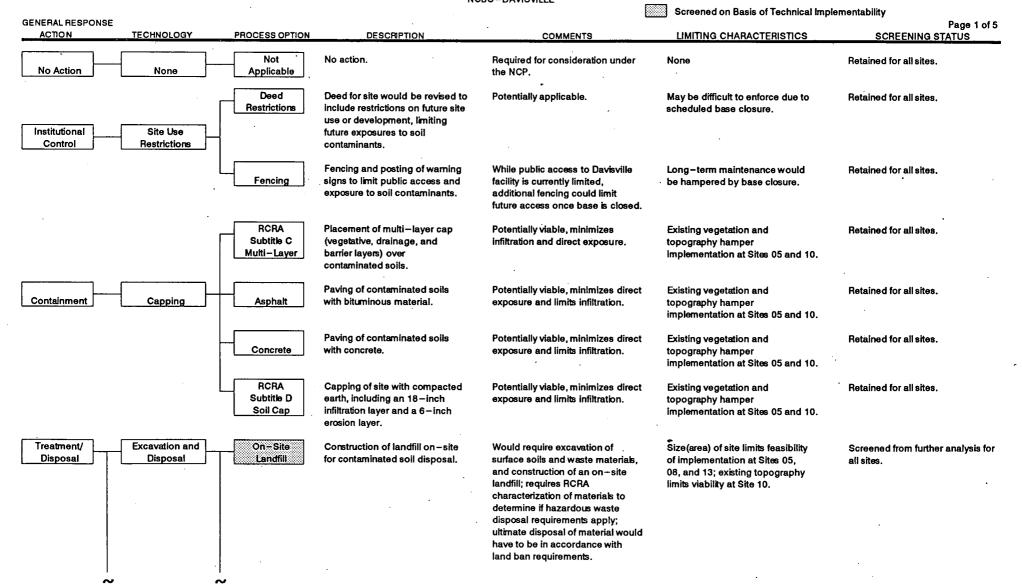


TABLE B-1 SOIL/SEDIMENT REMEDIAL TECHNOLOGY SCREENING SITES 05, 08, 10, AND 13 NCBC-DAVISMILE

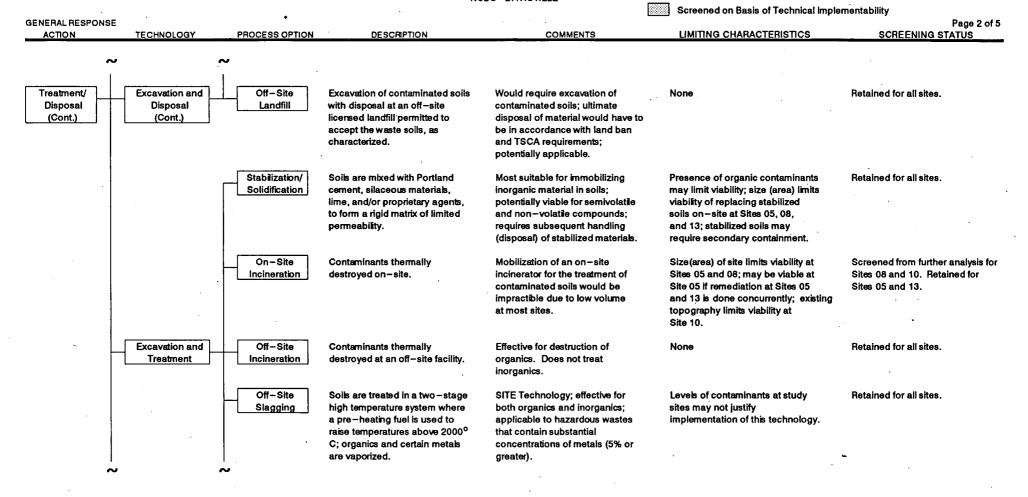


TABLE B-1 SOIL/SEDIMENT REMEDIAL TECHNOLOGY SCREENING SITES 05, 08, 10, AND 13 NCBC-DAVISVILLE

Screened on Basis of Technical Implementability

GENERAL RESPONSE Page 3 of 5 ACTION **TECHNOLOGY** PROCESS OPTION DESCRIPTION COMMENTS LIMITING CHARACTERISTICS **SCREENING STATUS** Treatment/ Disposal Mechanical/ Volatile compounds are Effective for removal of volatile Not applicable to PCB, PAH or Screened from further analysis for (Cont.) removed from soils through Thermal organics from soils. Less effective inorganic soil contaminants at all sites. Excavation and Aeration heating and/or mechanical than incineration in treating Sites 05, 08, 10, and 13, Treatment aeration. semi-volatiles. Does not treat (cont.) inorganics or waste materials. Plasma Heat from a plasma torch Most appropriate for soils and None Retained for all sites. Reactor creates a molten bath used to sludges contaminated with metals detoxify soils; organics are and hard-to-destroy organics: vaporized and residual melt SITE technology. material retains metals in an unleachable matrix. Thermal Organic contaminants are Proven for treatment of VOCs, Most applicable to heavily Screened for sites with low level Desorption volatilized by an externally-fired BNAs, and PCBs; not applicable contaminated materials; residual (< 1 ppm) contamination (Sites rotary dryer and removed as a to contaminants with low vapor levels are reported as less than 05, and 10). Retained for Sites condensed liquid. pressures and inorganic 1 ppm. 08 and 13. contaminants. Excavation and Soil Use of an extractant solution to Most applicable to sands and Large volume of soil required to Screened for Site 08. Treatment Washing remove contaminants from soils. gravels; handling of mixed justify mobilization/demobilization Retained for Sites 05, 10 and 13. (cont.) Solutions used include water, costs; low soil volumes at Sites 05 soils/wastes would require surfactants, acids, bases, and/or physical separation prior to and 08 limit viability; may be viable oxidizing or reducing agents. treatment. at Site 05 if remediation at Sites 05 and 13 is conducted concurrently. Acid Classified soil is washed with Most effective for inorganic Not applicable to PCB or PAH soil Retained for all sites. Extraction acid and effluent undergoes contaminants; may also be contaminants at Sites 05, 08, and additional treatment. effective for organic wastes; metal 13. Applicable to inorganic -containing acid solution requires contaminants at Sites 05, 08, 10, additional treatment. and 13.

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TABLE B-1 SOIL/SEDIMENT REMEDIAL TECHNOLOGY SCREENING SITES 05, 08, 10, AND 13 NCBC-DAVISWILE

Screened on Basis of Technical Implementability

GENERAL RESPONSE Page 4 of 5 SCREENING STATUS DESCRIPTION COMMENTS LIMITING CHARACTERISTICS ACTION TECHNOLOGY PROCESS OPTION Aerobic biodegradation of Effective for destruction of volatile Not applicable to PAH, PCB or Screened from further analysis for Landfarming contaminants in soils applied to organics. Ineffective for inorganic inorganic soil contaminants at all sites. the ground surface, with nutrient contaminants. Not applicable to Sites 05, 08, 10, and 13. Treatment/ Disposal combined soil/waste matrix. addition. (Cont.) Excavation and Effective for destruction of Not applicable to inorganic or Screened from further analysis for Alkali metals or alkali metal/ Dechlorination polyethylene glycol used to strip liquid-phase chlorinated PAH soil contaminants at Sites 05. Sites 05 and 10. Retained for Treatment organics, dioxins and PCBs. 08, and 10; potentially applicable Sites 08 and 13. (cont.) chlorine atoms from hazardous to PCB contamination at Sites 08 halogenated hydrocarbons. Ineffective for inorganic contaminants. and 13; not well demonstrated. Slurry Phase Excavated soil is prepared into a Not effective for inorganics and Not applicable to PCB, PAH or Screened from further analysis for Biodegradation pumpable slurry to which a certain high molecular weight inorganic soil contaminants at all sites. nutrient rich bacteria is added for semi-volatile compounds. Sites 05, 08, 10 and 13, degradation in a reactor system; additional unit processes may be added. Solvents preferentially dissolve Very limited extent of organic Screened from furthur analysis for Solvent Solvents extract contaminants by Extraction contaminants from a soil matrix preferential solubility; effective for contamination at Sites 08 and 10 Sites 08, and 10. Retained for VOCs, BNAs, and PCBs; limits viability; does not address Sites 05, and 13. and are removed with the inorganic contaminants. solvent for further processing or contaminated solvent solution disposal. requires additional treatment. Not highly effective for PCB, PAH Screened from further analysis for In Situ Stimulation of indigenous Effective for destruction of volatile bacteria or introduced strains, organics, especially proven for or inorganic surficial soil all sites. Treatment Biodegradation with nutrient addition. degradation of fuel spill contamination at Sites 05, 08, 10, contaminants; less effective for and 13. semi-volatile contaminants; ineffective for inorganics.

TABLE B-1 SOIL/SEDIMENT REMEDIAL TECHNOLOGY SCREENING SITES 05, 08, 10, AND 13 NCBC-DAVISVILLE

Screened on Basis of Technical Implementability **GENERAL RESPONSE** Page 5 of 5 ACTION TECHNOLOGY PROCESS OPTION DESCRIPTION COMMENTS LIMITING CHARACTERISTICS SCREENING STATUS \sim ~ Soil Subsurface soil aerated or Ineffective for non-volatile Not applicable to non-volatile soil Screened from further analysis for Venting vacuumed through use of air organics or inorganic contaminants at Sites 05, 08, all sites. "wells" to remove volatile contaminants. 10. and 13. contaminants. Radio Radio frequency waves heat soil Application limited to treatment of Not applicable to non-volatile soil Screened from further analysis for Frequency and thermally decompose. volatile organic contaminants. Not contaminants at Sites 05, 08, all sites. Treatment/ Heating vaporize, and distill hazardous effective for inorganic removal. 10, and 13, Disposal constituents. Not demonstrated on a large (Cont.) scale. Fungal Organic material innoculated with White rot fungi have been proven Not applicable to inorganic or Screened from further analysis for Degradation contaminant-specific fungi are in the treatment of creosote and semivolatile contaminants at Sites Sites 05 and 10. Retained for mixed with soils and additional pentachlorophenol; additional 05, 08, 10, and 13; applicable to Sites 08 and 13. 1. 3 2 20 1 1 1 200 organic material; as the fungi applications for the treatment of PCB contaminants at Sites 08 and degrade the organic material, PCBs are being developed. 13. they also degrade the contaminants. Soil Contaminated soils are flooded Applicable to medium solubility Requires further hydrogeologic Retained for all sites. Flushing In Situ with water, acids, bases, or organics. Acid solutions used for site characterization to confirm Treatment surfactants and the elutriated inorganic contaminants; pilot contact between contaminants (Cont.) solution is collected. scale systems have been and flushing solution and to developed for PCB and confirm ability to recapture semivolatile removal. flushing solution. Contaminated soils are melted Use of in situ vitrification has been Not applicable to surficial soil Screened from further analysis for Vitrification via energy supplied by an temporarily suspended due to a contamination at Sites 05, 08, 10, all sites. electric current, resulting in a recent fire at an ISV test site; and 13. promising technology for in situ glassy crystalline monolith. treatment of underground wastes and debris. In Situ A soil mixing system, consisting Proven for PCBs but not for metals Not applicable to surficial soil Screened from further analysis for Solidification/ of augers through which fixation or organics; best in soils with little contamination at Sites 05, 08, 10, all sites. Stabilization chemicals are injected, is used or no fines; sites with large and 13. to deliver and mix stabilization subsurface obstructions should be chemicals at depth in situ. avoided; freeze/thaw processes can limit long-term effectiveness. Steam Injection Steam is forced into soil via Applicable to soils contaminated Not applicable to surficial soil Screened from further analysis for and Vacuum injection wells to enhance vapor with VOCs and SVOCs. Ineffective contamination at Sites 05, 08, all sites. Extraction extraction; extracted gases are for mixed soil/waste matrix, and 10, and 13. treated using carbon filters. compounds with low vapor pressures.

TABLE B-2 SOIL/SEDIMENT PROCESS OPTION SCREENING SITES 05, 08, 10 AND 13 NCBC-DAVISVILLE

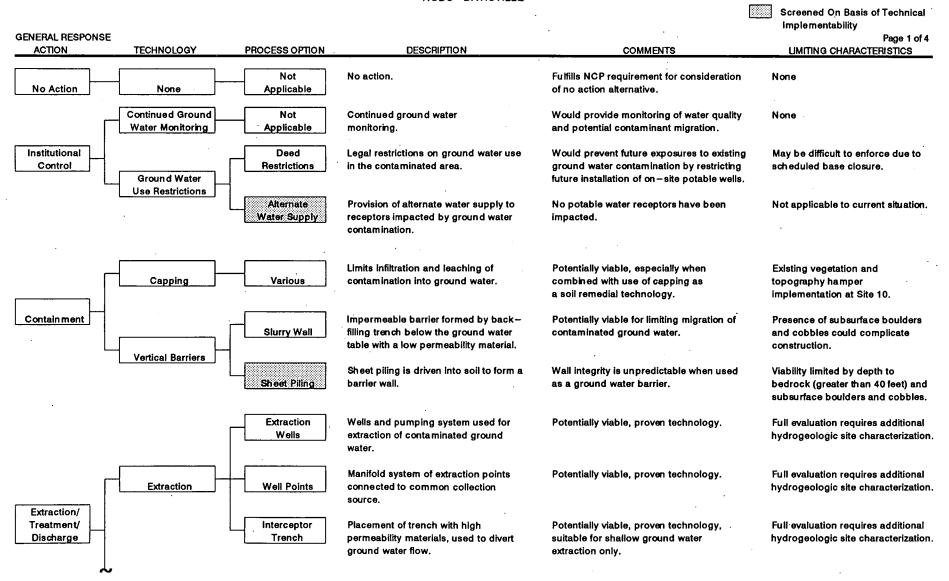
 Representative Process Option **GENERAL RESPONSE** Page 1 of 2 ACTION **TECHNOLOGY** PROCESS OPTION **IMPLEMENTABILITY EFFECTIVENESS** COST COMMENT Not May be effective if ARARs/TBCs No implementation is required. No cost. Selected process option for No Action None Applicable are not exceeded and if the site Sites 05, 08, 10, and 13. poses no unacceptable risks. Deed Limits disturbance of existing Requires appropriate legal Low capital cost. Selected process option for Institutional Site Use Restrictions contamination, unacceptable authority; enforcement may be Sites 05, 08, 10, and 13. Control Restrictions future site use, or introduction of hampered by base closure. additional contaminated materials. • Limits human exposure to site. Easily implemented; Low capital cost; low Selected process option for Fencing maintenance may be hampered maintenance cost. Sites 05, 08, 10, and 13. by base closure. **RCRA** Susceptible to physical damage; Fairly easily implemented; Moderate capital; moderate Subtitle C effective in limiting direct contact requires future land use maintenance. Multi-Layer with contaminated soils and restrictions; not conducive to infiltration. future use of the site. Susceptible to weathering and Easily implemented; requires Low capital; moderate Containment Capping Asphalt cracking; effective in limiting future land use restrictions: maintenance. direct contact with contaminated conducive to future industrial. soils. use of the site. Susceptible to weathering; Easily implemented; requires Moderate to high capital: effective in limiting direct contact Concrete future land use restrictions: moderate maintenance. with contaminated soils and conducive to future industrial infiltration. use of the site. **RCRA** Most easy to maintain; provides Easily implemented; requires Low capital: low to Selected process option for Subtitle D some protection against future land use restrictions. moderate maintenance. Sites 05, 08, 10 and 13. Soil Cap infiltration; easily supports vegetative cover; effective in limiting direct contact with soils. Treatment/ Excavation and Off - Site · Removes soil contaminants as a Requires compliance with land High capital; no O&M. Selected process option for Disposal Disposal Landfill future source of potential human disposal restrictions. Sites 05, 08, 10 and 13. exposure. Excavation and Stabilization/ Effective for immobilizing metals; May require bench - scale Moderate capital, moderate Selected process option for Treatment Solidification mat be effective for semivolatile testing to verify performance. O&M. Sites 05 and 13. and non-volatile organic compounds.

TABLE B-2 SOIL/SEDIMENT PROCESS OPTION SCREENING SITES 05, 08, 10 AND 13 NCBC-DAVISVILLE

 Representative Process Option GENERAL RESPONSE Page 2 of 2 **ACTION TECHNOLOGY** PROCESS OPTION **EFFECTIVENESS** IMPLEMENTABILITY COST COMMENT On-Site · Effective for destruction of Limited number of mobile units High capital: moderate O&M Selected process option for Incineration organic contaminants; requires available; may meet with public Sites 05 and 13. ash disposal. disapproval. Off-Site · Effective for destruction of Due to high demand, delays High capital, low O&M Selected process option for Incineration organic contaminants; requires may be encountered for waste Sites 05, 08 and 13. ash disposal. acceptance. Off-site Effective for organic destruction Demonstrated for metal bearing High capital; negligible to Excavation and Slagging and binding of inorganics into a bag-house dusts; efficiency low O&M. Treatment low permeability slag material. affected by particle size. (Cont.) moisture content and fusion temperature; not widely available. Treatment/ Plasma Effective for organic destruction Emerging technology; not widely High capital; low O&M. Disposal Reactor and binding of inorganics into a available. (Cont.) glasslike matrix. Thermat May not be effective in achieving Not well demonstrated. High capital; moderate Desorption low contaminant levels; more O&M. appropriate for treating grossly contaminated soils. Soil Effectiveness dependent on Not widely available; requires Moderate capital; low to Selected process option for Washing particle/contaminant distribution separation of waste materials moderate O&M. Site 10. and identification of effective prior to soil treatment. surfactant. Acid · Effective in the treatment of Not widely available. Moderate capital: low to Selected process option for Extraction inorganics. moderate O&M. Sites 05 and 13. Shown to be effective for PCBs Not widely available. Moderate capital; low to Dechlorination in soils. moderate O&M. Solvent • Under development; may be Not widely available. Moderate capital; low to Selected process option for Extraction effective in treating PCBs and moderate O&M. Sites 05 and 13. PAHs. In-Situ Fungal Effective for wood preserving Not widely available. Moderate capital; low to Selected process option for Treatment Degradation wastes and PCBs. moderate O&M. Site 08. Soil Under development for Requires recapture of flushing Moderate capital; low to Flushing application to semivolatile -. solutions. moderate O&M.

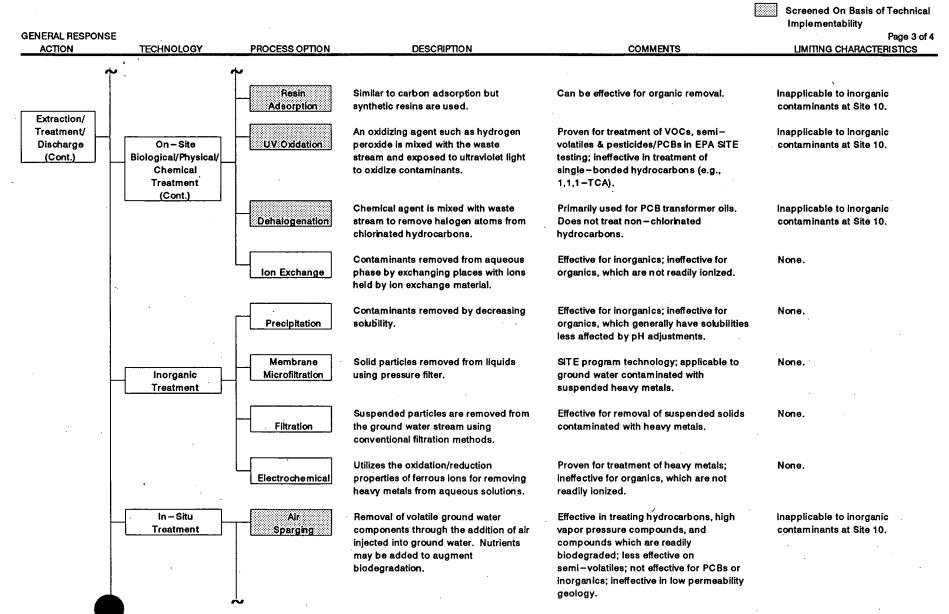
PCB-, and

inorganic-contaminated soils.



Screened On Basis of Technical

Implementability GENERAL RESPONSE Page 2 of 4 ACTION **TECHNOLOGY** PROCESS OPTION DESCRIPTION COMMENTS LIMITING CHARACTERISTICS Off-site Extracted ground water discharged to Regulations often prohibit discharge of None. **POTW** local POTW for treatment. subsurface water to sewer systems. Off-site Extracted ground water discharged to High ground water extraction rates can See comment. prohibit feasibility of this treatment option. RCRA Facility licensed RCRA facility for treatment and/or disposal. Extraction/ Treatment/ Activated sludge process utilizes Proven effective for VOCs and some BNA inapplicable to inorganic Discharge Bioreactor acclimated bacteria for aerobic compounds, ineffective for inorganics. contaminants at Site 10. (Cont.) degradation of contaminants. Organic contaminants removed from Applicable to VOCs, including aromatic Inapplicable to inorganic PACT ground water using powdered hydrocarbons, BNAs, and pesticides. contaminants at Site 10. activated carbon combined with Ineffective for inorganics. conventional biological treatment. Air Transfer of volatile organic compounds Applicable to VOC contaminants, including Inapplicable to inorganic Stripping to gaseous fraction through mixing aromatic hydrocarbons. Ineffective for contaminants at Site 10. Biological/Physical/ with large volumes of air in a packed inorganics, or compounds with low vapor Chemical column. pressures. Treatment Steam Similar to air stripping but the use of Applicable to volatile organic Inapplicable to inorganic Stripping steam increases contaminant contaminants and organics not readily contaminants at Site 10. volatilization. stripped in a regular air stripping system. Carbon Contaminants adsorbed to activated Applicable to organic contaminants, Inapplicable to inorganic Adsorption carbon by internal pores of carbon including aromatic hydrocarbons. contaminants at Site 10. granules. Ineffective for inorganics.



Screened On Basis of Technical Implementability

characterization and definition of

extraction system.

GENERAL RESPONSE Page 4 of 4 **ACTION TECHNOLOGY PROCESS OPTION** DESCRIPTION COMMENTS LIMITING CHARACTERISTICS Extraction/ In - Situ Nutrients and/or enhanced Effective for fuel products; not effective for inapplicable to inorganic Treatment/ Treatment Biodegradation microorganisms are added to ground inorganics or compounds resistant to contaminants at Site 10. Discharge (Cont.) water to augment natural degradation. Limited to geologies (Cont.) biodegradation. favoring aerobic conditions. Ground Treated water is recharged to the Potentially viable. Requires additional hydrogeologic Water ground water via wells and/or characterization and definition of infiltration galleries. extraction system. Treated water is discharged directly or Potentially viable. Requires additional hydrogeologic Discharge Surface Water indirectly (via storm sewer) into surface characterization and definition of water. extraction system. Sanitary Sewer/ Treated water is discharged indirectly Regulations may prohibit discharge of Requires additional hydrogeologic

ground water to sewer system.

to surface water body via sanitary

sewer and POTW.

POTW

TABLE B-4 GROUND WATER PROCESS OPTION SCREENING SITE 10

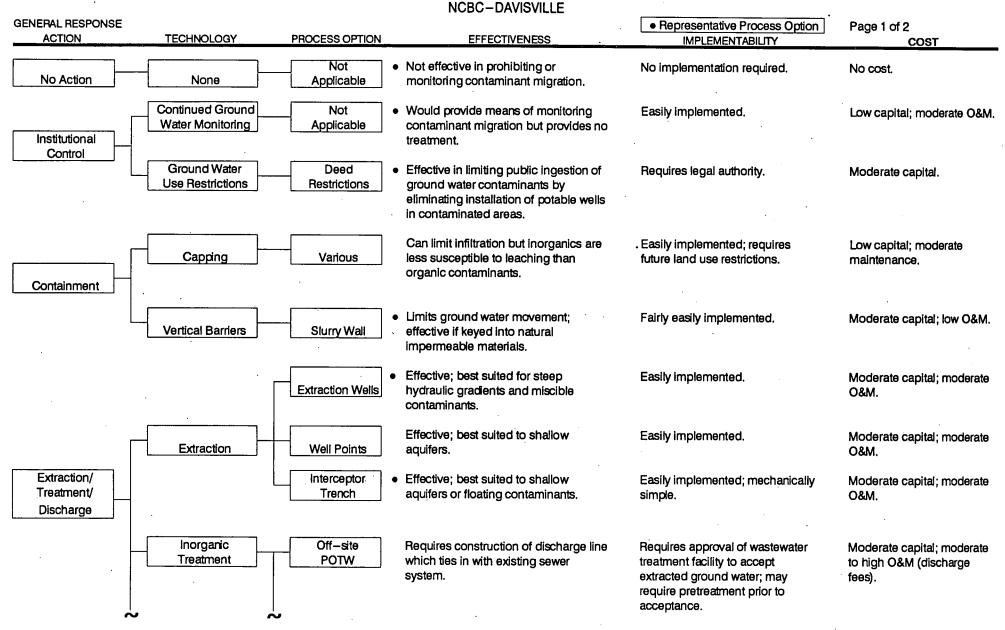


TABLE B-4 GROUND WATER PROCESS OPTION SCREENING SITE 10

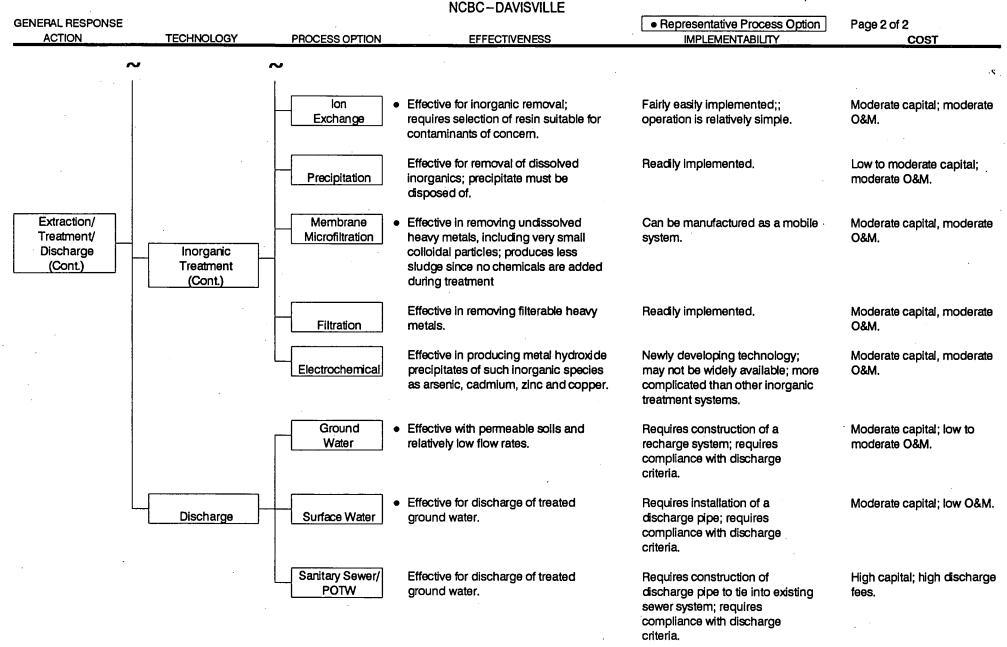


TABLE B-5 PCB-CONTAMINATED BUILDING REMEDIAL TECHNOLOGY SCREENING SITES 12 AND 14 NCBC-DAVISVILLE

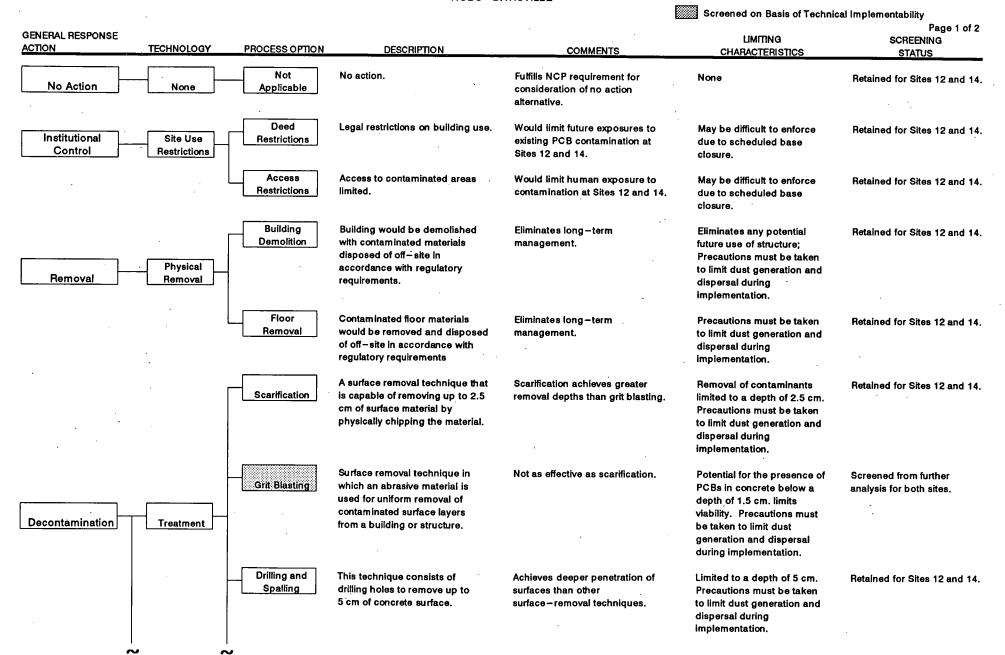


TABLE B-5 PCB-CONTAMINATED BUILDING REMEDIAL TECHNOLOGY SCREENING SITES 12 AND 14 NCBC-DAVISVILLE

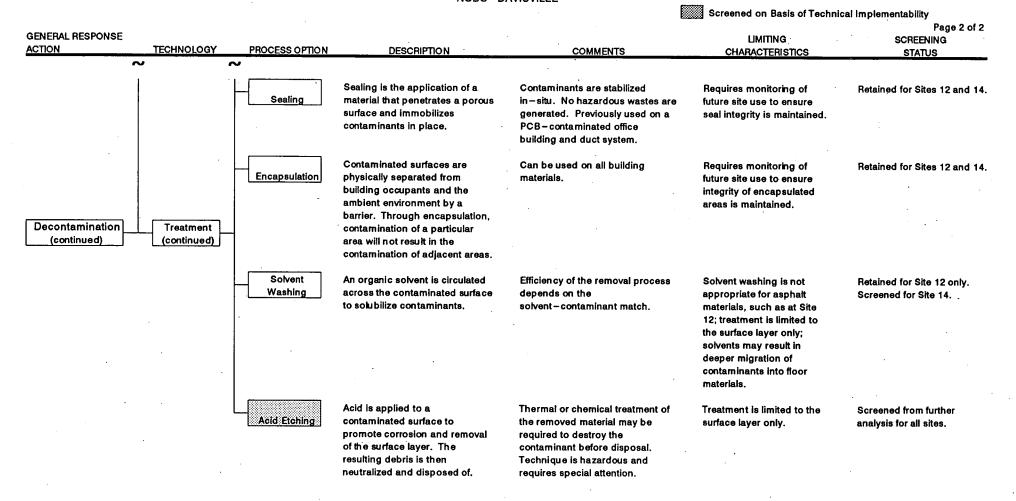


TABLE B – 6 PCB – CONTAMINATED BUILDING REMEDIAL PROCESS OPTION SCREENING SITES 12 AND 14 NCBC – DAVISVILLE

Representative Process Option Page 1 of 1 GENERAL RESPONSE **PROCESS OPTION EFFECTIVENESS** ACTION **TECHNOLOGY** IMPLEMENTABILITY COST Not effective in preventing Not No implementation is required. No cost. No Action Applicable exposures to contaminated None materials. Limits future activities on-site Deed Fairly easily implemented. Low capital. Institutional Site Use Restrictions and therefore limits potential Restrictions Control exposures to contaminated materials. Access Limits human exposures to site Easily implemented; requires Low capital, low Restrictions by limiting access to maintenance of long-term access maintenance. contaminated areas. restrictions. Building Removes contaminants of Fairly easily implemented. High capital. Demolition concern by demolishing entire building; potential future use of Removal Physical building is eliminated. Action Removal Floor Removes contaminated material Fairly easily implemented; Moderate capital. Removal only from building. requires dust control during implementation. Fairly easily implemented; quite Moderate to high Effective in removing Scarification time consuming; requires dust contaminants in building capital. surfaces to a depth of 2.5 cm. control during implementation. Drilling and Effective in removing Fairly easily implemented; Moderate to high Spalling contaminants in building requires dust control during capital. surfaces to a depth of 5 cm. implementation. Decontamination Treatment Effectiveness as a permanent Fairly easily implemented. Moderate capital; Sealing barrier has not yet been moderate established. maintenance. Very effective. However, future Moderately easy to implement. Moderate capital; Encapsulation use of encapsulated areas may moderate be limited. maintenance. Solvent . Moderate to high Not effective on asphaltic Equipment set-up and removal Washing surfaces; tempique may require time depends on the size and capital. configuration of equipment. more than application; remedial time frame uncertain.

TECHNOLOGY AND PROCESS OPTION SCREENING

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Deed Restrictions

Deed restrictions represent a means to restrict ground water use. Basically, all properties within a contaminated area are restricted, with respect to ground water usage based on restrictions placed within the deed to the property.

Capping

Capping is a process used to cover contaminated materials to prevent their contact with the land surface, infiltrating precipitation and/or ground water.

There are a variety of designs and capping materials available. The designs of modern caps may conform to the performance standards of 40 CFR 264.310, which addresses RCRA landfill closure requirements (Subtitle C caps). 40 CFR 258 presents standards for municipal solid waste landfill caps (Subtitle D caps). Most cap designs are multi-layered in accordance with the above-mentioned design standards; however, single-layered designs are also used for special purposes. The selection of capping materials and a cap design is influenced by specific factors such as local availability, costs of cover materials, desired function of cover materials, the nature of the contaminated materials, local climate and hydrogeology, and projected future use of the site in question.

Capping is applicable whenever contaminated materials are to be buried or left in place at a site. In general, capping is performed when extensive subsurface contamination at a site precludes excavation and removal of wastes because of potential hazards and/or unrealistic costs.

Capping is often performed together with ground water extraction or other containment technologies to prevent, or significantly reduce further plume development, thus reducing the time needed to complete ground water cleanup operations.

The main disadvantages of capping are the need for long-term maintenance and uncertain design life. Another disadvantage to capping is the high cost of proper soil and drainage materials in certain areas of the country.

On-Site Landfill

Construction of an on-site landfill suitable for the disposal of hazardous wastes would require the design and construction of the facility in accordance with RCRA requirements, as specified under 40 CFR Part 264. These requirements preclude construction of such a facility in areas such as the 100-year floodplain or in seismically unstable areas. The landfill must be constructed with the appropriate liner and leachate collection systems. Ground water monitoring long-term site management would also be required under RCRA. Land disposal regulations would apply to materials disposed of in an on-site landfill.

Off-Site Landfill

The disposal of contaminated media from a site at an off-site landfill has several advantages as well as disadvantages. Advantages include the lack of long term on-site management, the rapidity with which this may be implemented, the use of commonly employed excavation and trucking techniques. Disadvantages include the need to properly sample and analyze the waste material for proper characterization necessary to meet landfill requirements, the lack of destruction of the waste material, and the general lack of properly permitted and operating landfills who would accept the waste material.

Stabilization

Stabilization represents a treatment method that neutralizes hazardous contaminants and improves a waste's physical characteristics. Specifically, stabilization utilizes formulated reagents in combination with the waste to maintain contaminants in their most immobile form. This is achieved by reducing a waste's solubility or chemical reactivity. A wide range of reagents is available for stabilizing both organic and inorganic contaminated wastes.

Incineration

Incineration involves the thermal destruction of contaminants. High temperature oxidation occurring under controlled conditions degrades contaminants into products that generally include carbon dioxide, water vapor, sulfur dioxide, NO_{X} , hydrogen chloride gases and ash. Air pollution control equipment is necessary to minimize the discharge of gaseous contaminants into the air. Organics are destroyed in the treatment process. Some metals such as arsenic, mercury, and lead may vaporize during incineration. Other metals typically are not treated and remain in the ash residual. Incineration can be implemented on-site or off-site. A substantial treatment volume is typically required for on-site incineration to be a cost-effective alternative. Off-site incinerators are not plentiful, and delays in their acceptance of a given wastestream are not uncommon due to their great demand. Some common incinerator types include rotary kiln, fluidized bed and infrared thermal incinerators.

Slagging

Slagging is a high temperature process for the treatment of both organic and inorganic wastes. In a two-stage, high-temperature system, carbonaceous fuel is combusted with oxygen-enriched air under fuel-rich conditions in the first stage (burner section) followed by pneumatic injection of the waste into the hot (2,200-2,500 degree C) reducing flame in the second stage (reactor section). The intensive process conditions allow reaction times to be short (less than one-half second) and permit a high waste throughput. Close control of the operating parameters enables extraction of valuable metals and destruction of hazardous organic constituents.

The process temperature inside the reactor section is between 1,400 and 1,850 degrees C. In the high-temperature reducing atmosphere, metals such as zinc, lead, arsenic, and cadmium are vaporized from the waste along with volatile components such as alkali and halide compounds. Less volatile metals such as

copper, nickel, and cobalt, if present in sufficient quantities, coalesce as a molten alloy. The remaining components of the waste, including some metal oxides such as those of iron, melt into a molten slag.

The reactor feeds into a slag separator, or horizontal cyclone, where the process gases and volatile compounds are separated from the molten materials. The slag is continuously tapped and solidified on a non-contact, water-cooled, vibrating conveyor. The process gases are drawn from the slag separator through the off-gas system where the vapors are post-combusted with ambient air and condensed as metal oxides, and all remaining H2 and CO are combusted to water vapor and carbon dioxide. The gases are subsequently cooled, and the mixed metal oxide particulate is collected in a pulse-jet baghouse. A clean off-gas is discharged to the atmosphere.

Mechanical/Thermal Aeration

Mechanical/thermal aeration employs vapor pressure or volatility to separate contaminants from the media of interest. In these systems, soils are exposed to large quantities of air which allows the transfer of the volatile component from the liquid to the gaseous phase. To achieve the exposure, mechanical means such as tilling or other rotary operations may be used. Often heat is applied to this system to achieve separations of relatively high vapor pressure organic compounds.

Plasma Reactor

In a plasma reactor, feed material is heated in a molten bath where, under extremely high temperatures, it is detoxified. The melted matrix solidifies, with the inorganics retained in the final solid phase. The residual is a non-leachable, glassy residue which meets TCLP criteria. This technology is relatively innovative, with few vendors offering treatment systems. (SITE - Retech)

Thermal Desorption

Thermal desorption involves the use of a dryer to volatilize water and organic contaminants from the feed material into an inert carrier gas stream. The gas stream is treated to remove dust particles and a portion of the organic contaminants. The gas then passes through heat condensers, where it is cooled. The majority of the gas is reheated and recycled through the treatment system. A small portion is passed through a particulate filter and a carbon adsorption system before discharge. A thermal desorption process offered by Chemical Waste Management, Inc. (the X*TRAX system) is reported to reduce volatile organic concentrations to less than 1 ppm, semivolatile organic concentrations to less than 1 ppm, semivolatile organic concentrations to less than 10 ppm, and PCB concentrations to 2 to 25 ppm (from feed streams of 120 to 6,000 ppm). The feed material must be less than 2 inches in particle size and a minimum of 5,000 cubic yards is necessary for the system to be economically feasible.

Soil Washing

The soil washing process works on the principle that the majority of contaminants are associated with the fine-grained particles in the soil, and that the coarser-grained fraction is relatively clean. A typical soil washing process involves the separation of coarser-grained soils by creating a slurry

and treating the slurry within a hydrocylone. The coarse fraction is washed with a surfactant to remove contaminants and separated from the contaminants within an air flotation tank. The cleaned sand is dewatered and placed back on-site. The fine-grained fraction and contaminant-containing froth from the air flotation unit are dewatered, with the residual sludge requiring off-site disposal. The technology is reported to be effective on heavy metals, semi-volatile organics and PCBs. It is currently a relatively innovative technology, not widely proven in the United States.

Acid Extraction

Soil is treated by being washed in hydrochloric acid to remove inorganic contaminants. The soil is mixed with a hydrochloric acid solution with a pH less than 2. After extraction, the treated soils are rinsed, neutralized, and dewatered. The extractant solution is regenerated, with entrained soil, organics and heavy metals removed. The concentrated metal solution requires off-site treatment or, potentially, metals recovery. While only tested in the laboratory on a limited, bench-scale basis, the projected treatment capacity is 20 tons per hour.

Landfarming

Landfarming involves the above-grade treatment of soils using conventional soil management practices to enhance the microbial biodegradation of contaminants. Typically, soils are spread over a lined area with a drainage system installed between the soil and the liner. If volatile organics are being treated, the system is usually enclosed. Spray irrigations provides moisture control and distribution of nutrients and bacteria. Contaminated leachate collected by the drainage system can be reapplied to the surface. Landfarming has been used for the treatment of pesticides, creosote wastes, and aromatic hydrocarbons.

Fungal Treatment

This biological treatment process utilizes white rot fungi to treat soils in situ. This technology is typically used to treat soil contaminated with creosote-related compounds and currently the SITE Demonstration Program is evaluating its effectiveness in degrading pentachlorophenol (PCP). The treatment process consists of mixing contaminated soils with organic material inoculated with the fungi and wood chips. As the fungi degrade the wood, they also degrade the soil contaminants.

Dechlorination

Dechlorination is a process which involves the remediation of soils, sediments or liquid-phase wastes contaminated with chlorinated organic compounds. Various dechlorination processes have been developed. Typically these involve the replacement of chlorine atoms in halogenated compounds with atoms from the dechlorination agent, thereby rendering the original PCB compound a substituted aromatic compound which is no longer a PCB aroclor. The majority of these technologies are innovative and not widely proven.

Slurry Phase Biodegradation

This process is used to remediate soils and sludges contaminated with biodegradable organics in a manner similar to conventional activated sludge treatment. An aqueous slurry of waste material is prepared and environmental conditions are optimized for biodegradation. The slurry is aerated and mixed to allow for bacterial biodegradation of contamination. In some processes, contaminant-specific bacteria are used to effect treatment. Volatilization of VOCs is a potential concern in the system operation. The system can be combined with land treatment. Most applications to date have been for treating sludges containing petroleum and wood preservative organics such as creosote and pentachlorophenol.

Solvent Extraction

This process uses a solvent to extract contaminants from soil or sludge. Many variations of the process are currently being developed by different vendors and are being demonstrated under the SITE program. Liquified gases, such as propane, or liquid solvents are used to extract the organics from the wastestream. The soils are mixed with the solvent, followed by solvent recovery and soil drying. Vendors claim the process is successful in treating a wide range of organic compounds, including PCBs, wood preservatives, PAHs and other organics.

In Situ Biodegradation

In situ biodegradation is a technique for treating zones of contamination by microbial degradation processes. The basic concept involves altering environmental conditions to enhance microbial catabolism or cometabolism of organic contaminants, resulting in the breakdown and detoxification of those contaminants. This technology has developed rapidly over recent years, and bioreclamation appears to be one of the most promising of the in-situ treatment techniques.

Microbial metabolic activity can be classified into three main categories: aerobic respiration, in which oxygen is required as a terminal electron acceptor; anaerobic respiration, in which sulfate or nitrate serves as a terminal electron acceptor; and fermentation, in which the microorganism rids itself of excess electrons by exuding reduced organic compounds.

The bioreclamation method that has been most developed and is most feasible for in-situ treatment is one which relies on aerobic (oxygen-requiring) microbial processes. This method involves optimizing environmental conditions by providing an oxygen source and nutrients which are delivered to the subsurface through an injection well or infiltration system to enhance microbial activity.

The feasibility of bioreclamation as an in-situ treatment technique is dictated by waste and site characteristics. More specifically, those factors which determine the applicability of a bioreclamation approach are: biodegradability of the organic contaminants, environmental factors which affect microbial activity, and site hydrogeology.

Soil Venting

Soil venting is an in situ process in which a vacuum is applied to soils in the vadose zone. As the vacuum pulls air through the unsaturated soils, contaminants volatilize and are removed in the air stream. The air is then treated with activated carbon or a catalytic converter to remove organics prior to being discharged to the atmosphere. This technology is applicable to the in situ treatment of volatile organic hydrocarbons, including petroleum-and solvent-related contaminants, in the unsaturated zone and is often combined with in situ biodegradation.

Radio Frequency In Situ Heating

This technology involves the heating of soil in situ with radio frequency waves to thermally decompose, vaporize and distill hazardous constituents. Radio frequency energy is transmitted to the ground by inserting electrode tubes vertically into the contaminated soil or be placing an array of electrodes horizontally above the soil surface. As the soil temperature increases, hydrocarbons are volatilized or stripped from the soil by rising steam. Pyrolysis also contributes to the removal of contaminants. A vapor barrier placed over the surface captures the vapors and gases and the gases are further treated by incineration or carbon adsorption. The technology has been tested in the removal of tetrachloroethylene, PCBs and jet fuel (Hazardous Waste Consultant, 1990).

Soil Flushing

Soil flushing is similar to soil washing but it is performed in situ. As the soil washing fluid percolates down through the soil, it chemically reacts with, solubilizes, or emulsifies the contaminants. The solution and entrained contaminants are captured by a network of drains or wells and extracted for further treatment or disposal. It is best applied in highly permeable soils and may be most effective when combined with another in situ process such as chemical oxidation or bioremediation. Four different approaches (surfactant washing, hot water displacement, alkali-polymer-surfactant flooding and metal extraction) may be applicable to contaminants such as PCBs, oils, chlorinated solvents, creosote wastes, and inorganics. (Hazardous Waste Consultant, 1992).

In Situ Vitrification

In situ vitrification represents an innovative technology that electrically melts the waste media, creating an extremely stable glass-like solid. This process can be used to treat soil and sludges contaminated with mixtures of various waste types (i.e., organic, inorganic, and radioactive. In a typical arrangement, four electrodes connected to a utility distribution system are ingested into the soil. As current flows between electrodes, the adjacent soil is heated to 1600-2000°C. Advantages of in-situ vitrification include the potential ability to destroy, remove, or immobilize all contaminant groups and to reduce the volume of waste media being treated. Disadvantages of this process include the need to treat off-gas and the high capital costs associated with this process.

Steam Injection and Vacuum Extraction

This technology is similar to soil venting but utilizes steam to remove subsurface contaminants. Steam is injected into the subsurface via steam injection wells. The steam heats the subsurface soils, increasing the vapor pressure of the volatile contaminants and thereby increasing the rate at which they can be stripped from the soils. The air and steam are removed via vacuum extraction wells and undergo treatment prior to discharge or reuse within the treatment system. This treatment system treats both volatile organics and semivolatile organics in the subsurface and can be combined with in situ biodegradation.

Alternate Water Supply

Alternate water supply represents another type of institutional control in restricting ground water usage. Basically, ground water that is contaminated is no longer utilized as a potable water source, and an alternate source is tapped.

Vertical Barriers

Vertical barriers are low permeability cut-off walls or diversions installed below ground to contain, capture, or redirect ground water flow in the vicinity of a site. The most commonly used vertical barriers are slurry walls, particularly soil-bentonite slurry walls. Less common are cement-bentonite or concrete slurry walls, grouted barriers, and sheet piling cut-offs. Vertical barriers are most effective when they can "key" into natural subsurface impermeable layers. Shallow slurry walls keyed into impermeable clays offer a cost-effective means of reducing the ground water flow in unconsolidated earth materials.

Extraction Wells

Extraction wells represent a conventional technology which is frequently used in the removal of contaminated ground water. Stainless steel or PVC well casings and screens are installed within the contaminant plume, and submersible pumps are most commonly used to extract water from the well. An array of wells with overlapping radii of influence can be designed to capture an entire plume or to halt further migration. Accurate data from a site-specific pump test usually provides the hydrogeologic parameters necessary for the design of well system configurations.

Well Points

This ground water collection technology involves the removal of ground water through a group of closely spaced wells connected by a header pipe. The wells are installed by driving a perforated pipe with a pointed cap into the area to be dewatered. Well point systems are best suited for shallow aquifers where extraction is not needed below twenty feet. The suction lifting pump technique commonly employed with well points is ineffective beyond this depth (U.S. EPA, 1985b).

Extraction Trench (French Drain)

Extraction trenches may be employed as a means of collecting ground water through a perforated pipe placed below the natural ground water table. Ground water enters the perforated pipe and flows by gravity to the lowest point in the pipe where it is pumped to the surface for treatment and/or discharge. This technology is typically limited to areas where the depth to ground water is not so deep that trench construction becomes prohibitively expensive or complicated (bracing, etc.). This technology offers the advantage of a horizontally oriented intake structure which allows collection of ground water within the area of interest. Additionally, trenches are relatively simple to construct and are passive structures with little maintenance required.

Treatment at a POTW

This technology involves the discharge of wastewater from a site to a Publicly Owned Treatment Works (POTW) for off-site treatment. Aqueous wastes can constitute the majority of waste treated during a remedial cleanup effort. These aqueous wastes can include ground water, leachate, surface runoff, and other aqueous wastes. A number of criteria must be met when utilizing a POTW. These restrictions, as they apply to CERCLA sites, are detailed in the U.S. EPA's CERCLA Site Discharges to POTWs: Guidance Manual (U.S. EPA, 1990a).

Treatment at a RCRA Facility

Discharge to a RCRA facility represents an off-site treatment technology for remediating contaminated ground water. The extracted ground water is collected and transported off-site to a licensed RCRA facility for treatment. High extraction rates can greatly limit the cost-effectiveness of this alternative.

Biological Treatment

Biological water treatment methods have been well proven in their application at municipal wastewater treatment facilities. Recently, their application to the treatment of hazardous wastes has been evaluated. Biological treatment removes organic matter from the wastestream through biological degradation.

The most prevalent form of biological treatment is aerobic (i.e., in the presence of oxygen). Aerobic biological treatment can be effective for the treatment of aromatic hydrocarbons, polynuclear aromatic hydrocarbons, and phenols. The wastestream's biological oxygen demand (BOD) can provide an indication of the treatability of the waste by aerobic treatment.

Specialized biological treatment systems are being developed for specific contaminants not treatable under normal aerobic conditions. Such systems utilize contaminant-specific bacteria or special environmental conditions to enhance the biodegradation of the target contaminants.

Powdered Activated Carbon Treatment/Wet Air Oxidation

Powdered activated carbon treatment is a treatment process where powdered activated carbon is added to a traditional aerated biological treatment process. Treatment is achieved both through the biological degradation of contaminants and the adsorption of non-degradable contaminants onto the

carbon. It is often combined with wet air oxidation (WAO), where the WAO destroys the adsorbed pollutants and biomass while regenerating the carbon for reuse in the treatment system. WAO is a chemical treatment process which utilizes high temperatures (347-608°F) and pressures (300-3000 psig) to oxidize dissolved or suspended contaminants in aqueous waste streams. Generally, WAO is applicable for treating certain organic-containing media that are too toxic for biological remediation and too dilute to incinerate economically (Surprenant, 1988). Pressure, temperature, and time are controlled to achieve desired reductions in contaminant levels.

Air Stripping

Air stripping, a physical treatment method, consists of the mass transfer of a volatile chemical from a liquid phase to air by bringing a flow of air in contact with the liquid. Air strippers come in a variety of configurations, but the basic principle behind their operation is the same for each type.

The most common configuration in ground water treatment is the countercurrent packed tower, in which contaminated water is trickled downward over rings, spheres, or other types of packing material in a stainless steel, fiberglass, or PVC cylinder. Clean air is blown upward through the tower, volatilizing contaminants and exhausting them out the top. Air stripping is effective with contaminants exhibiting high Henry's law constants, which relate equilibrium concentrations of a chemical compound in liquid and gas phases. Removal efficiencies can vary widely depending on types of contaminant, influent concentrations, stripper design, temperature, and a number of other factors. However, a properly designed and operated air stripper can be expected to achieve greater than 95% removal efficiency for contaminants (Canter, et al., 1986).

Emission controls on the stripping column are often required to collect exhausted contaminants. Although this reduces the simplicity of the system, small carbon adsorption units can be connected to the gaseous outflow to capture contaminants. Environmental effects of exhausted contaminants are probably minimal, since most volatile organic compounds have atmospheric half-lives (time to degrade 50% of the contaminant) on the order of minutes or hours (Cuppitt, 1980).

Steam Stripping

Steam stripping differs from air stripping by the injection of steam, as opposed to air, into a tray or packed distillation column in order to remove volatile organic chemicals from waste streams. This type of process option is most effectively applied to aqueous solutions for the removal of volatile organic compounds that are immiscible in water. Steam stripping is more economical and effective than air stripping for treating wastes with high concentrations of volatiles and wastes with contaminants which have a low volatility (Surprenant, 1988). In regard to the specific treatment process, the waste stream enters near the top of the column and then flows by gravity countercurrent to the steam. As the waste stream passes down through the column, volatile compounds within the waste stream are lost to the steam/organic vapor stream rising from the bottom of the column. The concentration of volatile compounds in the waste stream reaches a minimum at the bottom of the column. The overhead vapor is condensed as it exits the column and the condensate is then decanted to achieve water/solvent separation.

Carbon Adsorption

One of the most frequently applied technologies for the removal of low concentrations of organics from waste streams is carbon adsorption. The process consists of bringing contaminated ground water in contact with a bed of granular activated carbon (GAC), where contaminants are held by physical and/or chemical forces on the activated surface of the carbon itself. The system is usually configured as one or several columns in series which are filled with activated carbon. Carbon adsorption is effective with a wide variety of organic contaminants, but the performance of the process can be influenced by pH, the adsorptive capacity of the carbon, and temperature. Removal efficiencies of greater than 99% can be expected (Canter, et al., 1986).

Spent activated carbon (carbon which has reached its adsorption capacity) must be regenerated through the application of heat. This usually entails removal of carbon from the unit for regeneration at an off-site incinerator. Operation of units in series prevents shutoff of the entire system during regeneration.

Resin Adsorption

Resin adsorption represents another physical treatment option for the removal of organic contaminants from aqueous waste streams. The operation of resin adsorption is similar to that of carbon adsorption. Specifically, organic molecules contacting the resin surface are held on the surface by physical forces and are subsequently removed during the resin regeneration cycle. Even though the process operation of resin adsorption is similar to carbon adsorption, many aspects of the two technologies differ. For example, the bonding forces in resin adsorption are usually weaker than those encountered in granulated activated carbon adsorption and therefore, resins may be regenerated chemically rather than thermally, as carbon adsorption systems must be regenerated. Resins generally have a lower adsorption capacity than carbon. Resin adsorption is most practical for treatment of colored organic wastes, when material recovery is practical, where selective adsorption is desired, where low leakage rates are required, where carbon regeneration is not practical and where the wastestream contains high levels of dissolved inorganic solids (Berkowitz, et al., 1978).

Reverse Osmosis

Osmosis is the spontaneous flow of solvent (e.g., water) from a dilute solution through a semipermeable membrane (impurities or solute permeates at a much slower rate) to a more concentrated solution. Reverse osmosis is the application of sufficient pressure to the concentrated solution to overcome the osmotic pressure and force the net flow of water through the membrane toward the dilute phase. This allows the concentration of solute (impurities) to be built up in a circulating system on one side of the membrane while relatively pure water is transported through the membrane. Ions and small molecules in true solution can be separated from water by this technique.

In the treatment of hazardous waste streams, the use of reverse osmosis is primarily limited to polishing low flow streams containing highly toxic contaminants. In general, good removal can be expected for high molecular weight organics and charged anions and cations. Multivalent ions are treated

more effectively than are univalent ions. However, reverse osmosis units are subject to chemical attack, fouling, and plugging. Pretreatment requirements can be expensive. Wastewater must be pretreated to remove oxidizing materials such as iron and manganese salts, to filter out particulates, adjust pH, and to remove oil, grease, and other film forms.

The most critical design consideration applicable to reverse osmosis technology is the design of the semipermeable membrane. Membranes are usually fabricated in flat sheets or tubular forms and are assembled into modules. The most common materials used are cellulose acetate and other polymers such as polyamides and polyether-polysulphone.

Ultraviolet (UV) Oxidation

UV oxidation is a chemical process which utilizes an oxidant in combination with ultraviolet radiation to treat specific waste streams containing phenols, cyanides, chlorinated hydrocarbons, organic sulfur compounds, and other rapidly oxidized organics. This process option transforms the contaminants into a less hazardous form. When reactions are carried to completion, halogenated compounds are converted to carbon dioxide, water, and residual halides. Treatment data indicate that destruction of organic contaminants to non-detectable levels is achieved within minutes (Hager, et al., 1987).

Dehalogenation

Dehalogenation is a chemical treatment process whereby a chemical agent is mixed with the waste stream to remove halogen atoms from chlorinated hydrocarbons. Dehalogenation is primarily used to treat PCB transformer oils. Dehalogenation, however, does not treat non-chlorinated hydrocarbons.

Ion Exchange

Ion exchange is a process whereby the toxic ions are removed from the aqueous phase by being exchanged with relatively harmless ions held by the ion exchange material. Ion exchange is a well established technology for removal of heavy metals and hazardous anions from dilute solutions. Ion exchange can be expected to perform well for these applications when fed wastes of variable composition, provided the system's effluent is continually monitored to determine when the resin bed exhaustion has occurred. However, the reliability of ion exchange is markedly affected by the presence of suspended solids.

Ion exchange systems are commercially available from a number of vendors. The units are relatively compact and are not energy intensive. Although exchange columns can be operated manually or automatically, manual operation is better suited for hazardous waste site applications because of the diversity of wastes encountered. In addition, use of several exchange columns at a site can provide considerable flexibility.

Precipitation

Precipitation is a physiochemical process whereby some or all of a substance in solution is transformed into a solid phase. It is based on alteration of the chemical equilibrium relationships affecting the solubility of inorganic species. Removal of metals as hydroxides or sulfides is the most common

precipitation application in wastewater treatment. Generally, lime or sodium sulfide is added to the wastewater in a rapid mixing tank along with flocculating agents. The wastewater flows to a flocculating chamber in which adequate mixing and retention time is provided for agglomeration of precipitate particles. Agglomerated particles are separated from the liquid phase by settling in a sedimentation chamber, and/or by other physical processes such as filtration.

Membrane Microfiltration

Membrane microfiltration involves the use of an automatic pressure filter in which the filter material has tiny openings (0.10 microns or 1 ten-millionth of a meter) which allow for the filtration of particles normally not separated from the wastestream using standard filtration processes. Membrane microfiltration is most applicable to hazardous waste suspensions, ground water contaminated with heavy metals, landfill leachate and process wastewaters containing uranium (U.S. EPA, 1991).

Filtration

Filtration is a type of physical separation of a solid material based on particle size. As commonly employed in ground water treatment, filtration involves the separation of suspended solids, primarily silt, from the influent stream. Filters generally work on the same principal as a domestic vacuum cleaner whereby particles are intercepted in a fabric. Fabric size, particle size, and density differences each play a role in the proper selection of a filtration device.

Electrochemical

Electrochemical treatment provides treatment of inorganic contaminants. Contaminated water passes through an electrochemical cell where ferrous ions, hydroxide ions and hydrogen are produced. The ferrous ions act as reducing agents for oxidized heavy metals and also react with the hydroxide ions, forming iron hydroxides and metal hydroxides. The metal hydroxides are removed by adsorption onto the iron hydroxide precipitate that is formed (Hazardous Waste Consultant, 1991).

Air Sparging

Air sparging involves the injection of air into special air injection wells. The air then "bubbles" up through the saturated subsurface soils into the unsaturated zone. As the air passes through the contaminated ground water in the saturated zone, it strips volatile organic contaminants from the ground water. The contaminants enter the vapor phase of the unsaturated zone and are then removed using conventional vapor extraction technology. This technology has not been widely proven and its effectiveness in treating contaminated ground water is not well demonstrated.

Discharge to Ground Water

Treated ground water can be subsequently discharged to ground water using recharge basins, infiltration galleries or reinjection wells. The technology selected for recharge is dependent on site-specific considerations such as available space, extent of contamination, and hydrogeology. Ground water

recharge systems can provide an added element of hydraulic control to ground water extraction systems. Typically recharge systems can be subject to clogging or other operational problems and must be closely monitored. Compliance with ground water discharge regulations must also be maintained.

Discharge to Surface Water

Treated ground water can also be discharged to a surface water body. This technology is typically easy to implement, given a surface water body is nearby. It requires compliance with NPDES requirements.

Discharge to Sanitary Sewer/POTW

If available nearby, discharge of treated or untreated ground water to a sanitary sewer for subsequent treatment at a Publicly Owned Treatment Works (POTW) is a possible alternative. Many POTWs have regulations prohibiting discharges of ground water to the treatment system and special approval for such a discharge may be required. The POTW may also require pretreatment of the wastestream prior to acceptance.

Building Demolition

Building demolition, a removal technology, provides a means to permanently remove contaminated surfaces to a licensed off-site landfill or treatment facility. Demolished building surfaces need to be sampled and analyzed prior to off-site disposal in order to properly characterize the waste and to determine associated disposal/treatment requirements. In addition, confirmatory sampling must be conducted to assure that all areas of contamination have been addressed.

Scarification

In this surface removal process, a scarifier tool consisting of pneumatically operated piston heads strike the contaminated surface, causing the concrete to chip off. Scarification is capable of removing contaminated surfaces to a depth of 2.5 cm. This technique is suitable for application in large open areas and small areas.

Grit Blasting

Grit blasting represents another type of surface removal technique in which an abrasive material is sprayed under high pressure for the removal of contaminated surface layers from a building or structure. This technique is used extensively throughout the industry to remove paint and contaminants near building surfaces. However, grit blasting is effective only as a surface treatment.

Drilling and Spalling

This surface removal technique consists of drilling holes into the concrete surface and then inserting a spalling bit to hydraulically spread and spall the contaminated surface. Greater penetration and, therefore, deeper removal of contaminated surfaces represents an advantage of this technique over other surface removal techniques. However, drilling and spalling is not suitable for hard-to-reach areas such as behind pipes and equipment and is applicable to concrete only (not concrete block).

Sealing

Sealing is the application of a material that penetrates a porous surface and immobilizes contaminants in-place. Contaminants are stabilized in-situ with no hazardous wastes generated. Although it is believed to act more like a barrier than a detoxifier, a manufacturer has provided evidence indicating that its sealant may facilitate chemical degradation⁽¹⁾. The effectiveness of sealants as a permanent barrier has not yet been established.

Encapsulation

In an encapsulation process, contaminants or contaminated structures are physically separated from building occupants and the ambient environment by a barrier. Acting as an impenetrable shield, a barrier keeps contaminants inside and away from clean areas, thereby alleviating the hazard. However, encapsulated structures are usually rendered inaccessible or inoperable since they are physically sealed off by the barrier or enclosure.

Solvent Washing

In this decontamination process, an organic solvent is circulated across the surface of a building to solubilize contaminants. Spent solvent is either thermally or chemically treated to remove contaminants and recycled if no degradation of the solvent occurs during treatment. The solvent washing removal system's applicability and its corresponding efficiency are dependent on the solvent-contaminant match. It should be noted that penetration of the solvent into the material matrix, followed by outward diffusion, may require a long period of time.

Acid Etching

Acid is applied to a contaminated surface to promote corrosion and removal of the surface layer. Thermal or chemical treatment of the removed material may be required to destroy the contaminant before disposal. Acid may cause decomposition of the contaminant as it is removed from the surface. This technique is applicable primarily to contaminants on mild steel and wood surfaces. Acid etching is only a surface treatment and is not effective on subsurface contamination of building materials.

APPENDIX C

GROUP I SITES (SITES 05, 06 AND 13)
PRELIMINARY COST ESTIMATES

ALTERNATIVE I-2 FENCING AND MAINTENANCE SITE 05 (TRANSFORMER OIL DISPOSAL AREA) AND SITE 13 (DISPOSAL AREA NORTHWEST)

	_					1992	1992	Years	(1) Present
Item	Quantity Units	Unit Price	Basis Year	Reference E	scalation	Unit Costs	Costs	(O&M)	Value (O&M)
CAPITAL COST - DIRECT			•					•	
Site Use Restrictions									
 Chain Link , 9 gauge wire, aluminized steel, 6' high 	2200 i. ft.	\$13.50	1992	2	1.000	\$13.50	\$29,700.00		
 Gate (3 ft wide – Site 05) 	1 each	\$235.00	1992	2	1.000	\$235.00	\$235.00		
 Gate (12 ft wide – Site 13) 	1 each	\$720.00	1992	2	1.000	\$720.00	\$720.00		
- Warning Signs	22 each	\$42.00	1992	2	1.000	\$42.00	\$924.00	,	•
Total Direct Capital Cost									\$31,579.00
CAPITAL COST - INDIRECT									
Engineering and Design (10 %)				1					\$3,157.90
Legal and Administrative (4%)				1		,			\$1,263.16
TOTAL CAPITAL COSTS									\$36,000.06
OPERATION AND MAINTENANCE C	OCTO								
- Site Fence Maintenance	1 each	\$100.00	1988	4	1.119	\$111.90	\$111.90	30	\$1,720.13
TOTAL NET PRESENT VALUE OF O	& M								\$1,720.13
				 					Ţ.,. <u></u>
SUBTOTAL COST			,				••		\$37,720.19
CONTINGENCY (20%)	-			•					\$7,544.04
TOTAL PRESENT VALUE COST FOR	RFENCING								\$45,264.22

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE I-3 RCRA SUBTITLE D SOIL CAP OPTION A SITE 05 (TRANSFORMER OIL DISPOSAL AREA) AND SITE 13 (DISPOSAL AREA NORTHWEST)

						1992	1992	Years	(1) Presen
Item	Quantity Units	Unit Price	Basis Year	Reference E	scalation	Unit Costs	Costs	(O&M)	Value (O&N
CAPITAL COST - DIRECT									-
Site Preparation									
Clear Vegetation and				•					
								•	
Brush (Site 05 only)	0.5 acres	\$3,825.00	1992	2	1.000	\$3,825.00	\$1,912.50		
Cap									
- 18" Infiltration Layer	3,800 cu. yd.	\$13.00	1992	23	1.000	\$13.00	\$49,400.00		
- 6" Erosion Layer	7,700 sq. yd.	\$4.01	1992	2	1.000	\$4.01	\$30,877.00		
- Seed, Fertilizer, Mulch	69 msf	\$44.00	1992	2	1.000	\$44.00	\$3,036.00		
- Health & Safety (17%)							\$14,163.21		
Equipment Decontamination									
- Rental of Steam Cleaner	1 month	\$400.00	1992	2	1.000	\$400.00	\$400.00		
- Construction of Decon Pit									
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
- Polyethylene Tarpaulin	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		
- Disposal (Tanker Truck)	1 each	\$1,000.00	1992	13	1.000	\$1,000.00	\$1,000.00		
Dust Control						•	•		
- Water Tank Sprayer	1 month	\$1,975.00	1992	2	1.000	\$1,975.00	\$1,975.00		
Total Direct Capital Cost									\$102,935.8
CAPITAL COST - INDIRECT									
ngineering and Design (10 %)				4					440 000 =
egal and Administrative (4%)				1					\$10,293.5
	· · _								\$4,117.4
TOTAL CAPITAL COSTS									\$117,346.8
OPERATION AND MAINTENANCE (COSTS								
Cap Operation and Maintenance									
- Annual Inspection	1 each	\$250.00	1988	3	1.119	\$279.75	\$279.75	30	64 300 0 4
- Repairs (per year)	1 each	\$500.00	1988	3	1.119	\$559.50	\$559.50	30 30	\$4,300.32
		4000.00	1000	· ·	1.110	Ψ353.30	, \$339.30	30	\$8,600.63
OTAL NET PRESENT VALUE OF C) & M								\$12,900.95
SUBTOTAL COST				•					\$130,247.77
CONTINGENCY (20%)									\$26,049.55
OTAL PRESENT VALUE COST FO	R RCRA SUBTITLE D	SOIL CAP							\$156,297.33

ALTERNATIVE I-3 RCRA SUBTITLE D SOIL CAP OPTION B

	_					1992	1992	Years	(1) Present
Item	Quantity Units	Unit Price	Basis Year	Reference E	scalation	Unit Costs	Costs	(O&M)	Value (O&M)
CAPITAL COST - DIRECT									
Site Preparation		•							
- No Significant Preparation Nece	essarv								
Сар	,								
- 18" Infiltration Layer	2,600 cu. yd.	\$13.00	1992	23	1.000	\$13.00	\$33,800.00		
- 6" Erosion Layer	5,200 sq. yd.	\$4.01	1992	2	1.000	\$4.01	\$20,852.00		
- Seed, Fertilizer, Mulch	46 msf	\$44.00	1992	2	1.000	\$44.00	\$2,024.00		
- Health & Safety (17%)		·	.**				\$9,634.92		
Equipment Decontamination			•				•		
- Rental of Steam Cleaner	1 month	\$400.00	1992	2	1.000	\$400.00	\$400.00		
- Construction of Decon Pit							•		
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
- Polyethylene Tarpaulin	400 sq. ft.	\$0.32	1992	2 .	1.000	\$0.32	\$128.00		
- Disposal (Tanker Truck)	1 each	\$1,000.00	1992	13	1.000	\$1,000.00	\$1,000.00	•	
Dust Control		·			• •				
- Water Tank Sprayer	1 month	\$1,975.00	1992	, 2	1.000	\$1,975.00	\$1,975.00		
Total Direct Capital Cost									\$69,858.02
CAPITAL COST - INDIRECT									
Engineering and Design (10 %)				1					\$6,985.80
Legal and Administrative (4%)			•	1					- \$2,794.32
TOTAL CAPITAL COSTS	-		· · · · · · · · · · · · · · · · · · ·		 	<u> </u>			\$79,638.14
OPERATION AND MAINTENANCE	COSTS								
Cap Operation and Maintenance	•								
- Annual Inspection	1 each	\$250.00	1988	3	1.119	\$279.75	\$279.75	30	\$4,300.32
- Repairs (per year)	1 each	\$500.00	1988	3	1.119	\$559.50	\$559.50	30	\$8,600.63
TOTAL NET PRESENT VALUE OF	O & M							· · · · · · · · · · · · · · · · · · ·	\$12,900.95
									#00 F00 00
SUBTOTAL COST									\$92,539.09
CONTINGENCY (20%)	ND DOD 4 6: 107771 = 5			-		•			\$18,507.82
TOTAL PRESENT VALUE COST FO	DH HCHA SUB IITLE [SUIL CAP			T.				\$111,046.91
1) Coloulated based on 50/ later									

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE I-4, OPTION A SOIL EXCAVATION AND OFF-SITE DISPOSAL AT HAZARDOUS WASTE LANDFILL/OFF-SITE INCINERATION SCENARIO 1

Item	Quantity Units	Unit Price	Basis Year	Reference E	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M
CAPITAL COST - DIRECT								_	
Site Preparation									
- Clear Vegetation and	•								
Brush (Site 05 only)	0.5 acres	\$3,825.00	1992	2	1.000	\$3,825.00	\$1,912.50		
Soil Excavation		40,020.00	,,,,	-	1.000	Ψ0,020.00	Ψ1,512.00		
-Mob/Demob	1 time	\$345.00	1992	2	1.000	\$345.00	\$345.00		•
-Excavation with Backhoe	5,100 cu. yd.	\$2.89	1992	2	1.000	\$2.89	\$14,739.00		
(2 1/2 cu. yd. bucket)	,			_		, 42.00			
-Health & Safety (17%)							\$2,505.63		
Equipment Decontamination							4 2,000.00		
- Rental of Steam Cleaner	1 month	\$400.00	1992	2	1.000	\$400.00	\$400.00		
 Construction of Decon Pit 		•		-,		*	4.00.00		
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
 Polyethylene Tarpaulin 	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		
Dust Control	•	·				****	,		
 Water Tank Sprayer 	1 month	\$1,975.00	1992	2	1.000	\$1,975.00	\$1,975.00		
Treatment						.,.,			
 Handling, Transport and Disposal Disposal of Excavated Soil to a 	ll of 1								
Hazardous Waste Landfill	6,900 tons	\$400.00	1992	21	1.000	\$400.00	\$2,760,000.00		
 Handling, Transport and 			•			*	4-1 ,		
Disposal of Excavated Soil to	•								
an Incinerator	750 tons	\$3,160.00	1992	22	1.000	\$3,160.00	\$2,370,000.00		
Clean Common Earth Backfill						, ,	,,,		
(including loading, transportation,		•							
and compaction)	5,100 cu. yd.	\$11.34	1992	2	1.000	\$11.34	\$57,834.00		
Seed, Fertilizer, and Mulch	69 msf	\$44.00	1992	2	1.000	\$44.00	\$3,036.00		
Total Direct Capital Costs	· · · · · · · · · · · · · · · · · · ·								\$5,212,919.2
CAPITAL COST - INDIRECT		•	• .						
Engineering and Design (10 %)				1		•			\$521,291.92
Legal and Administrative (4%)				1					\$208,516.77
TOTAL CAPITAL COSTS							· · · · · · · · · · · · · · · · · · ·		\$5,942,727.92
CONTINGENCY (20%)							,		¢1 100 545 5
TOTAL PRESENT VALUE COST FOR	SOIL EXCAVATION	N AND DISPOS	SAL					-	\$1,188,545.58 \$7,131,273.5
1) - Calmilated based on 5% interes	t rata								

^{(1) -} Calculated based on 5% interest rate.

ALTERN E I-4, OPTION A

SOIL EXCAVATION AND OFF-SITE DISPOSAL AT HAZARDOUS WASTE LANDFILL/OFF-SITE INCINERATION

SCENARIO 2

Item	Quantity Units	Unit Price	Basis Year	Reference Es	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M
CARITAL COOT DIDECT						,			
CAPITAL COST - DIRECT							•		
Site Preparation									
 No Preparation Necessary Soil Excavation 				•					
- Mob/Demob	1 time	\$345.00	1992	•	4 000	6045.00	#04E 00		
- Excavation with Backhoe		•	1992	2 2	1.000 1.000	\$345.00	\$345.00		٠.
	3,600 cu. yd.	\$2.89	1992	2	1.000	\$2.89	\$10,404.00		
(2 1/2 cu. yd. bucket)							04 700 00		
-Health & Safety (17%)							\$1,768.68		
Equipment Decontamination — Rental of Steam Cleaner	4	6400.00	1992	•	4.000	£400.00	6400.00		
	1 month	\$400.00	1992	2	1.000	\$400.00	\$400.00		
 Construction of Decon Pit Excavate Pit 	45	60.04	1000	0	4.000	00.04	044.40	•	
	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
Polyethylene Tarpaulin Dust Control	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		
- Water Tank Sprayer	4	64.075.00	1992	•	4 000	04.075.00			
Treatment	1 month	\$1,975.00	1992	2	1.000	\$1,975.00	\$1,975.00		
- Handling, Transport and	•			•					
Disposal of Excavated Soil to									•
a Hazardous Waste Landfill	4,600 tons	\$400.00	1992	21	1.000	\$400.00	61 040 000 00		
	4,000 1005	\$400.00	1992	21	1.000	\$400.00	\$1,840,000.00		
 Handling, Transport and Disposal of Excavated Soil to 	750 tons	\$3,160.00	1992	22	1.000	£2.460.00	en 270 000 00		
an Incinerator	750 10118	\$3,100.00	1992	22	1.000	\$3,160.00	\$2,370,000.00		
Clean Common Earth Backfill									
•				,					
(including loading, transportation,		\$11.34	1000	•	1 000	644.04	£40.004.00		
and compaction) Seed, Fertilizer, and Mulch	3,600 cu. yd. 46 msf		1992	2 2	1.000	\$11.34	\$40,824.00		•
Seed, Fertilizer, and Mulch	40 msi	\$44.00	1992	2	1.000	\$44.00	\$2,024.00		
Total Direct Capital Costs									\$4,267,912.78
CADITAL COST INDIDECT								<u> </u>	
<u>CAPITAL COST - INDIRECT</u> Engineering and Design (10 %)				1					£40£ 704 00
Legal and Administrative (4%)	•		•	1		-			\$426,791.28
Legal and Administrative (4%)									\$170,716.51
TOTAL CAPITAL COSTS									\$4,865,420,57
OONTNOTNOV (CCC)	•								
CONTINGENCY (20%)			041					•	\$973,084.11
TOTAL PRESENT VALUE COST FOR	SOIL EXCAVATION	N AND DISPO	SAL						\$5,838,504.68

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE I-4, OPTION B ROTARY KILN INCINERATION OF SOIL SCENARIO 1

<u>Item</u>	Quantity Units	Unit Price	Basis Year	Reference E	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M
CAPITAL COST - DIRECT									·····
Site Preparation				•					
Clear Vegetation and									
Brush (Site 05 only)	0.5 acres	\$3,825.00	1992	2	1.000	#2 OOE 00	¢4 040 50		
Soil Excavation	0.5 acres	φ5,625.00	1992	2	1.000	\$3,825.00	\$1,912.50		
- Mob/Demob	1 time	\$345.00	1992	. 2	1.000	\$345.00	¢245.00		
- Excavation with Backhoe	5,100 cu. yd.	\$2.89	1992	2	1.000	\$345.00 \$2.89	\$345.00		
(2 1/2 cu. yd. bucket)	5,100 ca. ya.	Ψ2.03	1332	2	1.000	⊅∠.09	\$14,739.00		
-Health & Safety (17%)			•				\$2,505.63		
Equipment Decontamination							φ2,303.63		
- Rental of Steam Cleaner	1 month	\$400.00	1992	2	1.000	\$400.00	\$400.00		
- Construction of Decon Pit		\$100.00	1002		1.000	\$ +00 .00	φ 4 00.00		
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
- Polyethylene Tarpaulin	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		
Dust Control	100 04.11.	, 40.02		-	1.000	Ψ0.02	Ψ120.00		
- Water Tank Sprayer	1 month	\$1,975.00	1992	2	1.000	\$1,975.00	\$1,975.00		
Treatment		4.,5.0.00		_	1.000	Ψ1,010.00	Ψ1,570.00		
-Transportable Rotary Kiln (including loading, transportation	1								
and compaction)	7,700 tons	\$400.00	1989	9	1.098	\$439.20	\$3,381,840.00	•	
-Transport of Site 05 Soil to						•			
Site 13 for Incineration	2,100 tons	\$2.11	1992	2	1.000	\$2.11	\$4,431.00		
 TCLP Analysis of Ash 	5 samples	\$1,440.00	1991	20	1.046	\$1,506.24	\$7,531.20		
Ash Disposal	•					•	• •		
 Placement of Ash 	5,100 cu. yd.	\$1.34	1992	2	1.000	\$1.34	\$6,834.00		
- 6" Topsoil	69 msf	\$405.00	1992	2	1.000	\$405.00	\$27,945.00		
 Seed, Fertilizer, and Mulch 	69 msf	\$44.00	1992	2	1.000	\$44.00	\$3,036.00		
Total Direct Capital Costs	-						· · · · · · · · · · · · · · · · · · ·		\$3,453,666.43
CAPITAL COST - INDIRECT					·	•			
Engineering and Design (15 %)				1		•			\$518,049.96
egal and Administrative (5%)				1					\$172,683.32
OTAL CAPITAL COSTS									\$4,144,399.72
CONTINGENCY (90%)									
CONTINGENCY (20%)	ON OFF 11001-							•	\$828,879.94
OTAL PRESENT VALUE COST FOR	ON-SITE INCINERA	ATION							\$4,973,279.66

ALTERNATIVE 1-4, OPTION B ROTARY KILN INCINERATION OF SOIL SCENARIO 2

	Oversity Heire	Ush Dates	Regio Vene	Datasanas E	acclation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M
Item	Quantity Units	Unit Price	Basis Tear	Reference E	Scalation	Unit Cosis	Cosis	(Ualvi)	Value (Oalvi
CAPITAL COST - DIRECT									
Site Preparation				•					
- No Preparation Necessary	•								
Soil Excavation	•					•			
- Mob/Demob	1 time	\$345.00	1992	2	1.000	\$345.00	\$345.00		
-Excavation with Backhoe	3,600 cu. yd.	\$2.89	1992	2	1.000	\$2.89	\$10,404.00		
(2 1/2 cu. yd. bucket)		, —			•	•			
-Health & Safety (17%)		•					\$1,768.68		
Equipment Decontamination				•			• •		•
- Rental of Steam Cleaner	1 month	\$400.00	1992	2	1.000	\$400.00	\$400.00		
- Construction of Decon Pit	,	4		_		¥•			
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
- Polyethylene Tarpaulin	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		•
Dust Control	700 04.11.	40.02		_			¥ <u></u>		
- Water Tank Sprayer	1 month	\$1,975.00	1992	2.	1.000	\$1,975.00	\$1,975.00		
Treatment	1 111011111	Ψ1,010.00	1002		1.000	\$1,010.00	41,010.00		•
-Transportable Rotary Kiln									
(including loading, transportation			•					•	
and compaction)	, 5,400 tons	\$400.00	1989	9	1.098	\$439.20	\$2,371,680.00		
- TCLP Analysis of Ash	3 samples	\$1,440.00	1991	20	1.046	\$1,506.24	\$4,518.72		
Ash Disposal	o samples	Ψ1,440.00	1001	20	1.040	Ψ1,000.E4	ψ1,010.7£		
- Placement of Ash	3,600 cu. yd.	\$1.34	1992	2	1.000	\$1.34	\$4,824.00		
- 6" Topsoil	46 msf	\$405.00	1992	2	1.000	\$405.00	\$18,630.00		
- Seed, Fertilizer, and Mulch	46 msf	\$44.00	1992	2	1.000	\$44.00	\$2,024.00		
- Seed, Fertilizer, and Mulch	40 1115	\$44.00	1992	2	1.000	φ44.00	Ψ2,024.00		
Total Direct Capital Costs									\$2,416,741.50
CAPITAL COST - INDIRECT	·								
Engineering and Design (15%)				1					\$362,511.23
Legal and Administrative (5%)				1					\$120,837.08
				•					,,
TOTAL CAPITAL COSTS									\$2,900,089.80
CONTINGENCY (20%)							•		\$580,017.96
TOTAL PRESENT VALUE COST FOR	ON-SITE INCINER	RATION							\$3,480,107.76
) - Calculated based on 5% interes		· · · · · · · · · · · · · · · · · · ·		<u> </u>			·		

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE I-4, OPTION C SOIL EXCAVATION AND STABILIZATION/SOLIDIFICATION SCENARIO 1

item	Quantity Units	Unit Price	Basis Year	Reference Es	calation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M
CARITAL COOT DIDECT									
CAPITAL COST - DIRECT									
Site Preparation									
- Clear Vegetation and	0.5	00 005 00	1000	•	4 000	00 005 00	04.040.50		
Brush (Site 05 only)	0.5 acres	\$3,825.00	1992	2	1.000	\$3,825.00	\$1,912.50		
Soil Excavation			4000						
- Mob/Demob	1 time	\$345.00	1992	. 2	1.000	\$345.00	\$345.00		
- Excavation with Backhoe	5,100 cu. yd.	\$2.89	1992	2	1.000	\$2.89	\$14,739.00		
(2 1/2 cu. yd. bucket)		•							
-Health & Safety (17%)			•				\$2,505.63		
Equipment Decontamination									
 Rental of Steam Cleaner 	1 month	\$400.00	1992	2	1.000	\$400.00	\$400.00		
 Construction of Decon Pit 			,						
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
 Polyethylene Tarpaulin 	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		
Dust Control	•					•			
- Water Tank Sprayer	1 month	\$1,975.00	1992	2	1.000	\$1,975.00	\$1,975.00		
reatment						. ,			
- Transport of Site 05 Soil	, .			*					
to Site 13	2100 tons	\$2.11	1992	2	1.000	\$2.11	\$4,431.00		
- Mob/Demob	1 time	\$100,000.00	1992	17	1.000	\$100,000.00	\$100,000.00		
- Stabilization	7,700 tons	\$200.00	1991	27	1.046	\$209.20	\$1,610,840.00		
- TCLP Analysis of Stabilized Soil	5 Samples	\$1,440.00	1991	20	1.046	\$1,506.24	\$7,531.20		
- Stabilized Soil Disposal	7,700 tons	\$72.00	1991	14	1.046	\$75.31	\$579,902.40		
Clean Common Earth Backfill	7,700 10113	Ψ/ 2.00	1551	14	1.040	Ψ/ 0.01	ψοτο ₁ σος.πο		
(including loading, transportation,									
and compaction)	5,100 cu. yd.	\$11.34	1992	2	1.000	\$11.34	\$57,834.00		
Seed, Fertilizer, and Mulch	5,100 cu. ya. 69 msf	\$11.34 \$44.00	1992	. 2	1.000	\$11.34 \$44.00	\$57,834.00 \$3,036.00		
seed, Perulizer, and Mulcir	os ms	\$44 .00	1992	. 2	1.000	Ф44 .00	\$3,U30.UU		
otal Direct Capital Costs									\$2,385,623.8
CAPITAL COST - INDIRECT									
Engineering and Design (10 %)		•		. 1			,		\$238,562.3
egal and Administrative (4%)				1					\$95,424.9
				.					Ψ35,727.5
OTAL CAPITAL COSTS									\$2,719,611.1
CONTINGENCY (20%)									\$543,922.2
OTAL PRESENT VALUE COST FOR	SOIL EVOAVATION	AND STABILIZ	ATIONISOUE	MEICATION			,		\$3,263,533.4

ALTERNA 1-4, OPTION C SOIL EXCAVATION AND STABILIZATION/SOLIDIFICATION SCENARIO 2

ltem	Quantity Units	Unit Price	Basis Year	Reference E	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M
OARITAL OOGT PUREOT					`		•		
CAPITAL COST - DIRECT									
Site Preparation									
- No Preparation Necessary									
Soil Excavation			4000	•	4 000	0045.00	0045.00		
- Mob/Demob	1 time	\$345.00	1992	2	1.000	\$345.00	\$345.00		
- Excavation with Backhoe	3,600 cu. yd.	\$2.89	1992	2	1.000	\$2.89	\$10,404.00		
(2 1/2 cu. yd. bucket)						•			
-Health & Safety (17%)							\$1,768.68		
Equipment Decontamination				_					
 Rental of Steam Cleaner 	1 month	\$400.00	1992	2	1.000	\$400.00	\$400.00		
 Construction of Decon Pit 									
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
 Polyethylene Tarpaulin 	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00	•	
Dust Control							*		
 Water Tank Sprayer 	1 month	\$1,975.00	1992	2	1.000	\$1,975.00	\$1,975.00		
Freatment									
 Transport of Site 05 Soil 									
to Site 13	450 tons	\$2.11	1992	. 2	1.000	\$2.11	\$949.50		
Mob/Demob	1 time	\$100,000.00	1992	17	1.000	\$100,000.00	\$100,000.00		•
 Stabilization 	5,400 tons	\$200.00	1991	27	1.046	\$209.20	\$1,129,680.00		
- TCLP Analysis of Stabilized Soil	5 samples	\$1,440.00	1991	- 20	1.046	\$1,506.24	\$7,531.20		
 Stabilized Soil Disposal 	5,400 tons	\$72.00	1991	14	1.046	\$75.31	\$406,684.80		
Clean Common Earth Backfill	·								
(including loading, transportation,									
and compaction)	3,600 cu. yd.	\$11.34	1992	2	1.000	\$11.34	\$40,824.00		
Seed, Fertilizer, and Mulch	46 msf	\$44.00	1992	2	1.000	\$44.00	\$2,024.00		
•			•						
Fotal Direct Capital Costs				·					\$1,702,758.2
CAPITAL COST - INDIRECT		-		•					
Engineering and Design (10 %)				1					\$170,275.8
Legal and Administrative (4%)				1					\$68,110.3
OTAL CAPITAL COSTS				·					\$1,941,144.4
CONTINGENCY (20%)				•	,				\$388,228.8
TOTAL PRESENT VALUE COST FOR		441D OT4 DU 17							\$2,329,373.3

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE I-4, OPTION D SOIL EXCAVATION, ACID EXTRACTION, AND SOLVENT EXTRACTION SCENARIO 1

Item	Quantity Units	Unit Price	Basis Year	Reference E	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M
					11 12.00000	OM COSIO	00010		Value (Oalv
CAPITAL COST - DIRECT				•					
Site Preparation									
- Clear Vegetation and									
Brush (Site 05 only)	0.5 acres	\$3,825.00	1992	2	1.000	\$3,825.00	\$1,912.50	•	
Soil Excavation		•					,		
- Mob/Demob	1 time	\$345.00	1992	2 .	1.000	\$345.00	\$345.00		
- Excavation with Backhoe	5,100 cu. yd.	\$2.89	1992	2	1.000	\$2.89	\$14,739.00		
(2 1/2 cu. yd. bucket)	•								
-Health & Safety (17%)							\$2,505.63		
Equipment Decontamination									
- Rental of Steam Cleaner	1 month	\$400.00	1992	,2	1.000	\$400.00	\$400.00		-
 Construction of Decon Pit 									
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10	•	
 Polyethylene Tarpaulin 	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		
Oust Control					•	•			
 Water Tank Sprayer 	1 month	\$1,975.00	1992	2	1.000	\$1,975.00	\$1,975.00		
reatment	•								
- Transport of Site 05 Soil						•			•
to Site 13	2,100 tons	\$2.11	1992	2	1.000	\$2.11	\$4,431.00		-
 Acid Extraction 	2,700 tons	\$400.00	1992	24	1.000	\$400.00	\$1,080,000.00		
 Solvent Extraction 	5,800 tons	\$400.00	1992	24	1.000	\$400.00	\$2,320,000.00		
- TCLP Analysis of Soil	5 samples	\$1,440.00	1991	20	1.046	\$1,506.24	\$7,531.20		
Clean Common Earth Backfill							•		
(including loading, transportation,	•								
and compaction)	5,100 cu. yd.	\$11.34	1992	2	1.000	\$11.34	\$57,834.00		
Seed, Fertilizer, and Mulch	69 msf	\$44.00	1992	2	1.000	\$44.00	\$3,036.00		
otal Direct Capital Costs					•				\$3,494,881.43
CAPITAL COST - INDIRECT									
ingineering and Design (10 %)				4					6040 400 4
egal and Administrative (4%)				1					\$349,488.14
				1					\$139,795.26
OTAL CAPITAL COSTS									\$3,984,164.83
CONTINGENCY (20%)		•		-				· ·	6700 000 ~
OTAL PRESENT VALUE COST FOR									\$796,832.97

Calculated based on 5% interest rate

ALTERNA E I-4, OPTION D SOIL EXCAVATION, ACID EXTRACTION, AND SOLVENT EXTRACTION SCENARIO 2

						1992	1992	Years	(1) Present
Item	Quantity Units	Unit Price	Basis Year	Reference E	scalation	Unit Costs	Costs	(O&M)	Value (O&N
CAPITAL COST - DIRECT									
Site Preparation									
No Preparation Necessary									
Soil Excavation								•	
- Mob/Demob	. 1 time	\$345.00	1992	2	1.000	\$345.00	\$345.00		
-Excavation with Backhoe	3,600 cu. yd.	\$2.89	1992	2	1.000	\$345.00 \$2.89	\$345.00 \$10,404.00		
(2 1/2 cu. yd. bucket)	3,600 cu. yu.	Ψ2.03	1992	2	1.000	\$2.09	\$10,404.00		
-Health & Safety (17%)							64 700 00		
Equipment Decontamination							\$1,768.68		
- Rental of Steam Cleaner	1 month	\$400.00	1992	2	1.000	\$400.00	\$400.00		
- Construction of Decon Pit	: 11101101	φ + υυ.υυ	1332	2	1.000	φ400.00	Ψ400.00		
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
- Polyethylene Tarpaulin	400 sq. ft.	\$0.32	1992	2	1.000	\$2. 94 \$0.32	\$128.00		
Dust Control	400 Sq. II.	φυ.υ <u>z</u>	1332	2	1.000	φυ.32	φ120.00		
- Water Tank Sprayer	1 month	\$1,975.00	1992	2	1.000	\$1,975.00	\$1,975.00	•	
Treatment	1 IIIOIIII	φ1,313.00	1332	2	1.000	φ1,973.00	φ1,973.00		
- Transport of Site 05 Soil									•
to Site 13	500 tons	\$2.11	1992	2	1.000	\$2.11	\$1,055.00		
- Acid Extraction	500 tons	\$400.00	1992	24	1.000	\$400.00	\$200,000.00		
- Solvent Extraction	5,000 tons	\$400.00	1992	24	1.000	\$400.00	\$2,000,000.00		
- TCLP Analysis of Soil	4 samples	\$1,440.00	1991	20	1.046	\$1,506.24	\$6,024.96		
Clean Common Earth Backfill	, campio	4 1, 1 10.00	.00 /	20	1.010	\$1,000.21	Ψ0,0 2 4.00		
(including loading, transportation,									
and compaction)	3,600 cu. yd.	\$11.34	1992	. 2	1.000	\$11.34	\$40,824.00		
Seed, Fertilizer, and Mulch	46 msf	\$44.00	1992	2	1.000	\$44.00	\$2,024.00		
Total Direct Capital Costs									\$2,264,992.74
CAPITAL COST - INDIRECT									
Engineering and Design (10 %)			•	1	*				\$226,499.27
Legal and Administrative (4%)				1				•	\$90,599.7
TOTAL CAPITAL COSTS									\$2,582,091.72
CONTINGENCY (20%)									\$516,418.34
TOTAL PRESENT VALUE COST FOR	SOIL EXCAVATION	, ACID EXTRA	CTION AND	SOLVENT EX	TRACTION		•		\$3,098,510.07

^{(1) -} Calculated based on 5% interest rate.

COST REFERENCES

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- 5. TRC Environmental Consultants, Inc.; 1991.
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- 8. Compendium of Costs of Remedial Technologies at Hazardous Waste Sites; Environemntal Law Institute; September 1983.
- 9. Pollution Engineering; November 1989.
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- 15. Geraghty & Miller, Inc.; December 1991.
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- 20. Compuchem Analytical Laboratories, November 1991.
- 21. Personal Communication; Envirosafe Services of America, Inc.; July 1992.
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- 24. VISITT Version 1.0; Vendor Information System for Innovative Treatment Technologies, EPA/542/R-92/001, June 1992.
- 25. Palmer, S.A.K., et al., 1988. <u>Metal/Cyanide Containing Wastes Treatment Technologies</u>, Noyes Data Corporation.
- 26. Personal Communication; ENPRO Environmental Professionals, Inc., December 18, 1992.
- 27. EmTech Environmental Services, Inc. November 1991.

APPENDIX D

GROUP II SITES (SITE 08)
PRELIMINARY COST ESTIMATES

ALTERNATIVE II-2 FENCING AND MAINTENANCE SITE 08 - DPDO FILM PROCESSING DISPOSAL AREA

						1992	1992	Years	(1) Present
Item	Quantity Units	Unit Price I	Basis Year	Reference	Escalation	Unit Costs	Costs	(O&M)	Value (O&M)
CAPITAL COST - DIRECT							•		
Site Use Restrictions									
 Chain Link , 9 gauge wire, aluminized steel, 6' high 	140 l. ft.	\$13.50	1992	2	1.000	\$13.50	\$1,890.00		
- Gate (3 ft wide)	1 each	\$235.00	1992	2	1.000	\$235.00	\$235.00		
- Warning Signs	4 each	\$42.00	1992	2	1.000	\$42.00	\$168.00		
Total Direct Capital Cost									\$2,293.00
			•			**************************************			
CAPITAL COST - INDIRECT									
Engineering and Design (10 %)				1				•	\$229.30
Legal and Administrative (4%)				1					\$91.72
TOTAL CAPITAL COSTS									\$2,614.02
OPERATION AND MAINTENANCE CO	<u>osts</u>				•				
 Site Fence Maintenance 	1 each	\$50.00	1988	4	1.119	\$55.95	\$55.95	30	\$860.06
TOTAL NET PRESENT VALUE OF O 8	& M		_				•		\$860.06
SUBTOTAL COST		:							\$3,474.08
CONTINGENCY (20%)									\$694.82
TOTAL PRESENT VALUE COST FOR	FENCING								\$4,168.90

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE II—3 RCRA SUBTITLE D SOIL CAP SITE 08 — DPDO FILM PROCESSING DISPOSAL AREA

						1992	1992	Years	(1) Present
Item	Quantity Units	Unit Price	Basis Year	Reference E	scalation	Unit Costs	Costs	(O&M)	Value (O&M)
CAPITAL COST - DIRECT		•							
Site Preparation									
 No Preparation Necessary 									
Сар									
- 18" Infiltration Layer	140 cu. yd.	\$13.00	1992	23	1.000	\$13.00	\$1,820.00		
- 6" Erosion Layer	280 sq. yd.	\$4.01	1992	2	1.000	\$4.01	\$1,122.80		
- Seed, Fertilizer, Mulch	2.5 msf	\$44.00	1992	2	1.000	\$44.00 -	\$110.00		
Equipment Decontamination				_					
- Rental of Steam Cleaner	1 week	\$135.00	1992	. 2	1.000	\$135.00	\$135.00		
 Construction of Decon Pit Excavate Pit 	45	00.04	4000	•	4 000	20.04	04440		
	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
Polyethylene Tarpaulin	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		
Total Direct Capital Cost									\$3,359.90
CAPITAL COST - INDIRECT									
Engineering and Design (10 %)				4					\$335.99
Legal and Administrative (4%)				¦					\$335.99 \$134.40
Logal and Administrative (+%)				'					φ134.4U
TOTAL CAPITAL COSTS									\$3,830.29
OPERATION AND MAINTENANCE	COSTS								
- Annual Inspection	1 each	\$50.00	1988	. 3	1.119	\$55.95	\$55.95	30	\$860.06
- Repairs (per year)	1 each	\$100.00	1988	· 3	1.119	\$111.90	\$111.90	30	\$1,720.13
TOTAL NET PRESENT VALUE OF (O 0 M								60 500 40
TOTAL NET PRESENT VALUE OF C			. <u> </u>		<u> </u>				\$2,580.19
SUBTOTAL COST									\$6,410.48
CONTINGENCY (20%)									\$0,410.46 \$1,282.10
TOTAL PRESENT VALUE COST FO									\$1,282.10 \$7,692.57

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE II-4, OPTION A SOIL EXCAVATION AND OFF-SITE DISPOSAL AT A HAZARDOUS WASTE LANDFILL SCENARIO 1 SITE 08 - DPDO FILM PROCESSING DISPOSAL AREA

tem	Quantity Units	Unit Price	Basis Year	Reference E	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M
CAPITAL COST - DIRECT									
- Mob/D em ob	1 time	\$345.00	1992	2	1.000	\$345.00	\$345.00		
-Excavation with Backhoe	185 cu. yd.	\$2.89	1992	2	1.000	\$2.89	\$534.65		
(2 1/2 cu. yd. bucket)		4 2.00	1002	-	1.000	Ψ2.03	Ψ337.03		
Equipment Decontamination									
- Rental of Steam Cleaner	1 week	\$135.00	1992	2	1.000	\$135.00	\$135.00		
- Construction of Decon Pit		V 100.00	1002	_	1.000	Ψ100.00	ψ100.00		
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
- Polyethylene Tarpaulin	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		
Oust Control	• "	,		. –		40.02	V120.00		
- Water Tank Sprayer	1 week	\$640.00	1992	2	1.000	\$640.00	\$640.00		
reatment		·				*******	40.0.00	•	
-Transport and Disposal of Excavated Soil to a Hazardous Waste Landfill	278 tons	\$400.00	1992	21	1.000	\$400.00	\$111,000.00		
Clean Common Earth Backfill	185 cu. yd.	\$11.34	1992	2	1.000	\$11.34	\$2,097.90	•	
including loading, transportation,	100 00. yu.	411.0 1	1002	_	1.000	Ψ11.04	Ψ2,037.30		
and compaction)									
Seed, Fertilizer, Mulch	2.5 msf	\$44.00	1992	2	1.000	\$44.00	\$110.00		
otal Direct Capital Costs									\$115,034.65
CAPITAL COST - INDIRECT							-		
ingineering and Design (10 %)									614 500 47
egal and Administrative (4%)				1					\$11,503.47
				•					\$4,601.39
OTAL CAPITAL COSTS									\$131,139.50
CONTINGENCY (20%)									
OTAL PRESENT VALUE COST FO	DAGU EVANUATION								\$26,227.90 \$157,367.40

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE II-4, OPTION A PCB CONTAMINATED SOIL EXCAVATION AND OFF-SITE DISPOSAL AT A HAZARDOUS WASTE LANDFILL SCENARIO 2 SITE 08 - DPDO FILM PROCESSING DISPOSAL AREA

						1992	1992	Years	(1) Present
Item	Quantity Units	Unit Price	Basis Year	Reference	Escalation	Unit Costs	Costs	(O&M)	Value (O&M)
CAPITAL COST - DIRECT									
- Mob/Demob	1 time	\$345.00	1992	2	1.000	\$345.00	\$345.00		
-Excavation with Backhoe	11 cu. yd.	\$2.89	1992	2			\$31.79		
(2 1/2 cu. yd. bucket)	71 ou. yu.	Ψ2.00	1002	_	1.000	Ψ2.00	Ψ01.73		
Equipment Decontamination						*			
- Rental of Steam Cleaner	1 day	\$45.00	1992	2	1.000	\$45.00	\$45.00		
- Construction of Decon Pit	,	V .0.00	,,,,	_	11000	4 10.00	4 40.00		
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
- Polyethylene Tarpaulin	400 sq. ft.	\$0.32	1992	.2			\$128.00		
Treatment	•	·				*****	¥.120.00		
-Transport and Disposal of Excavated Soil to a Hazardous	17 tons	\$400.00	1992	21	1.000	\$400.00	\$6,800.00		
Waste Landfill					•		•		
Clean Common Earth Backfill	11 cu. yd.	\$11.34	1992	2	1.000	\$11.34	\$124.74		
(including loading, transportation,	.,,,	******		_		4.1.01	Ψ12 tiV 1		
and compaction)	•								
Total Direct Capital Costs	. <u></u>				· /- ·				\$7,518.63
CAPITAL COST - INDIRECT									
Engineering and Design (10 %)				1					\$751.86
Legal and Administrative (4%)				.1					\$300.75
TOTAL CAPITAL COSTS									\$8,571.24
CONTINGENCY (20%)									\$1,714.25
TOTAL PRESENT VALUE COST FOI	R SOIL EXCAVATION	I AND DISPOS	SAL						\$10,285.49

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE II-4, OPTION A PCB CONTAMINATED SOIL EXCAVATION AND OFF-SITE DISPOSAL AT A HAZARDOUS WASTE LANDFILL AND CAP SITE SCENARIO 3

SITE 08 - DPDO FILM PROCESSING DISPOSAL AREA

									(1)
ltem	Quantity Units	Unit Price	Basis Year F	Reference E	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	Presei Value (O&I
CAPITAL COST - DIRECT				,					
Soil Excavation									
- Mob/Demob	1 time	\$345.00	1992	2	1.000	\$345.00	\$345.00		
- Excavation with Backhoe	11 cu. yd.	\$2.89	1992	2	1.000	\$2.89	\$31.79		•
(2 1/2 cu. yd. bucket)									
Equipment Decontamination		4405.00	4000	_					
Rental of Steam Cleaner Construction of Decon Pit	2 weeks	\$135.00	1992	2	1.000	\$135.00	\$270.00		
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
Polyethylene Tarpaulin	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		
Dust Control	6 1	000000	4655	_	4 4				
– Water Tank Sprayer Freatment	2 weeks	\$660.00	1992	2	1.000	\$660.00	\$1,320.00		
- Transport and Disposal of	17 tons	\$400.00	1992	21	1.000	£400.0C	40.000.60		
Excavated Soil to a Hazardous Waste Landfill	17 tons	\$400.00	1992	21	1.000	\$400.00	\$6,800.00		
Clean Common Earth Backfill	11 cu. yd.	\$11.34	1992	2	1.000	\$11.34	\$124.74		
including loading, transportation,	va. ya.	Ψ11.0 1	IJJE	_	1.000	Ψ11.04	Ø124.74		
and compaction)									
Soil Cap									
- 18' Infiltration Layer	140 cu. yd.	\$13.00	1992	23	1.000	\$13.00	\$1,820.00		
- 6" Erosion Layer	280 sq. yd.	\$4.01	1992	2	1.000	\$4.01	\$1,122.80		
 Seed, Fertilizer, Mulch 	2.5 msf	\$44.00	1992	2	1.000	\$44.00	\$110.00		
Total Direct Capital Costs						·····			\$12,116.4
CAPITAL COST - INDIRECT									
Engineering and Design (10 %)				1					\$1,211.6
egal and Administrative (4%)				1				•	\$484.6
OTAL CAPITAL COSTS									\$13,812.7
PERATION AND MAINTENANCE COS	STS								
 Annual Inspection 	1 each	\$50.00	1988	3	1.119	\$55.95	\$55.95	` 30	\$860.0
- Repairs (per year)	1 each	\$100.00	1988	3	1.119	\$111.90	\$111.90	30	\$1,720.1
OTAL NET PRESENT VALUE OF O &	М								\$2,580.1
UBTOTAL COST									
ONTINGENCY (20%)									\$16,392.9
OTAL PRESENT VALUE COST FOR S	OL EXCAVATION,	DISPOSAL, AN	ND SOIL CAP						\$3,278.5 \$19,671.5
- Calculated based on 5% interest re	eto.								

ALTERNATIVE II-4, OPTION B SOIL EXCAVATION AND OFF-SITE INCINERATION SCENARIO 1 SITE 08 - DPDO FILM PROCESSING DISPOSAL AREA

ltem	Quantity Units	Unit Price	Basis Year	Reference E	Scalation	1992 Unit Costs	1992 Costs	Years (O&M)	Present Value (O&M
		.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,							2000 Orthodolauthatti Bartanidah
CAPITAL COST - DIRECT									
Mob/Demob	1 time	\$345.00	1992	2	1.000	\$345.00	\$345.00		
 Excavation with Backhoe 	185 cu. yd.	\$2.89	1992	2	1.000	\$2.89	\$534.65		
(2 1/2 cu. yd. bucket)						•			
Equipment Decontamination									
 Rental of Steam Cleaner 	2 weeks	\$135.00	1992	2	1.000	\$135.00	\$270.00		
 Construction of Decon Pit 									
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
Polyethylene Tarpaulin	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		
Dust Control							•		
 Water Tank Sprayer 	2 weeks	\$640.00	1992	2	1.000	\$640.00	\$1,280.00		
Treatment							•		
 Handling, Transport, and 									
Disposal of Excavated Soil to									
an Incinerator	278 tons	\$3,160.00	1992	22	1.000	\$3,160.00	\$878,480.00		
Clean Common Earth Backfill	185 cu. yd.	\$11.34	1992	2	1.000	\$11.34	\$2,097.90		
(including loading, transportation,	•					·	,,		
and compaction)									
Total Direct Capital Costs									\$883,179.65
CAPITAL COST - INDIRECT									
Engineering and Design (10 %)				1					\$88,317.97
Legal and Administrative (4%)				4					\$35,327.19
	·			•					φου, σ27.13
TOTAL CAPITAL COSTS									\$1,006,824.80
CONTINGENCY (20%)									\$201,364.96
TOTAL PRESENT VALUE COST FO	R SOIL EXCAVATION	AND INCINE	RATION						\$1,208,189.76

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE II-4, OPTION B PCB CONTAMINATED SOIL EXCAVATION AND OFF-SITE INCINERATION SCENARIO 2 SITE 08 - DPDO FILM PROCESSING DISPOSAL AREA

Item	Quantity Units	Unit Price	Basis Year	Reference E	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M)
•				****************					
CAPITAL COST - DIRECT									
– Mob/Demob	1 time	\$345.00	1992	2	1.000	\$345.00	\$345.00		
 Excavation with Backhoe 	11 cu. yd.	\$2.89	1992	2	1.000	\$2.89	\$31.79		
(2 1/2 cu. yd. bucket)									
Equipment Decontamination									
 Rental of Steam Cleaner 	1 day	\$45.00	1992	2	1.000	\$45.00	\$45.00		
 Construction of Decon Pit 									
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
Polyethylene Tarpaulin	400 sq. ft.	\$0.32	1992	. 2	1.000	\$0.32	\$128.00		
Treatment						•			
 Handling, Transport, and 	1								
Disposal of Excavated Soil to									
an Incinerator	17 tons	\$3,160.00	1992	22	1.000	\$3,160.00	\$53,720.00		
Clean Common Earth Backfill	11 cu. yd.	\$11.34	1992	2	1.000	\$11.34	\$124.74		
(including loading, transportation,									
and compaction)									
Total Direct Capital Costs		· · · · · · · · · · · · · · · · · · ·	·				···		\$54,438.63
CAPITAL COST - INDIRECT									
Engineering and Design (10 %)				1					\$5,443.86
Legal and Administrative (4%)				;					\$2,177.55
Logar and Administrative (476)				•					φ2,177.55
TOTAL CAPITAL COSTS									\$62,060.04
CONTINGENCY (20%)									610 410 04
TOTAL PRESENT VALUE COST FOR	D SUIL EXCVIVATION	A AND INCINE	PATION						\$12,412.01
TOTAL TRESENT VALUE COST FO	H GOIL ENGAVATION	A VIAD HACHAE	TATION						\$74,472.05

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE II-4, OPTION B PCB CONTAMINATED SOIL EXCAVATION AND OFF-SITE INCINERATION AND RCRA SUBTITLE D SOIL CAP SCENARIO 3

SITE 08 - DPDO FILM PROCESSING DISPOSAL AREA

Item	Quantity Units	Unit Price	Basis Year	Reference E	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M)
CAPITAL COST - DIRECT									
- Mob/Demob	1 time	\$345.00	1992	2	1.000	\$345.00	\$345.00		
 Excavation with Backhoe 	11 cu. yd.	\$2.89	1992	2	1.000	\$2.89	\$31.79		
(2 1/2 cu. yd. bucket)									
Equipment Decontamination									
- Rental of Steam Cleaner	2 weeks	\$135.00	1992	2	1.000	\$135.00	\$270.00		
- Construction of Decon Pit									
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
 Polyethylene Tarpaulin 	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		
Dust Control				_					
_ – Water Tank Sprayer	2 weeks	\$660.00	1992	2	1.000	\$660.00	\$1,320.00		
Treatment							•		
 Handling, Transport, and 									
Disposal of Excavated Soil to		_							
an Incinerator	17 tons	\$3,160.00	1992	22	1.000	\$3,160.00	\$53,720.00		
Clean Common Earth Backfill	11 cu. yd.	\$11.34	1992	2	1.000	\$11.34	\$124.74		
(including loading, transportation,									
and compaction)			•						
Сар									
- 18" Infiltration Layer	140 cu. yd.	\$13.00	1992	23	1.000	\$13.00	\$1,820.00		
- 6" Erosion Layer	280 sq. yd.	\$4.01	1992	2	1.000	\$4.01	\$1,122.80		
 Seed, Fertilizer, Mulch 	2.5 msf	\$44.00	1992	2	1.000	\$44.00	\$110.00		
Total Direct Capital Costs						***			\$59,036.43
CAPITAL COST - INDIRECT									-
Engineering and Design (10 %)				. 1					\$5,903.64
Legal and Administrative (4%)				1					\$2,361.46
TOTAL CAPITAL COSTS	,		······································						\$67,301.53
OPERATION AND MAINTENANCE	COSTS								
- Annual Inspection	1 each	\$50.00	1988	3	1.119	\$55.95	\$55.95	30	\$860.06
- Repairs (per year)	1 each	\$100.00	1988	3	1.119	\$111.90	\$111.90	30	\$1,720.13
									·
TOTAL NET PRESENT VALUE OF C) & M								\$2,580.19
SUBTOTAL COST									660 004 70
									\$69,881.72
CONTINGENCY (20%)	D COIL EVOAVATION	I INCINEDATIO	NI ANIO 041						\$13,976.34
TOTAL PRESENT VALUE COST FO	IN SUIL EXCAVATION	, INCINERATIO	IN, AND CAL	-					\$83,858.06

COST REFERENCES

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APPENDIX E

GROUP III SITES (SITES 12 AND 14)
PRELIMINARY COST ESTIMATES

ALTERNATIVE III-2 SITE ACCESS AND DEED RESTRICTIONS SITE 12 (BUILDING 316) and SITE 14 (BUILDING 38)

Item	Quantity Units	Unit Price	Basis Year	Reference Escalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1 Present Value (O&M
TOTAL CAPITAL COSTS								\$0.00
OPERATION AND MAINTENANCE COS	STS							
Site Access - Security Guard	1 year	\$29,120.00	1992	2 1.000	\$29,120.00	\$29,120.00	30	\$447,632.64
TOTAL NET PRESENT VALUE OF O &	M			· .				\$447,632.64
SUBTOTAL COST CONTINGENCY (20%)							2	\$447,632.64 \$89,526.53
TOTAL PRESENT VALUE COST FOR A	LTERNATIVE III -	2						\$537,159.17

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE III—3 SEALING SITE 12 (BUILDING 316) and SITE 14 (BUILDING 38) SCENARIO 1 (1 ppm)

									721
						1992	1992	Years	(1) Present
Item	Quantity Units	Unit Price	Basis Year	Reference E	scalation	Unit Costs	Costs	(O&M)	Value (O&M)
CAPITAL COSTS - DIRECT							· ·		
Floor Sealing			•						
Epoxy grout (1/4" thickness)	27,820 sq. ft.	\$6.65	1992	2	1.000	\$6.65	\$185,003.00		
Concrete (4" thickness)	344 cu. yd.	\$115.00	1992	. 2	1.000	\$115.00	\$39,560.00		
Health & Safety (17%)	•		,				\$38,175.71		
Confirmatory Sampling & Analysis (outside of sealed area)							•		
- Chip Sampling	10 samples	\$200.00	1991	5	1.046	\$209.20	\$2,092.00		
- Analysis (TCL Pest/PCB)	10 each	\$350.00	1992	10	1.000	\$350.00	\$3,500.00		
Soil Disposal	6 tons	\$72.00	1991	14	1.046	\$75.31	\$451.87		
Concrete Replacement (Site 12)		•							
(for previously removed areas)						. •			
- Concrete Paving (6" thickness)	47 sq. yd.	\$18.82	1992	2	1.000	\$18.82	\$884.54		
Asphalt Replacement (Site 14)						·			
(for previously removed areas)									
- Asphaltic Concrete Paving	78 sq. yd.	\$6.70	1992	2	1.000	\$6.70	\$522.60		
(2 1/2" thickness)	, , ,						, -		
Direct Capital Costs Subtotal							9		\$270,189.72
CAPITAL COSTS - INDIRECT							•		
Engineering (10%)				4		•			607.040.07
Legal and Administrative (4%)									\$27,018.97
Legar and Administrative (476)				· •					\$10,807.59
TOTAL CAPITAL COSTS									\$308,016.28
CONTINCENCY (COV)									
CONTINGENCY (20%) TOTAL PRESENT VALUE COST FOR AL	TERMATIVE III A AA								\$61,603.26
TOTAL PRESENT VALUE GOST FOR AL	TERNATIVE III = 3 SC	:-NAHI() 1							\$369,619.54

^{(1) -} Calculated based on a 5% interest rate.

ALTERNATIVE III—3 SEALING SITE 12 (BUILDING 316) and SITE 14 (BUILDING 38) SCENARIO 2 (10 ppm)

	_					1992	1992	Years	(1 Present
Item	Quantity Units	Unit Price	Basis Year	Reference E	scalation	Unit Costs	Costs	(O&M)	Value (O&M)
CAPITAL COSTS - DIRECT					-				
Floor Sealing									
Epoxy grout (1/4" thickness)	4,765 sq. ft.	\$6.65	1992	2	1.000	\$6.65	\$31,687.25		
Concrete (4" thickness)	59 cu. yd.	\$115.00	1992	2	1.000	\$115.00	\$6,785.00		
Health & Safety (17%)							\$6,540.28		
Confirmatory Sampling & Analysis (outside of sealed area)	•								
– Chip Sampling	10 samples	\$200.00	1991	5	1.046	\$209.20	\$2,092.00		
- Analysis (TCL Pest/PCB)	10 each	\$350.00	1992	10	1.000	\$350.00	\$3,500.00		
Concrete Replacement (Site 12)									٠
(for previously removed areas)									
- Concrete Paving (6" thickness)	47 sq. yd.	\$18.82	1992	2	1.000	\$18.82	\$884.54		
Asphalt Replacement (Site 14)									
(for previously removed areas)									
 Asphaltic Concrete Paving (2 1/2" thickness) 	78 sq. yd.	\$6.70	1992	2	1.000	\$6.70	\$522.60		
Direct Capital Costs Subtotal									\$52,011.67
CARITAL COOTS INDIDECT				··· -					
CAPITAL COSTS - INDIRECT		•					•		65 004 47
Engineering (10%) Legal and Administrative (4%)				1					\$5,201.17
Legal and Administrative (4%)				!					\$2,080.47
TOTAL CAPITAL COSTS									\$59,293.31
CONTINGENCY (20%)									\$11,858.66
TOTAL PRESENT VALUE COST FOR	ALTERNATIVE III_3 SC	ENARIO 2	•						\$71,151.97

^{(1) -} Calculated based on a 5% interest rate.

ALTERNATIVE III – 4 FLOOR AND SOIL REMOVAL WITH OFF-SITE DISPOSAL AT HAZARDOUS WASTE LANDFILL/OFF-SITE INCINERATION SITE 12 (BUILDING 316) and SITE 14 (BUILDING 38) SCENARIO 1 (1 ppm)

-									(1)
						1992	1992	Years	Present
Item	Quantity Units	Unit Price	Basis Year	Reference	Escalation	Unit Costs	Costs	(O&M)	Value (O&M)
CAPITAL COSTS - DIRECT		•							
Floor Demolition and Soli Excavation				•	:	•			
Floor Removal	380 cu. yd.	\$68.00	1992	.2	1.000	\$68.00	\$25,840.00		
Contaminated Soil Excavation	524 cu. yd.	\$11.90	1992	2	1.000	\$11.90	\$6,235.60		
Health & Safety (17%)							\$5,452.85		
Floor Disposal (Off-Site)				,					
Floor Material and Soil Disposal									
- Transport and Disposal of	1,540 tons	\$400.00	1992	21	1.000	\$400.00	\$616,000.00		
Material to TSCA-Approved Landfill									
Incineration									
Handling, Transport and Disposal of Excavated Concrete to an Incinerator	19 cu. yd.	\$3,160.00	1992	22	1.000	\$3,160.00	\$60,040.00		·
Health & Safety (17%)							\$114,926.80		
Confirmatory Sampling & Analysis							\$114,020.00		
- Chip Sampling	10 samples	\$200.00	1991	. 5	1.046	\$209.20	\$2,092.00		
- Soil Sampling	10 samples	\$200.00	1991	5	1.046	\$209.20	•	٠	
- Analysis (TCL Pest/PCB)	20 each	\$350.00	1992	10	1,000	\$350.00	• •		• ,
Clean Common Earth Backfill	541 cu. yd.	\$11.34	1992	2	1.000	\$11.34			
(Including Loading, Transportation	•	•	,			*	, - ,		
and Compaction)									
Concrete Replacement (Site 12)									
- Concrete Paving (6" thickness)	1,502 sq. yd.	\$18.82	1992	2	1.000	\$18.82	\$28,267.64		
Asphalt Replacement (Site 14)									
 Asphaltic Concrete Paving (2 1/2" thickness) 	1,712 sq. yd.	\$6.70	1992	2	1.000	\$6.70	\$11,470.40	,	
Direct Capital Costs Subtotal									\$885,552.23
							·		

ALTERNATIVE III-4

FLOOR AND SOIL REMOVAL WITH OFF-SITE DISPOSAL AT HAZARDOUS WASTE LANDFILL/OFF-SITE INCINERATION SITE 12 (BUILDING 316) and SITE 14 (BUILDING 38) SCENARIO 1 (1 ppm)

Continued)

Item	Quantity Units	Unit Price Basis Year Reference Escalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M)
CAPITAL COSTS – INDIRECT Engineering (10%) Legal and Administrative (4%)		1 1				\$88,555.22 \$35,422.09
TOTAL CAPITAL COSTS						\$1,009,529.54
CONTINGENCY (20%) TOTAL PRESENT VALUE COST FO	PR ALTERNATIVE III-4, SC	ENARIO 1			•	\$201,905.91 \$1,211,435.45

^{(1) -} Calculated based on a 5% interest rate.

ALTERNATIVE III – 4
FLOOR AND SOIL REMOVAL WITH OFF-SITE DISPOSAL AT HAZARDOUS WASTE LANDFILL/OFF-SITE INCINERATION
SITE 12 (BUILDING 316) and SITE 14 (BUILDING 38)
SCENARIO 2 (10 ppm)

					•			***************************************	
ltem	Ougality Unite	Link Brian	Bools Voss	Defenses	Facilities	1992	1992	Years	(1) Present
11011	Quantity Units	Unit Price	Basis Year	Reference	Escalation	Unit Costs	Costs	(O&M)	Value (O&M)
CAPITAL COSTS - DIRECT									
Floor Demolition and Soil Excavation	•				•				
Floor Removal	61 cu. yd.	\$68.00	1992	2	1.000	\$68.00	\$4,148.00		
Contaminated Soil Excavation	89 cu. yd.	\$11.90	1992	2	1.000	\$11.90	\$1,059.10		
Health & Safety (17%)					•		\$885.21		
Floor Disposal (Off-Site)									
Floor Material and Soil Disposal									
- Transport and Disposal of	255 tons	\$400.00	1992	21	1.000	\$400.00	\$102,000.00		
Materials to TSCA-Approved						¥	+		
Landfill									
Incineration	•	•							
 Handling, Transport and Disposal 	19 cu. yd.	\$3,160.00	1992	22	1.000	\$3,160.00	\$60,040.00		
of Excavated Concrete to	•					• •			
an Incinerator	•							_	
Health & Safety (17%)		•					\$27,546.80		
Confirmatory Sampling & Analysis									
 Chip Sampling 	10 samples	\$200.00	1991	5	1.046	\$209.20	\$2,092.00		
 Soil Sampling 	10 samples	\$200.00	1991	5	1.046	\$209.20	\$2,092.00		
Analysis (TCL Pest/PCB)	20 each	\$350.00	1992	10	1.000	\$350.00	\$7,000.00		
Clean Common Earth Backfill	110 cu. yd.	\$11.34	1992	. 2	1.000	\$11.34	\$1,247.40		
(Including Loading, Transportation									
and Compaction)									
Concrete Replacement (Site 12)									
 Concrete Paving (6" thickness) 	241 sq. yd.	\$18.82	1992	2	1.000	\$18.82	\$4,535.62		
Asphalt Replacement (Site 14)									
 Asphaltic Concrete Paving 	413 sq. yd.	\$6.70	1992	2	1.000	\$6.70	\$2,767.10		
(2 1/2" thickness)							• •		
Direct Capital Costs Subtotal		·							\$215,413,23

ALTERNATIVE III-4

FLOOR AND SOIL REMOVAL WITH OFF-SITE DISPOSAL AT HAZARDOUS WASTE LANDFILL/OFF-SITE INCINERATION SITE 12 (BUILDING 316) and SITE 14 (BUILDING 38) SCENARIO 2 (10 ppm)

(Continued)

Item	Quantity Units Unit Price Basis Year	Reference Escalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M)
CAPITAL COSTS – INDIRECT Engineering (10%) Legal and Administrative (4%)		1 1				\$21,541.32 \$8,616.53
TOTAL CAPITAL COSTS						\$245,571.08
CONTINGENCY (20%) TOTAL PRESENT VALUE COST FO	R ALTERNATIVE III-4, SCENARIO 2			·		\$49,114.22 \$294,685.29

^{(1) -} Calculated based on a 5% interest rate.

ALTERNATIVE III-5 SOLVENT WASHING SITE 12 (BUILDING 316) ONLY SCENARIO 1 (1 ppm)

lltem	Quantity Units	Unit Price	Basis Year	Reference	Escalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1 Present Value (O&M
CAPITAL COSTS - DIRECT				· ·			•		
Solvent Washing (Floor)								,	
Floor	1 L.S.	\$30,000.00	1992	26	1.000	\$30,000.00	\$30,000.00		
Health & Safety (17%)		·	•			• •	\$5,100.00		•
Confirmatory Sampling & Analysis			•				•		
Chip Sampling	10 samples	\$200.00	1991	5	1.046	\$209.20	\$2,092.00	•	
Analysis (TCL Pest/PCB)	10 each	\$350.00	1992	10	1.000	\$350.00	\$3,500.00		
Disposal of Spent Solvent									
- Transportation	1 load	\$550.00	1991	11	1.046	\$575.30	\$575.30		
- Treatment	28 drums	\$240.00	1991	11	1.046	\$251.04	\$7,029.12		
Health & Safety (17%)				•			\$1,292.75		
Concrete Replacement (Site 12)		٠							
(for previously removed areas)									
- Concrete Paving (6" thickness)	47 sq. yd.	\$18.82	1992	2	1.000	\$18.82	\$884.54		•
Direct Capital Costs Subtotal						•	•		<u>\$50,473.71</u>
									Ψ30,473.7
CAPITAL COSTS - INDIRECT				•			•		
Engineering (10%)			1	1					\$5,047.37
Legal and Administrative (4%)		•		1				•	\$2,018.95
OTAL CAPITAL COSTS			 						\$57,540.03
CONTINGENCY (20%)									\$11,508.01
TOTAL PRESENT VALUE COST FOR	ALTERNATIVE III-5, S	CENARIO 1				•			\$69,048.04

^{(1) -} Calculated based on a 5% interest rate.

ALTERNATIVE III-5 SOLVENT WASHING SITE 12 (BUILDING 316) ONLY SCENARIO 2 (10 ppm)

	0	t In la Palma	Peole Voor	Reference	Escalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M)
Item	Quantity Units	Unit Price	Basis Year	Hererence	ESCAIAIIUI	Utili Gosis	00313	<u>(Cam)</u>	NACCO (CAID)
CAPITAL COSTS - DIRECT									
Solvent Washing (Floor)					•				
Floor	1 L.S.	\$6,000.00	1992	26	1.000	\$6,000.00	\$6,000.00		
Health & Safety (17%)							\$1,020.00		
Confirmatory Sampling & Analysis									
- Chip Sampling	10 samples	\$200.00	1991	. 5	1.046	\$209.20	\$2,092.00		
- Analysis (TCL Pest/PCB)	10 each	\$350.00	1992	10	1.000	\$350.00	\$3,500.00		
Disposal of Spent Solvent				,				•	
 Transportation 	1 load	\$375.00	1991	11		\$392.25	\$392.25		
- Treatment	4 drums	\$240.00	1991	11	1.046	\$251.04	\$1,004.16		
Health & Safety (17%)							\$237.39		
Concrete Replacement (Site 12)	•								
(for previously removed areas)									
- Concrete Paving (6" thickness)	47 sq. yd.	\$18.82	1992	2	1.000	\$18.82	\$884.54		
Direct Capital Costs Subtotal							 		\$15,130.34
CAPITAL COSTS - INDIRECT									
Engineering (10%)				1		*			\$1,513.03
Legal and Administrative (4%)	•			1					\$605.21
TOTAL CAPITAL COSTS									\$17,248.59
									00 440 74
CONTINGENCY (20%)					-				\$3,449.72
TOTAL PRESENT VALUE COST FO	OR ALTERNATIVE III-5, S	SCENARIO 2		•				•	\$20,698.30
									

^{(1) -} Calculated based on a 5% interest rate.

COST REFERENCES

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- 12. Remedial Action at Waste Disposal Sites; October 1985; EPA/625/6-85/006.
- 13. Personal Communication; DuPont Environmental Treatment; September 1992.
- 14. Personal Communication; American Waste Services; September 1992.
- Geraghty & Miller, Inc.; December 1991.
- 16. Personal Communication; Burlington Environmental; September 1992.
- 17. TRC Environmental Corporation; September 1992.
- 18. U.S. Environmental Engineering; September 1992.
- 19. Delta Cooling Towers, Inc.; September 1992.
- 20. Compuchem Analytical Laboratories, November 1991.
- 21. Personal Communication; Envirosafe Services of America, Inc.; July 1992.
- 22. Rollins Environmental; September 1992.
- 23. TRC Environmental Corporation; October 1992.
- 24. VISITT Version 1.0; Vendor Information System for Innovative Treatment Technologies, EPA/542/R-92/001, June 1992.
- 25. Palmer, S.A.K., et al., 1988. <u>Metal/Cyanide Containing Wastes Treatment Technologies</u>, Noyes Data Corporation.
- 26. Personal Communication; ENPRO Environmental Professionals, Inc., December 18, 1992.
- 27. EmTech Environmental Services, Inc. November 1991.

APPENDIX F

GROUP VI SITES (SITE 10)
PRELIMINARY COST ESTIMATES

ALTERNATIVE VI-1 ONE-TIME GROUND WATER MONITORING AT THE END OF 5 YEARS SITE 10 - CAMP FOGARTY

tem	Quantity Units	Unit Price	Basis Year F	Reference E	ecalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M)
	Quality Office	Omit ince	Dasis I d ai i	JOIOTOLICO E	Scalalion	OIII OOSIS	COSIS	(Odivi)	Value (Calvi)
TOTAL CAPITAL COSTS					· · · · · · · · · · · · · · · · · · ·				\$0.00
OPERATION AND MAINTENANCE COS	STS								
Ground Water Monitoring									
including trip blanks, field blanks and	duplicate samples)						•		
 Sampling at end of 5 years Analysis: 	5 samples	\$200.00	1991	5	1.046	\$209.20	\$1,046.00		\$1,046.00
TAL + cyanide	6 samples	\$390.00	1992	10	1.000	\$390.00	\$2,340.00	•	\$2,340.00
 Report Preparation 	1 each	\$14,000.00	1992	17	1.000	\$14,000.00	\$14,000.00		\$14,000.00
OTAL NET PRESENT VALUE OF O &	M								\$17,386.00
SUBTOTAL COST			,				,		\$17,386.00
CONTINGENCY (20%)								•	\$3,477.20
OTAL PRESENT VALUE COST FOR G	ROUND WATER M	ONITORING A	AT THE END OF	FIVE YEAR	is				\$20,863.20

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE VI-2 GROUND WATER MONITORING FOR 30 YEARS, DEED RESTRICTIONS, AND FENCING SITE 10 -CAMP FOGARTY

Item	Quantity Units	Unit Price	Basis Year I	Reference E	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	1) Present Value (O&M
0.10:T.1: 0.00.T. D.10:T.0.T.									•
CAPITAL COST - DIRECT						•			
Fencing Chain Link O source wire	4000 4	649.50	1000	•	4.000	640.50	000 450 00	•	•
 Chain Link, 9 gauge wire, aluminized steel, 6' high 	4900 I. ft.	\$13.50	1992	2	1.000	\$13.50	\$66,150.00		
- Gate (12-ft wide)	1 each	\$720.00	1992	2	1.000	\$720.00	\$720.00		-
- Warning Signs	49 each	\$42.00	1992	2	1.000	\$120.00 \$42.00	\$7,20.00 \$2,058.00		
Walling Olgrio	45 04011	Ψ+2.00	1332	۷ .	1.000	Ψ72.00	φ2,000.00		
Direct Capital Cost									\$68,928.00
CAPITAL COSTS - INDIRECT									
Engineering and Design (10%)	•			1			\$6,892.80		
Legal and Administrative (4%)	•			1			\$2,757.12		
3				•			V2,. 072		
Indirect Capital Cost Total	•								\$9,649.9
TOTAL CAPITAL COSTS		:							\$78,577.92
OPERATION AND MAINTENANCE (COSTS	÷		· · · · ·					
Ground Water Monitoring (including trip blanks, field blanks a	nd duplicate samples)				ر				
Ground Water Monitoring (including trip blanks, field blanks a		\$200.00	1991	5	1.046	\$209.20	\$1.046.00	30	\$16 079 11
Ground Water Monitoring (including trip blanks, field blanks at — Sampling	nd duplicate samples) 5 samples	\$200.00	1991	5	1.046	\$209.20	\$1,046.00	30	\$16,079.1°
Ground Water Monitoring (including trip blanks, field blanks a		\$200.00 \$390.00	1991	5	1.046 1.000	·			
Ground Water Monitoring (including trip blanks, field blanks at - Sampling - Analysis:	5 samples					\$209.20 \$390.00 \$14,000.00	\$1,046.00 \$2,340.00 \$14,000.00	30 30 30	\$35,970.48
Ground Water Monitoring (including trip blanks, field blanks at - Sampling - Analysis: TAL + cyanide	5 samples	\$390.00	1992	10	1.000	\$390.00	\$2,340.00	30	\$35,970.48 \$215,208.00
Ground Water Monitoring (including trip blanks, field blanks at - Sampling - Analysis: TAL + cyanide - Report Preparation Site Fence Maintenance ANNUAL O & M COST	5 samples 6 samples 1 each 1 each	\$390.00 \$14,000.00	1992 1992	10 17	1.000 1.000	\$390.00 \$14,000.00	\$2,340.00 \$14,000.00	30 30	\$16,079.11 \$35,970.48 \$215,208.00 <u>\$3,440.25</u>
Ground Water Monitoring (including trip blanks, field blanks at - Sampling - Analysis: TAL + cyanide - Report Preparation	5 samples 6 samples 1 each 1 each	\$390.00 \$14,000.00	1992 1992	10 17	1.000 1.000	\$390.00 \$14,000.00	\$2,340.00 \$14,000.00 <u>\$223.80</u>	30 30	\$35,970.48 \$215,208.00
Ground Water Monitoring (including trip blanks, field blanks at - Sampling - Analysis: TAL + cyanide - Report Preparation Site Fence Maintenance ANNUAL O & M COST TOTAL NET PRESENT VALUE OF O	5 samples 6 samples 1 each 1 each	\$390.00 \$14,000.00	1992 1992	10 17	1.000 1.000	\$390.00 \$14,000.00	\$2,340.00 \$14,000.00 <u>\$223.80</u>	30 30	\$35,970.44 \$215,208.00 <u>\$3,440.25</u> \$270,697.85
Ground Water Monitoring (including trip blanks, field blanks at - Sampling - Analysis: TAL + cyanide - Report Preparation Site Fence Maintenance ANNUAL O & M COST	5 samples 6 samples 1 each 1 each	\$390.00 \$14,000.00	1992 1992	10 17	1.000 1.000	\$390.00 \$14,000.00	\$2,340.00 \$14,000.00 <u>\$223.80</u>	30 30	\$35,970.48 \$215,208.00 <u>\$3,440.25</u>

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE VI-3, OPTION A RCRA SUBTITLE D SOIL CAP SITE 10 - CAMP FOGARTY

									(1)
Item	O				_	1992	1992	Years	Present
1011	Quantity Units	Unit Price	Basis Year	Reference	Escalation	Unit Costs	Costs	(O&M)	Value (O&M)
CAPITAL COST - DIRECT							•		
Site Preparation				•					
- Debris Removal/Characterization	180 tons	\$200.00	1992	. 2	1.000	\$200.00	\$36,000.00		
- Debris Transportation and	180 tons	\$350.00	1992	2	1.000	\$350.00	\$63,000.00		
Disposal	•	•	• • •	_		V 000.00	400,000.00	•	
- Clear Vegetation and Brush	25 acres	\$3,825.00	1992	2	1.000	\$3,825.00	\$95,625.00		
- Regrade Site	80,000 cu. yd.	\$3.40	1992	2	1.000	\$3.40	\$272,000.00		-
Cap	•					******		,	
- 18" Infiltration Layer	61,000 cu. yd.	\$13.00	1992	23	1.000	\$13.00	\$793,000.00		
- 6" Erosion Layer	120,000 sq. yd.	\$4.01	1992	2	1.000	\$4.01	\$481,200.00		
 Seed, Fertilizer, Mulch 	1100 msf	\$44.00	1992	2	1.000	\$44.00	\$48,400.00		
- Health & Safety (17%)						• • • • • • • • • • • • • • • • • • • •	\$224,842.00		
Equipment Decontamination				•			4- <u>-</u> 1,0 1100		
- Rental of Steam Cleaner	2 months	\$400.00	1992	2	1.000	\$400.00	\$800.00		
- Construction of Decon Pit						* / / 3 3 1 3 3	4000.00		
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
- Polyethylene Tarpaulin	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		i
- Disposal (Tanker Truck)	1 each	\$1,600.00	1992	13	1.000	\$1,600.00	\$1,600.00		
Dust Control						4.,000.00	41,000.00		
– Water Tank Sprayer	2 months	\$1,975.00	1992	2	1.000	\$1,975.00	\$3,950.00		
Total Direct Capital Cost		···						•	\$2,020,589.10
				-					
CAPITAL COST - INDIRECT									
Engineering and Design (10 %)				1	•				\$202,058.91
Legal and Administrative (4%)				1					\$80,823.56
TOTAL CAPITAL COSTS									\$2,303,471.57

ALTERNATIVE VI-3, OPTION A RCRA SUBTITLE D SOIL CAP SITE 10 - CAMP FOGARTY (Continued)

ltem	Quantity Units	Unit Price	Basis Year	Reference E	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1 Present Value (O&M
OPERATION AND MAINTENANCE CO	QTQ .								
Cap O & M	<u>010</u>					. · ·			
- Annual Inspection	1 each	\$500.00	1988	3	1.119	\$559.50	\$559.50	30	\$8,600.6
- Repairs (per year)	1 each	\$1,000.00	1988	3	1.119	\$1,119.00	\$1,119.00	30	\$17,201.2
Ground Water Monitoring	1 00011	4 1,000.00	1000	, .	1.110	Ψ1,110.00	Ψ1,115.00	. 00	Ψ17,201.2
(including trip blanks, field blanks and	duplicate samples)							
- Sampling	5 samples	\$200.00	1991	5	1.046	\$209.20	\$1,046.00	30	\$16,079.1
Analysis:									
TAL + cyanide	6 samples	\$390.00	1992	10	1.000	\$390.00	\$2,340.00	30	\$35,970.48
 Report Preparation 	1 each	\$14,000.00	1992	17.	1.000	\$14,000.00	\$14,000.00	30	\$215,208.00
ANNUAL O&M COST							\$19,064.50		
TOTAL NET PRESENT VALUE OF O &	<u>M</u>		·						\$293,059.49
SUBTOTAL COST		•							#0 F00 F04 0
CONTINGENCY (20%)									\$2,596,531.07
00111111011 (20%)									\$519,306.2 1
TOTAL PRESENT VALUE COST FOR F	RCRA SUBTITLE D	SOIL CAP	•						\$3,115,837.28

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE VI-3 - CONTAINMENT, OPTION B RCRA SUBTITLE D SOIL CAP WITH SLURRY WALL SITE 10 - CAMP FOGARTY

						1992	1992	Years	(1) Present
Item	Quantity Units	Unit Price	Basis Year	Ref.	Escalation	Unit Costs	Costs	(O&M)	Value (O&M
CAPITAL COST - DIRECT									
Site Preparation									
Debris Removal/Characterization	180 tons	\$200.00	1992	2	1.000	\$200.00	\$36,000.00		
Debris Transportation and	180 tons	\$350.00	1992	2		\$350.00	\$63,000.00		
Disposal	100 10113	Ψ000.00	1332	-	1.000	φ330.00	\$00,000.00		
Clear Vegetation and Brush	25 acres	\$3,825.00	1992	2	1.000	\$3,825.00	\$95,625.00		
- Regrade Site	80,000 cu. yd.	\$3.40	1992	2		\$3,023.00	\$272,000.00		
Slurry Wall Construction	00,000 oa. ya.	. 40.40	1092		1.000	ψ0.40	Ψ212,000.0 Ų		
(1400 ft x 3 ft x 45 ft)									
- Mob/Demob	1 time	\$500.00	1992	2	1.000	\$500.00	\$500.00		•
- 1 1/2 cu. yd. Hydraulic Backhoe	7,000 cu. yd.	\$3.74	1992	2		\$3.74	\$26,180.00		
- Bulldozer (300 hp)	7,000 cu. yd.	\$3.35	1992	2		\$3.35	\$23,450.00		
- Health & Safety (17%)	.,	40.00	.002	_	1.000	Ψ0.00	\$8,522.10		
- Soil /Bentonite Trench	4,200 sq. ft.	\$8.00	1984	15	1.219	\$9.75	\$40,958.40		
- Water Tank Rental	3 months	\$105.00	1992	2		\$105.00	\$315.00		
- Pumping/Mixing Equipment	3 months	\$8,250.00	1992	2		\$8,250.00	\$24,750.00		•
Cap				•	.,,,,,,	4 -, 2 -5.55	42.11.00.00		
- 18" Infiltration Layer	61,000 cu. yd.	\$13.00	1992	23	1.000	\$13.00	\$793,000.00		
- 6" Erosion Layer	120,000 sq. yd.	\$4.01	1992	. 2		\$4.01	\$481,200.00		
- Seed, Fertilizer, Mulch	1,100 msf	\$44.00	1992	2		\$44.00	\$48,400.00		
Health & Safety (17%)		·				• • •	\$325,363.09		•
Equipment Decontamination							, ,		
- Rental of Steam Cleaner	3 months	\$400.00	1992	2	1.000	\$400.00	\$1,200.00		
 Construction of Decon Pit 		•					, .,		
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
 Polyethylene Tarpaulin 	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		
- Disposal (Tanker Truck)	1 each	\$1,600.00	1992	13	1.000	\$1,600.00	\$1,600.00		
Site Trailer	3 months	\$450.00	1992	2	1.000	\$450.00	\$1,350.00		
Dust Control							. ,		
 Water Tank Sprayer 	3 months	\$1,975.00	1992	2	1.000	\$1,975.00	\$5,925.00		
Piezometer Installation				•		•			
Mob/Demob	1 time	\$1,000.00	1992	16	1.000	\$1,000.00	\$1,000.00		
3 Borings/Piezometers	1 l. sum	\$4,420.00	1992	16	1.000	\$4,420.00	\$4,420.00		
Health & Safety (17%)							\$751.40		
Total Direct Capital Cost	•								\$2,255,682.09

ALTERNATIVE VI-3 - CONTAINMENT, OPTION B RCRA SUBTITLE D SOIL CAP WITH SLURRY WALL SITE 10 - CAMP FOGARTY (Continued)

ltem	Quantity Units	Unit Price	Basis Year I	Ref. E	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M)
CAPITAL COST - INDIRECT								•	\$225,568.21
Engineering and Design (10 %) Legal and Administrative (4%)				1					\$90,227.28
TOTAL CAPITAL COSTS									\$2,571,477.58
OPERATION AND MAINTENANCE C	<u>osts</u>								
Сар			ভ ্						
Annual Inspection	1 each	\$500.00	1988	3	1.119	\$559.50	\$559.50	30	\$8,600.63
-Repairs (per year)	1 each	\$1,000.00	1988	3	1.119	\$1,119.00	\$1,119.00	30	\$17,201.27
Annual Slurry Wall	80 hours	\$100.00	1989	9	1.098	\$109.80	\$8,784.00	30	\$135,027.65
– Maintenance/Monitoring									
Ground Water Monitoring									
(including trip blanks, field blanks and	d duplicate samples)						•		
Sampling Analysis:	5 samples	\$200.00	1991	5	1.046	\$209.20	\$1,046.00	30	\$16,079.11
TAL + cyanide	6 samples	\$390.00	1992	10	1.000	\$390.00	\$2,340.00	. 30	\$35,970.48
 Report Preparation 	1 each	\$14,000.00	1992	17	1.000	\$14,000.00	\$14,000.00	30	\$215,208.00
ANNUAL O&M COST							\$27,848.50		
TOTAL NET PRESENT VALUE OF O	& M								\$428,087.14
SUBTOTAL COST						•			\$2,999,564.72
CONTINGENCY (20%)							,		\$599,912.94
TOTAL PRESENT VALUE COST FOR	RCRA SUBTITLE D	SOIL CAP W	TH SLURRY W	ALL_					\$3,599,477.66

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE VI-4, SOIL TREATMENT - OPTION A SOIL EXCAVATION AND OFF-SITE DISPOSAL AT NON-HAZARDOUS WASTE LANDFILL SITE 10 - CAMP FOGARTY

ltem	Quantity Units	Unit Price	Basis Year	Reference E	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1 Present Value (O&M
CAPITAL COST - DIRECT									
Site Preparation									
- Debris Removal/Characterization	180 tons	\$200.00	1992	2	1.000	\$200.00	\$36,000.00		
 Debris Transportation and Disposal 	180 tons	\$350.00	1992	2	1.000	\$350.00	\$63,000.00		
 Clear Vegetation and Brush 	25 acres	\$3,825.00	1992	2	1.000	\$3,825.00	\$95,625.00		
Excavation					•				•
Mob/D em ob	1 time	\$345.00	1992	2	1.000	\$345.00	\$345.00		
 Excavation with Backhoe (2 1/2 cu. yd. bucket) 	80,000 cu. yd.	\$2.89	1992	2	1.000	\$2.89	\$231,200.00		
- Health & Safety (17%) Equipment Decontamination							\$39,304.00		
Rental of Steam Cleaner Construction of Decon Pit	2 months	\$400.00	1992	2	1.000	\$400.00	\$800.00		
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
 Polyethylene Tarpaulin 	400 sq. ft.	\$0.32	1992	2 .	1.000	\$0.32	\$128.00		
Dust Control	•								•
 Water Tank Sprayer 	2 months	\$1,975.00	1992	2	1.000	\$1,975.00	\$3,950.00		
Treatment									
 Transport and Disposal of Excavated Soil to Non – Hazardous Waste Landfill 	108,000 tons	\$72.00	1991	- 14	1.046	\$75.31	\$8,133,696.00		
Clean Common Earth Backfill	80,000 cu. yd.	\$11.34	1992	2	1.000	\$11.34	\$907,200.00		
(including loading, transportation,	,	•				•		•	
and compaction)									
Seed, Fertilizer, Mulch	1,080 msf	\$44.00	1992	2	1.000	\$44.00	\$47,520.00		
Total Direct Capital Costs									\$9,558,812.10
CAPITAL COST INDIRECT	,						,		-
Engineering and Design (10 %)				1 .					\$955,881.2
Legal and Administrative (4%)			·	1					\$382,352.48
TOTAL CAPITAL COSTS									310,897,045.79
CONTINGENCY (20%)								•	\$2,179,409.16

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE VI-4, SOIL TREATMENT - OPTION B SOIL EXCAVATION AND ON-SITE SOIL WASHING SITE 10 - CAMP FOGARTY

	_					1992	1992	Years	(1) Present
Item	Quantity Units	Unit Price	Basis Year	Reference E	scalation	Unit Costs	Costs	(O&M)	Value (O&M)
CAPITAL COST - DIRECT			•					4	
Site Preparation			•			•			
- Debris Removal/Characterization	180 tons	\$200.00	1992	2	1.000	\$200.00	\$36,000.00		
- Debris Transportation and	180 tons	\$350.00	1992	2	1.000	\$350.00	\$63,000.00		
Disposal	100 10113	Ψ050.00	1992	2	1.000	φ35U.UU	\$63,000.00		
- Clear Vegetation and Brush	25 acres	\$3,825.00	1992	2	1.000	\$3,825.00	\$95,625.00		
Excavation	20 acres	Ψ3,025.00	1992		1.000	φ3,023.00	\$95,625.00		
- Mob/Demob	1 time	\$345.00	1992	~ 2	1.000	\$345.00	\$345.00		
- Excavation with Backhoe	80,000 cu. yd.	\$2.89	1992	2	1.000	\$2.89	\$231,200.00		
(2 1/2 cu. yd. bucket)	00,000 ou. yu.	Ψ2.03	1332	2	1.000	Ψ2.03	\$231,200.00		
- Health & Safety (17%)					4		\$39,304.00		
Equipment Decontamination	•						φ33,304.00		
- Rental of Steam Cleaner	3 months	\$400.00	1992	2	1.000	\$400.00	\$1,200.00		
- Construction of Decon Pit	o monuto	Ψ+00,00	1002	_	1.000	ψ+00.00	Ψ1,200.00		
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10		
- Polyethylene Tarpaulin	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		
Dust Control	100 04.16.	40.02	1002	_	1.000	Ψ0.02	ψ120.00		
- Water Tank Sprayer	3 months	\$1,975.00	1992	2	1.000	\$1,975.00	\$5,925.00		
Treatment		41,070.00	1002	-	1.000	Ψ1,570.00	Ψ0,520.00		
- Soil Washing Unit (All Inclusive)	80,000 cu.yd	\$200.00	1991	15	1.046	\$209.20	\$16,736,000.00		
- TCLP Analysis of Treated Soil	10 ea.	\$1,400.00	1991	5	1.046	\$1,464.40	\$14,644.00		
Filter Cake and Residual Disposal	5,400 ton	\$200.00	1991	14	1.046	\$209.20	\$1,129,680.00		
(assume hazardous)		4 _00.00	,,,,,	• •	1.010	4200.20	\$1,120,000,00		
Placement of Washed Soil	76,000 cu.yd	\$1.34	1992	2	1.000	\$1.34	\$101,840.00		
Seed, Fertilizer, Mulch	1,080 msf	\$44.00	1992	2	1.000	\$44.00	\$47,520.00		
Total Direct Capital Costs	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	4			.,,,,,	4 1 1.00	V17,020.00	•	\$18,502,455.10
									¥10,002,700.10
CAPITAL COST - INDIRECT				•					
Engineering and Design (15 %)				1					\$2,775,368.27
Legal and Administrative (5%)				1					\$925,122.76
				•		•			4020,122.70
TOTAL CAPITAL COSTS									\$22,202,946.12
CONTINGENCY (20%)									\$4,440,589.22
TOTAL PRESENT VALUE COST FOR	SOIL EXCAVATION	AND SOIL W	ASHING					;	\$26,643,535.34
				·					
(1) Colouist Passed on FO Interes									

^{(1) -} Calculate pased on 5% interest rate.

ALTERNATIVE VI-4, STREATMENT - OPTION C SOIL EXCAVATION AND STABILIZATION/SOLIDIFICATION SITE 10 - CAMP FOGARTY

Item	Quantity Units	Unit Price	Basis Year	Reference E	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	Present Value (O&M
CAPITAL COST - DIRECT	**			•					
Site Preparation	4								
- Debris Removal/Characterization	180 tons	\$200.00	1992	. 2	1.000	\$200.00	\$36,000.00		
 Debris Transportation and Disposal 	180 tons	\$350.00	1992	2	1.000	\$350.00	\$63,000.00		
- Clear Vegetation and Brush	25 acres	\$3,825.00	1992	2	1.000	\$3,825.00	\$95,625.00		
Excavation		4-,		_		, , ,	, ,		
- Mob/Demob	1 time	\$345.00	1992	2	1.000	\$345.00	\$345.00		
- Excavation with Backhoe	80,000 cu. yd.	\$2.89	1992	2	1.000	\$2.89	\$231,200.00		
(2 1/2 cu. yd. bucket)	00,000 00, 32.	42.00		_		4 2.55	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		
- Health & Safety (17%)	•				•		\$39,304.00	•	
Equipment Decontamination	•						\$00,00 00		
- Rental of Steam Cleaner	3 months	\$400.00	1992	2	1.000	\$400.00	\$1,200.00		
 Construction of Decon Pit 		•		_		,	4 .,======		
Excavate Pit	15 cu. yd.	\$2.94	1992	2	1.000	\$2.94	\$44.10	•	
 Polyethylene Tarpaulin 	400 sq. ft.	\$0.32	1992	2	1.000	\$0.32	\$128.00		
Dust Control		•				•	•		
- Water Tank Sprayer	3 months	\$1,975.00	1992	2	1.000	\$1,975.00	\$5,925.00		
Treatment			-						
Mob/Demob	1 time	\$100,000.00	1992	17	1.000	\$100,000.00	\$100,000.00		
 Stabilization 	120,000 tons	\$200.00	1991	27	1.046	\$209.20	\$25,104,000.00		
 TCLP Analysis of Treated Soil 	10 each	\$1,400.00	1991	5	1.046	\$1,464.40	\$14,644.00		
Stabilized Soil Disposal									
 Excavate/Grade Disposal Area 	113,000 cu.yd	\$2.48	1992	2	1.000	\$2.48	\$280,240.00		
 4 ft of Sand Material 	45,000 cu.yd	\$22.00	1992	2	1.000	. \$22.00	\$990,000.00		
 2 60 mil HDPE Liner Layers 	610,000 sq.ft	\$1.10	1991	5	1.046	\$1.15	\$701,866.00	•	
 Placement of Stabilized Soil 	88,000 cu.yd	\$1.34	1992	2	1.000	\$1.34	\$117,920.00		
- 3 ft Clean Soil	34,000 cu.yd	\$1.34	1992	2	1.000	\$1.34	\$45,560.00		
1 ft of Topsoil	11,000 cu.yd	\$12.93	1992	2	1.000	\$12.93	\$142,230.00		
 Seed, Fertilizer, Mulch 	305 msf	\$44.00	1992	2	1.000	\$44.00	\$13,420.00		
Total Direct Capital Costs					,				\$27,982,651.1
CAPITAL COST - INDIRECT							•		
Engineering and Design (15 %)	•			1					\$4,197,397.6
Legal and Administrative (5%)				1				-	\$1,399,132.5
TOTAL CAPITAL COSTS									\$33,579,181.3
CONTINGENCY (20%) TOTAL PRESENT VALUE COST FOR	SOIL EXCAVATION	AND STABILIZ	ATION/SOLIE	DIFICATION					\$6,715,836.26 \$40,295,017.58

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE VI-4, GROUND WATER EXTRACTION OPTION D MULTI-WELL EXTRACTION SITE 10 - CAMP FOGARTY

Item	Quantity Units	Unit Price	Basis Year	Reference	Escalation	1992 Unit Costs		Years O&M)	(1) Present Value (O&M)
CAPITAL COSTS - DIRECT								<i>30m</i>	value (Odin)
Ground Water Extraction									
-Well Construction and Materials						•			
(17 45-ft. shallow overburden - 6")	17 ea	\$8,919.31	1992	6	1.000	\$8,919.31	\$151,628.27	٠	
-Submersible Pumps	17 ea	\$305.00	1992	2		\$305.00	\$5,185.00	•	
- Mobilization/Demobilization	1 ea	\$10,000.00	1992	. 6		\$10,000.00	\$10,000.00	,	
-Standby Time	60 hr	\$175.00	1992	6		\$175.00	\$10,500.00		
-Conveyance Piping and Appurtenances	700 l.ft.	\$5.50	1991	5	1.027	\$5.65	\$3,953.95		
-Excavation and Backfill	260 cu. yd	\$3.69	1992	2	1.000	\$3.69	\$959.40		
-Bedding Sand	50 cu. yd	\$24.00	1992	. 2	1.000	\$24.00	\$1,200.00		
Direct Capital Cost Total				<u> </u>	•				\$183,426.62
CAPITAL COSTS - INDIRECT				•		-			
Engineering and Design(10%)				1					\$18,342.66
Legal and Administrative(4%)				1		·			\$7,337.06
TOTAL CAPITAL COSTS									\$209,106.35
CONTINGENCY(20%)									\$41,821.27
TOTAL PRESENT VALUE COST FOR ALTER	RNATIVE VI-4 - OP	TION D (MULTI	-WELL EX	KTRACTION)					\$250,927.62

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE VI-4, GROUND WATER EXTRACTION - OPTION D EXTRACTION OF GROUND WATER VIA INTERCEPTOR TRENCH SITE 10 - CAMP FOGARTY

	Overette Helte	I I nie Dvina	Basis Vess	Reference	Engalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M)
Item	Quantity Units	Unit Price	Basis Year	Reference	ESCAIALION	Unit Costs	CUSIS	(Oalvi)	value (Oalvi)
CAPITAL COST - DIRECT									•
Ground Water Extraction Trench									
-Excavation and Backfill	· 1200 cu. yd.	\$3.69	1992	2	1.000	\$3.69	\$4,428.00		
-Bedding Sand	100 cu. yd.	\$24.00	1992	2	1.000	\$24.00	\$2,400.00		
-1/2" Crushed Stone	100 cu. yd.	\$18.83	1992	2	1.000	\$18.83	\$1,883.00		
-4" O.D. Slotted HDPE	330 l. ft.	\$8.10	1992	2	1.000	\$8.10	\$2,673.00		•
-Submersible Pumps	3 each	\$620.00	1992	2	1.000	\$620.00	\$1,860.00		
-Pre-Cast Concrete Manhole	3 each	\$4,195.00	1992	2	1.000	\$4,195.00	\$12,585.00		
Pipe Trench from Manhole to	•								
Treatment Area								•	-
 1 1/4" O.D. Non-Slotted HDPE Pipe 	400 l. ft.	\$2.59	1992	2	1.000	\$2.59	\$1,036.00 ·		·
-Excavation and Backfill	150 cu. yd.	\$3.69	1992	2	1.000	\$3.69	\$553.50		
-Bedding Sand	30 cu. yd.	\$24.00	1992	2	1.000	\$24.00	\$720.00		
Total Direct Capital Cost							W-1,0-4,		\$28,138.50
CAPITAL COST - INDIRECT									
Engineering and Design (10 %)				1				•	\$2,813.85
Legal and Administrative (4%)				1	•				\$1,125.54
TOTAL CAPITAL COSTS		······································							\$32,077.89
CONTINGENCY (20%)									\$6,415.58
									• •
TOTAL PRESENT VALUE COST FOR	R GROUND WATER	EXTRACTION	VIA INTERC	EPTOR TREM	ICH				\$38,493.47

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE VI-4, GROUND WATER TREATMENT OPTION E MEMBRANE MICROFILTRATION SITE 10 - CAMP FOGARTY

Item	Quantity Units	Unit Price	Basis Year	Reference E	Escalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1 Present Value (O&M
CAPITAL COST - DIRECT								• •	
Microfiltration System	•								
-Microfiltration System	1 L.S.	\$450,000.00	1991	23	1.046	\$470,700.00	\$470,700.00		
-Electrical Connection	1 L.S.	\$20,000.00	1992	5	1.000	\$20,000.00	\$20,000.00		
-Piping and Controls	1 L.S.	\$20,000.00	1992	5	1.000	\$20,000.00	\$20,000.00		
Total Direct Cost									\$510,700.0
CAPITAL COST - INDIRECT									
Engineering and Design (15 %)									\$76,605.00
Legal and Administrative (5%)		•							\$25,535.0
TOTAL CAPITAL COSTS									\$612,840.0
OPERATION AND MAINTENANCE	COSTS								
Ground Water Monitoring	00010								
Sampling & Analysis		•							
(including trip blanks, field blank	s and duplicate samp	les)	Λ,						
-GW Sampling	5 samples	\$200.00	1991	5	1.024	\$204.80	\$1,024.00	10	\$7,907.3
-GW Analysis:	· · ·					,	Ţ 1,0 2 1.00		Ψ1,001.0
TAL + cyanide	6 samples	\$390.00	1992	10	1.000	\$390.00	\$2,340.00	10	\$18,069.48
 Report Preparation 	1 each	\$21,000.00	1992	17	1.000	\$21,000.00	\$21,000.00	10	\$162,162.00
Microfiltration O&M									
-Microfiltration O&M	1 year	\$75,000.00	1991	23	1.046	\$78,450.00	\$78,450.00	5	\$339,610.05
- Microfiltration Operator	2,190 man-hrs	\$20.00	1987	25	1.148	\$22.96	\$50,282.40	5 5	\$217,672.51
	_,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	,	,	20	1.140	Ψ22.50	Ψ30,202.40	3	φ217 ₁ 072.5
Discharge Sampling & Analysis									
-GW Analysis:		••••							
	12 samples	\$390.00	1992	10	1.000	\$390.00	\$4,680.00	5	\$20,259.72
-GW Analysis:	·	\$390.00	1992	10	1.000	\$390.00	\$4,680.00 \$157,776.40	5	·
-GW Analysis: TAL + cyanide Annual O&M (1992 \$) FOTAL NET PRESENT VALUE OF O	·	\$390.00	1992	10	1.000	\$390.00	•	5	<u>\$765,681.09</u>
-GW Analysis: TAL + cyanide Annual O&M (1992 \$)	·	\$390.00	1992	10	1.000	\$390.00	•	5	\$20,259.72 \$765,681.09 \$1,378,521.09 \$275,704.22

^{(1) -} Calcuised based on 5% interest rate



ALTERNATIVE VI-4, GROUND WATER TREATMENT OPTION F ION EXCHANGE SITE 10 - CAMP FOGARTY

Item	Oversia II-4-	H-MB	Baris Vara	D-1		1992	1992	Years	(1 Present
110111	Quantity Units	Unit Price	Basis Year	Reference	Escalation	Unit Costs	Costs	(O&M)	Value (O&M
CAPITAL COST - DIRECT		·							
Ground Water Treatment System									
-lon Exchange Unit	1 each	\$116,200.00	1984	12	1.219	\$141,647,80	\$141,647.80		
-Electrical Connection	1 L.S.	\$20,000.00	1992	5	1.000	\$20,000.00	\$20,000.00		
-Piping and Controls	1 L.S.	\$20,000.00	1992	5	1.000	\$20,000.00	\$20,000.00		•
-Transfer Pumps	2 each	\$470.00	1992	19	1.000	\$470.00	\$940.00		
Total Direct Cost				 				·	\$182,587.8
CAPITAL COST - INDIRECT									
Engineering and Design (15 %)									\$27,388.1
Legal and Administrative (5%)							•		\$9,129.3
TOTAL CAPITAL COSTS								-	\$219,105.3
					,				
OPERATION AND MAINTENANCE C	COSTS						•		
Ground Water Monitoring									
Sampling & Analysis									
(including trip blanks, field blanks -GW Sampling		es) \$200.00	1991	_	4 004	0004.00	04.004.00	4.0	
-GW Analysis:	5 samples	\$200.00	1991	5	1.024	\$204.80	\$1,024.00	10	\$7,907.3
TAL + cyanide	6 samples	\$390.00	1992	10	1.000	\$390.00	60 240 00	. 40	040.000.4
- Report Preparation	1 each	\$21,000.00	1992	17	1.000	\$390.00 \$21,000.00	\$2,340.00	10 10	\$18,069.4
nopoliti lopalation	r o aon	Ψ21,000.00	1332	17	1.000	\$21,000.00	\$21,000.00	10	\$162,162.0
Ion Exchange O&M									
lon Exchange Operator	4,380 man-hr	\$20.00	1987	25	1.148	\$22.96	\$100,564.80	5	\$435,345.02
 Regenerant Transportation and Disposal 	1,800,000 gal.	\$0.23	1992	17	1.000	\$0.23	\$414,000.00	5	\$1,792,206.00
-Filter Cake Transportation	90 cu. yd.	\$250.00	1992	17	1.000	\$250.00	\$22,500.00	5	\$97,402.50
-Filter Cake Disposal	9 loads	\$3,000.00	1992	17	1.000	\$3,000.00	\$27,000.00	5	\$116,883.00
Discharge Sampling & Analysis					•				
-GW Analysis:									
TAL + cyanide	12 samples	\$390.00	1992	10	1.000	\$390.00	\$4,680.00	5	\$20,259.7
Annual O&M (1992 \$)				. •		7000.00	\$593,108.80	J	ΨΕ υ ,Ευυ.12
TOTAL NET PRESENT VALUE OF O	eм ·	•							\$2,650,235.05

ALTERNATIVE VI-4, GROUND WATER TREATMENT OPTION F ION EXCHANGE SITE 10 - CAMP FOGARTY (Continued)

Item	Quantity	Units	Unit Price	Basis Year	Reference Escalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M)
SUBTOTAL CONTINGENCY (20%)									\$2,869,340.41 \$573,868.08
TOTAL PRESENT VALUE COST FOR	R ION EXCH	HANGE TRE	ATMENT SYS	STEM			· 		\$3,443,208.49

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE VI-4, GROUND WATER DISCHARGE - OPTION G DISCHARGE TO GROUND WATER SITE 10 - CAMP FOGARTY

Item	Quantity Units	Unit Price	Basis Year	Reference Es	calation	1992 Unit Costs	1992 Costs	Years (O&M)	(1 Present Value (O&M
CAPITAL COST - DIRECT							•		
Reinjection Trenches									
Excavation and Backfill	660 cu. yd.	\$3.69	1992	2	1.000	\$3.69	\$2,435.40		
Leaching Field Chambers 8'x4'x1.5'	80 each	\$240.00	1992	2	1.000	\$240.00	\$19,200.00		
-Bedding Sand	370 cu. yd.	\$24.00	1992	2	1.000	\$24.00	\$8,880.00	•	• •
-2" PVC Pipe (drilled holes) Piping From Treatment Area to	660 I. ft.	\$22.00	1991	5	1.046	\$23.01	\$15,187.92	•	•
Reinjection Trenches				•	•				
-Excavation and Backfill	370 cu. yd.	\$3.69	1992	2	1.000	\$3.69	\$1,365.30		
-PVC Piping	1000 l. ft.	\$6.70	1992	2	1.000	\$6.70	\$6,700.00		
-Bedding Sand	75 cu. yd.	\$24.00	1992	2	1.000	\$24.00	\$1,800.00		
Total Reinjection Trench Direct Cap	pital Cost						-		\$55,568.62
CAPITAL COST - INDIRECT									
Engineering and Design (15 %)									\$8,335.29
Legal and Administrative (5%)		•							\$2,778.43
TOTAL CAPITAL COSTS									\$66,682.34
SUBTOTAL									\$66,682.34
CONTINGENCY (20%)									\$13,336.47
TOTAL PRESENT VALUE COST FO	OD DISCUADOE TO C		-D						\$80,018.81

^{(1) -} Calculated based on 5% interest rate.

ALTERNATIVE VI-4, GROUND WATER DISCHARGE - OPTION H DISCHARGE TO SURFACE WATER SITE 10 - CAMP FOGARTY

Item	Quantity Units	Unit Price	Basis Year	Reference E	scalation	1992 Unit Costs	1992 Costs	Years (O&M)	(1) Present Value (O&M)
CAPITAL COST - DIRECT Piping From Treatment Area to Discharge Point Excavation and Backfill PVC Piping Bedding Sand	1300 cu. yd. 3500 l. ft. 260 cu. yd.	\$3.69 \$6.70 \$24.00	1992 1992 1992	2 2 2	1.000 1.000 1.000	\$3.69 \$6.70 \$24.00	\$4,797.00 \$23,450.00 \$6,240.00		
Total Discharge to Surface Water D	Pirect Capital Cost	*****			 .				\$34,487.00
CAPITAL COST - INDIRECT	·								
Engineering and Design (15 %) Legal and Administrative (5%)	·				•			ŕ	\$5,173.05 \$1,724.35
TOTAL CAPITAL COSTS									\$41,384.40
SUBTOTAL CONTINGENCY (20%)									\$41,384.40 \$8,276.88
TOTAL PRESENT VALUE COST FO	OR DISCHARGE TO SU	JRFACE WATE	R			•			\$49,661.28

^{(1) -} Calculated based on 5% interest rate.

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